
"HIS MASTER'S VOICE"

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6 PARRAMATTA ROAD HOMEBUSH, N.S.W.


## SPECIFICATIONS

POWER SUPPLY: $230-260$ volts, A.C., $50 \mathrm{c} / \mathrm{s}$.
CONSUMPTION:
130 watts.
AERIAL INPUT:
300 ohms balanced.
INTERMEDIATE FREQUENCIES:
Vision Carrier: $36.875 \mathrm{Mc} / \mathrm{s}$.
Sound Carrier $31.375 \mathrm{Mc} / \mathrm{s}$.
FUSE:
1 amp.
VALVES AND SEMI-CONDUCTORS

| TR1 | SE 5002 | First IF Amplifier |
| :--- | :--- | :--- |
| TR2 | SE 5002 | Second IF Amplifier |
| TR3 | BF 184 | Third IF Amplifier |
| TR4 | SE 1002 | Video Driver |
| TR5 | SE 7010 | Video Output |
| TR6 | SE 1002 | AGC |
| TR7 | SE 1002 | AGC Amplifier |
| TR8 | SE 1002 | Sync Separator |
| TR9 | SE 1002 | Noise Gate |
| TR10 | SE 1002 | Inter-Carrier Amplifier |
| TR11 | SE 1002 | Limiter |
| TR12 | SE 1002 | Audio Amplifier |
| TR13 | SE 1002 | Vertical Multivibrator |
| TR14 | SE 1002 | Vertical Multivibrator |


| VALVES AND SEMI-CONDUCTORS (continued) |  |  |
| :--- | :--- | :--- |
| TR15 | SE 1002 | Vertical Feedback Amplifier |
| V1 | 6GK8 | RF Amplifier |
| V2 | 6HG8 | Frequency Changer |
| V3 | 6BQ5 | Audio Output |
| V4 | 6CW5 | Vertical Output |
| V5 | 6JW8 | Horizontal Oscillator and |
|  |  | Reactance Valve |
| V6 | 6CM5 | Horizontal Output |
| V7 | 6AL3 | Damper Diode |
| V8 | 1S2 | EHT Rectifier |
| MR1 | OA90 | Video Detector |
| MR2 | OA210 | HT Rectifier |
| MR3 | OA210 | HT Rectifier |
| MR4 | OA91 | AGC Stand Off Diode |
| MR5 | BA100 | Delay Diode |
| MR6 | AB1101 | Noise Gate Catcher |
| MR7 | AA119 | Limiter Diode |
| MR8 | AA119 | Ratio Detector Diode |
| MR9 | AA119 | Ratio Detector Diode |
| MR10 | AB1101 | Sync Clipper |
| MR11 | BA100 | Sync Gate |
| MR12 | AB1101 | Vertical Drive Catcher |
| MR13 | OA202 | Blanking Clamp |
| MR14 | AB1101 | Phase Discriminator |
| MR15 | AB1101 | Phase Discriminator |



## CAUTION

The normal $\mathrm{B}+$ voltages in these receivers are dangerous. Use extreme caution when servicing. The high voltage at the picture tube anode ( 16,000 volts) will give an unpleasant shock but does not supply enough current to give a fatal shock. However, secondary human reactions to otherwise harmless shocks have been known to cause injury.

Always discharge the picture tube to the chassis, or to its aquadag coating, before handling the tube. The picture tube is highly evacuated and, if broken, it may violently expel glass fragments. When handling the picture tube, always wear goggles.

## CIRCUIT DESCRIPTION

## R.F. INPUT

The input signal is applied through a centre-tapped transformer matched for 300 ohm input impedance to the neutralised triode RF amplifier type 6GK5 (V1). The gain of the amplifier is controlled by the negative AGC voltage applied to its grid.

The amplified RF signal is coupled to the grid of the frequency changer type 6HG8 (V2P). A direct connection to this grid (TP1) is brought out for I.F. alignment use. The output of the local oscillator section (V2T) is also coupled in, and mixing takes place in the grid circuit. A connection (TP2) to the screen of the pentode mixer is brought out for RF alignment use.

The I.F. component of the mixer current is selected by the anode coil, L2, and coupled to the I.F. amplifier TRI.

## I.F. AMPLIFIER AND AGC AMPLIFIER

TR1 and TR2, the first two IF amplifiers, are connected in series across the low voltage rail, and their current is controlled by the output from the AGC amplifier, TR7 being applied to the base of TR1. TR1 and TR2 transistors type SE5002 are so-called "forward AGC types." This means that as the current in the transistor increases, the amplification is reduced. This requires a positive going potential on the base to reduce the gain. This is in the opposite sense to the requirements of the valve tuner, and is the reason for the inclusion of the AGC amplifier/ inverter (TR7). A second function of this transistor, an SE1002, is to compensate for the change in current in the AGC-controlled transistors to maintain a constant load on the low voltage rail, independent of AGC and therefore of signal strength.

The output from the last IF amplifier, a BF184 (TR3), is detected by an OA90 (MR1) and a narrow band of frequencies from the output is also applied to the noise gate transistor TR9, an SE1002. The band of frequencies selected normally contains very small amounts of signal power, and sufficient signal is obtained to switch on TR9 only when impulse noise occurs, or when the receiver fine tuning is set too far from the normal position.

## VIDEO DRIVER AND NOISE GATE

The detected video signal is applied to the video amplifier/driver transistor, an SE1002 (TR4). In the collector, an amplified video signal is developed across R38. This amplified video is used to drive sync. separator and AGC stages, and is gated by the noise gate transistor TR9. This video signal has positive sync. pulses. Without gating, impulse noise would appear as positive pulses, producing spurious sync. pulses and AGC voltage. When impulse noise switches on TR9, its collector falls, introducing a negative pulse to the video signal, which prevents generation of the spurious information. If the negative pulse is too great, it effectively removes the supply voltage to the driver, and interrupts the $5.5 \mathrm{Mc} / \mathrm{s}$ signal selected by IFT2 thereby introducing noise pulses in the audio section. This is prevented by the diode MR6 which limits the low voltage excursion of TR9 collector to approximately 14 V .

A video output at low impedance is taken from the emitter of the video driver through a $5.5 \mathrm{Mc} / \mathrm{s}$ null trap to the base of the video output transistor, an SE7010 (TR5).

## VIDEO OUTPUT

The picture control varies the gain of the output transistor TR5, by varying the emitter resistance, and therefore the amount of degeneration taking place in the emitter. The collector circuit has a peaking transformer to maintain a level frequency response over the video band. The signal applied to the base is proportioned, so that the black level of the picture is just at TR5 cut-off potential, and only the video information is amplified. As black level is at the cut-off potential, the gain control in the emitter does not affect the black information and gives a constant black level picture control. The proportioning of the video signal to achieve this, is controlled by the contrast range control in the AGC circuit.

## GATED A.G.C.

The AGC transistor, an SE1002 (TR6), has the output of the video driver transistor applied to its base and a potential on its emitter, which is varied with the contrast
range control. The collector is supplied with positive gating pulses from the horizontal output transformer and only passes collector current during the time of this pulse. The pulses of current build up a negative charge on C63 which is used to control the tuner gain, and through the AGC amplifier, the IF gain. The value of collector current and therefore AGC voltage is controlled by the base-emitter potential. The emitter potential is set by the contrast range control, the base potential being the sync. tip voltage at the video driver output. Variations in signal strength increase or reduce the sync. tip height, thus altering the AGC produced with a consequent change of gain to compensate for the varying signal strength. The action of this feedback loop maintains the baseemitter potential at an almost constant value. Adjustment of the emitter potential with the contrast range control, is matched by variation of receiver gain, so that the output sync. tip varies the same amount to maintain this base-emitter potential. This control therefore acts as an amplitude control of the video out from the video driver. White level approximately represents zero signal in, and therefore remains fixed, and adjustment of signal amplitude is used as the means of setting the black level at the video output transistor cut-off.

The collector-base junction of a transistor is a diode which is back-biased, and collector current is in fact the leakage across this backbiased diode. If the potential across this diode is reversed, it will cause a high current to flow. The AGC potential would appear as just such a forward bias on the collector-base junction of the AGC transistor and would rapidly discharge the AGC voltage developed across C63. The diode MR4 prevents this action occurring, being biased off by the derived negative potential.

## SYNC. SEPARATOR

The video output from the driver transistor is coupled through a capacitor to the base of the sync. separator transistor, an SE1002 (TR8). The base emitter diode d.c. restores the sync. tips to a potential just greater than the emitter potential. The current drawn by the base during sync. tips is the current amplified in the collector to produce a train of sync. pulses. The sync. pulses are then differentiated by C69-R71 for application to the horizontal phase discriminator, and integrated by R60-C80, R69-C67, R68-C66, to remove the horizontal sync. pulses for vertical triggering.

## VERTICAL MULTIVIBRATOR AND OUTPUT

The AB1101 (MR10) is normally conducting, and shorting the input sync. line to earth.

When the incoming sync. pulse is large enough to overcome the current in R90 and switch off the diode, the sync. pulse then appears across MR10 and passes on to the vertical multivibrator through the BA100 diode (MR11).

Two SE1002 transistors (TR13 and TR14) form a multivibrator to supply drive to the vertical output valve, a 6CW5 (V4).

During the scan period, TR13 is switched on and the emitter is at a potential determined by the bias components, R90B and R91. At this time, TR14 is switched off and the potential of its emitter is falling towards earth as C97 charges. The base of TR14 is connected to the collector of TR13, and the potential is determined by the drop across R93 and RV7, the vertical hold control. As TR14 emitter potential falls to a value approximately half a volt less than the base, the transistor starts to conduct, and the potential on the emitter reverses direction and rises. The rise in potential is coupled through C97 to the emitter of TR13, and reduces the current in it. The collector potential therefore rises further, switching on TR14. The action is cumulative and reverses the state of the transistors so that TR14 is on, and TR13 is off. TR13 emitter then starts to run down as C97 reverses its charge until TR13 once more switches on and returns the system to the original condition.

MR11 isolates the oscillator from the sync. feed until the end of the scan, when the return voltage of R90a drops below the bias potential on TR13 base.

MR12 prevents TR14 collector from dropping below the "knee" of the collector characteristic, thus isolating the timing components in the emitter from the collector circuit.

The collector circuit contains the capacitor Cl00 which is charged through the high value of collector resistor, and discharged by TR1 4 when it conducts during the flyback. The waveform across C100, corrected by a feedback waveform derived from the resistor in series with the yoke (R109) and amplified by TR15, is used to drive the vertical output valve $V 4$.

The whole current of V 4 is the current used by the printed board containing the transistor signal circuits, thus using the printed board as the cathode load of V4. The anode transformer (T3) drives the yoke, and an extra winding also provides vertical blanking for the picture tube.

## HORIZONTAL PHASE DISCRIMINATOR AND OSCILLATOR

The AB1101 phase discriminator diodes (MR14 and MR15) have anti-phase sine waves applied from a balanced winding on the oscillator coil, with picture phasing set
by the integrators R116, C111 and R115 and RV3, C110. Using the sine-waves as the reference voltage, a negative going sync. pulse, differentiated by C69, R71 is applied to the junction of the diodes. When the oscillator and the sync. pulse are at the same frequency and in lock, there is zero output from the discriminator.

The triode section of the 6JW8 oscillator valve, $V 5$, has its anode connected to one side of the oscillator coil, and its grid, through phase-shift network C117, R118, to the other. The signal current in the anode is therefore leading the anode voltage, and the valve has the effect of a capacitor across the tuned circuit. Variation of bias on the valve varies the magnitude of the current and of the effective capacitor, thus controlling frequency.

When the oscillator tends to run at a different frequency to the incoming sync. pulses, a positive or negative output is obtained from the discriminator which is applied to the reactance valve as bias, and varies the effective tuning capacity, bringing the oscillator back to frequency.

The oscillator is the cathode, grid and screen of the pentode section of V 5 operating as a triode, with an electron coupled output taken from the anode to drive the horizontal output stage.

## HORIZONTAL DEFLECTION CIRCUITS

The horizontal driver valve produces a negative pulse output which is timed to cut off the horizontal output valve at the end of the scan.

When cut off sharply, the magnetic field that has been established in the horizontal output transformer during the scan collapses and the oscillatory circuit comprised of the transformer inductance and stray capacitances tends to "ring." However, after onehalf cycle of oscillation the damping diode starts to conduct. During the "flyback" time the magnetic energy has established itself in the reverse direction, and the picture tube spot has returned to the left-hand side of the screen.

When the damping diode conducts, it permits current to flow at a controlled rate through part of the transformer. This current, passed by the auto-transformer into the deflection coils, form the initial part of the horizontal scan. As the damper ceases to conduct the line output valve takes over and supplies the necessary current to complete the scan, at which point a further negative pulse on the grid starts the cycle over again.

During the flyback, a high voltage pulse is produced at the anode of the EHT rectifier, which is peak-rectified and then smoothed by the capacitance between inner and outer bulb coatings of the picture tube, and supplies EHT of approximately 16,000 volts.

Energy recovered by the damping diode produces a boosted HT voltage of 690 volts which is divided down to 540 volts for supplying the G2 electrode voltage of the picture tube.
INTERCARRIER AMP. AND LIMITER
The output from IFT2 is inductively coupled to the base of the SE1002 intercarrier amplifier (TR10). The collector load of TR10 is the base circuit of the limiter transistor, an SE1002 (TR11), which limits the positive excursion of the base signal by driving the collector below the knee, and the negative excursion by cut-off and the action of the AAll9 diode (MR7). The bias for TR10 is derived from the emitter voltage of TR11, which stabilises the bias point for large variations of transistor characteristics. The collector load of TR11 is a ratio detector employing two transformers, IFT4 and IFT5, and the AA119 diodes (MR8 and MR9).
SOUND AMPLIFIER AND OUTPUT
The audio from the ratio detector is applied to the volume control RV6 and the required amount is amplified by an SE1002 transistor (TR12) and used to drive the sound output valve, a 6BQ5 (V3). Negative feedback from the output transformer is applied to the emitter of TR12 and stability at high frequencies is maintained by an auxiliary feedback loop round the output stage using C90.

## DISMANTLING

## TO REMOVE BACK

1. Disconnect aerial.
2. Remove four back-fixing screws.
3. Remove mains lead from its groove.

## to Remove the eht cage

1. Loosen the two screws at the base of the chassis back.
2. Remove the screw through the side panel.
3. Ease cage from chassis then lift, twisting it in an anti-clockwise direction.

TO REMOVE THE FRONT ESCUTCHEON

1. Pull off Channel Selector, Set Black, Picture, Volume and Off/On knobs.
2. Remove cabinet back as above.
3. With the handle in raised position, remove the five lug screws, and lift off.
TO REMOVE THE PICTURE TUBE
4. Remove front escutcheon and the Back as above.
5. Lay the picture tube on its face, remembering to protect its surface, and remove the four screws holding the picture tube. Lift off the chassis.

## ADJUSTMENTS

HORIZONTAL OSCILLATOR. This is set at the factory and normally should not need further adjustment. However, after a change of components it may be necessary to readjust. The procedure is as follows:

Set the Horizontal Hold control to the midway position. The bias at the cathode of V5 should then be approximately 2.5 volts. Short the junction of R118 and R119 to earth and adjust L34 until the picture floats into lock.

Remove the shorting lead from the junction of R118 and R119. Short-circuit the sync. by earthing the junction of R63 and R64 (i.e., the base of the sync. transistor), and adjust RV3 until the picture again floats into lock.

Remove the short-circuit and check that no delay in picture locking occurs when the channel switch is operated.

CONTRAST RANGE. First adjust the SetBlack control so that the picture information, which is normally black, is turned up to grey. Using the Vertical Hold control, roll the picture until the vertical blanking bar is visible in the centre of the screen. Adjust RV1 so that the sync. pulse is seen to be a little darker than the surrounding grey blanking bar. Return the Set-Black and Vertical Hold controls to the normal settings.
A.G.C. The pre-set AGC control should be set, when necessary, to the weakest signal, i.e., that displaying the most "snow" or grey to white flecks in the picture. Adjust the control to the position which just reduces the snow to a minimum.

FOCUS. The only time that focus adjustment may be necessary is after replacement of the picture tube. The focus potentiometer (RV11), which is a strip pre-set type, is
located underneath the chassis near the front edge and is accessible when the back is removed. Adjust for overall focus across the picture tube face.

LINEARITY. Before adjusting either vertical or horizontal linearity, the picture shift magnets should be neutralised. To do this, the two magnets should be rotated with respect to each other. The neutralised setting is such that, when both magnets are rotated together, they have little effect on the picture position.

After adjustment has been made for best linearity, the picture may need re-centring. The linearity should be retouched where necessary.

VERTICAL. The vertical linearity pre-set potentiometer RV9 is located on the R.H. sub-chassis (viewed from the back). For best linearity, RV9 should be adjusted in conjunction with the HEIGHT control, using a pattern on the screen.

HORIZONTAL. The horizontal linearity coil L35 is situated underneath the main chassis near V6, and may be adjusted from the rear. The core should be adjusted for best linearity, using a pattern on the screen. Two positions of the core provide good linearity, but the position in which the core is farthest out of the coil is the correct one.

PICTURE CENTRING. The picture may be centred by rotating the two shift magnets on the tube neck, behind the deflection yoke. Rotate both magnets together to shift the picture in the required direction, and move one magnet with respect to the other, to change the strength of the field, and so the amount of picture shift.

## INTERCARRIER I.F. ALIGNMENT



The following equipment is necessary:
(1) $5.5 \mathrm{Mc} / \mathrm{s}$ sweep.
(2) Injection probe (Fig. 1).
(3) Attenuator.
(4) Display unit.
(5) Detector (Fig. 2).

Fig. 1.
STAGE 1

## $5.5 \mathrm{Mc} / \mathrm{s}$ Trap

(a) Inject $5.5 \mathrm{Mc} / \mathrm{s}$ Sweep through probe of Fig. 1 to junction of L29 and R36 (base of TR4). Connect detector (Fig. 2) to collector of video output (TR5) and connect the display unit to the output of the detector.
(b) Adjust the slug in L30 for a minimum of output at $5.5 \mathrm{Mc} / \mathrm{s}$.


Fig. 2.

STAGE 2

## Intercarrier I.F.

(a) Remove the detector from collector of video output transistor and reconnect it to collector of TR10.
(b) Adjust level of input such that the detected output is below limiting in the amplifier. Then adjust the slugs of IFT2 and IFT3 to produce a symmetrical response about $5.5 \mathrm{Mc} / \mathrm{s}$, which should be slightly over-
coupled and with a bandwidth of 200 $\mathrm{Kc} / \mathrm{s}$.
(c) Remove detector from collector of TR10 and connect it to collector of TR11. With the input adjusted so that the intercarrier amp. does not limit, tune the slug of IFT4 for a maximum output at 5.5 $\mathrm{Mc} / \mathrm{s}$.

STAGE 3

## Ratio Detector

(a) Remove detector from TRIl and connect the display unit only to junction of R81 and C87. Increase input so that the amplifier limits.
(b) Tune slug in IFT5 to produce an $S$ response that is symmetrical, and zero at 5.5 Mc/s.

## VISION I.F. ALIGNMENT

The following equipment is necessary:
(1) I.F. Sweep.
(2) I.F. injection probe (Fig. 1).
(3) Attenuator.
(4) Display unit.
(5) $0-5$ volt bias supply.

STAGE 1
(a) Connect the display unit to junction of L29 and R36 and set $Y$ amp to give full deflection with 2 volts input.
(b) Open cut link connected to C40.
(c) Using probe of Fig. 1 and attenuator, inject I.F. sweep into last stage by connecting between C40 and earth strip.


Fig. 1.
(d) Connect +2.5 volts of bias to junction of R23 and R61.
(e) Set attenuator to give full deflection on display and tune L27 to a maximum at $34.625 \mathrm{Mc} / \mathrm{s}$. Tune IFTI to produce a symmetrical response about $34.625 \mathrm{Mc} / \mathrm{s}$. If a hole appears in the response it can be removed by detuning L32.
(f) Adjust L28 to give the desired bandwidth, and L27 and IFT1 to produce the I.F. response shape as shown in curve $A$.

STAGE 2
(a) Remove probe from C40 and reconnect link.
(b) Connect probe between tuner test point and earth, set attenuator to give full deflection on display. Switch tuner to channel 12 (blank channel).
(c) Tune L15 (located on tuner) to peak the response at $34.625 \mathrm{Mc} / \mathrm{s}$ and then tune L21 for a symmetrical response.
(d) Tune L25 and L26 to peak response at $34.625 \mathrm{Mc} / \mathrm{s}$ and then retune L15 and L21 to produce the response shape of curve $B$.

STAGE 3 (TRAPS)
(a) Adjacent Sound Carrier.

Tune L22 to $38.375 \mathrm{Mc} / \mathrm{s}$ and C23 for maximum rejection.
(b) Sound Carrier.

Tune L24 to $31.375 \mathrm{Mc} / \mathrm{s}$ (Response should be 22 db down).
(c) Noise Gate.

Tune L32 to approximately $32.5 \mathrm{Mc} / \mathrm{s}$ so that it falls 6 db below peak response.
(d) Adjacent Vision Carrier.

Tune L23 to $28.875 \mathrm{Mc} / \mathrm{s}$. It may now be necessary to retune L21 so that the response of Curve $C$ is produced.

## STAGE 4

Check that maximum gain occurs at +1.7 volts and that the response shape remains substantially unchanged between +1.7 volts and 4 volts.

I.F. ALIGNMENT CURVES


$\left.\begin{array}{l}8 \\ 9\end{array}\right\}$ A.G.C.KEYING PULSE
$\left.\begin{array}{l}7 \\ 5 \\ 6\end{array}\right\}$ A.G.C.C. TO TUNER CONTROL
4 video output
PRINTED CIRCUIT BOARD (VIEWED FROM COPPER SIDE)

## PARTS LIST - MODEL WI-EI

| REF. | PART No. | dESCRIPTION | REF. | PART No. | description |
| :---: | :---: | :---: | :---: | :---: | :---: |
| RESISTORS |  |  | RESISTORS (continued) |  |  |
| Note: All resistors are $\frac{1}{2}$ watt rating, except where noted |  |  | R73 | 740-0012 | 470 ohms $\pm 10 \%$ |
| R21 | 750-0362 | 2.7 K ohms $\pm 10 \% 5 \mathrm{watt}$ | R74 | 740-0022 | 1 K ohm $\pm 10 \%$ |
| R22 | 740-0682 | 680 ohms $\pm 10 \%$ | R75 | 740-0922 | 330 ohms $\pm 10 \%$ |
| R23 | 740-0022 | 1 K ohm $\pm 10 \%$ | R76 | 740-0252 | $1: 5 \mathrm{~K}$ ohms $\pm 10 \%$ |
| R24 | 740-1162 | 180 ohms $\pm 10 \%$ | R77 | 740-0262 | 560 ohms $\pm 10 \%$ |
| R25 | 740-0052 | 3.3 K ohms $\pm 10 \%$ | R78 | 740-0662 | 82 ohms $\pm 10 \%$ |
| R26 | 740-0382 | 6.8 K ohms $\pm 10 \%$ | R79 | 740-0382 | 6.8 K ohms $\pm 10 \%$ |
| R27 | 740-0082 | 10 K ohms $\pm 10 \%$ | R80 | 740-0382 | 6.8 K ohms $\pm 10 \%$ |
| R28 | 740-0272 | 150 ohms $\pm 10 \%$ | R81 | 740-0102 | 22 K ohms $\pm 10 \%$ |
| R29 | 740-0022 | 1 K ohm $\pm 10 \%$ | R82 | 742-0722 | 560 K ohms $\pm 10 \% 1$ watt |
| R30 | 740-0272 | 150 ohms $\pm 10 \%$ | R82a | 740-0222 | 180 K ohms $\pm 10 \%$ |
| R31 | 740-0652 | 100 ohms $\pm 10 \%$ | R83 | 740-1492 | 6.8 Megohms $\pm 10 \%$ |
| R32 | 740-0082 | 10 K ohms $\pm 10 \%$ | R84 | 740-0362 | 390 K ohms $\pm 10 \%$ |
| R33 | 740-0262 | 560 ohms $\pm 10 \%$ | R85 | 740-0022 | 1 K ohm $\pm 10 \%$ |
| R34 | 740-0082 | 10K ohms $\pm 10 \%$ | R85a | 740-0292 | 270 ohms $\pm 10 \%$ |
| R35 | 740-0002 | 390 ohms $\pm 10 \%$ | R86 | 740-1052 | 330 K ohms $\pm 20 \%$ |
| R36 | 740-0042 | 2.7 K ohms $\pm 10 \%$ | R86a | 740-0512 | 100 K ohms $\pm 20 \%$ |
| R37 | 740-0222 | 180 K ohms $\pm 10 \%$ | R87 | 740-0282 | 220 ohms $\pm 10 \%$ |
| R38 | 740-0012 | 470 ohms $\pm 10 \%$ | R88 | 742-0022 | 4.7 K ohms $\pm 10 \% 1 \mathrm{watt}$ |
| R39 | 740-0002 | 390 ohms $\pm 10 \%$ | R89 | 740-0062 | 3.9 K ohms $\pm 10 \%$ |
| R40 | 740-0322 | 1.2 K ohms $\pm 10 \%$ | R90 | 740-0222 | 180 K ohms $\pm 10 \%$ |
| R41 | 740-0322 | 1.2 K ohms $\pm 10 \%$ | R90a | 740-0242 | 33 K ohms $\pm 10 \%$ |
| R42 | 750-0632 | 8.2 K ohms $\pm 10 \% 4$ watt | R90b | 740-0112 | 27 K ohms $\pm 10 \%$ |
|  |  | Metox | R91 | 740-0242 | 33 K ohms $\pm 10 \%$ |
| R43 | 742-0812 | 1.5 Meg. $\pm 20 \% 1 \mathrm{watt}$ | R92 | 740-0032 | 2.2 K ohms $\pm 10 \%$ |
| R44 | 750-0782 | 6.8 K ohms $\pm 10 \% 4$ watt | R93 | 740-0022 | 1 K ohm $\pm 10 \%$ |
|  |  | Metox | R93a | 740-0792 | 8.2 K ohms $\pm 10 \%$ |
| R45 |  |  | R94 | 740-0242 | 33 K ohms $\pm 10 \%$ |
| R46 | 740-0062 | 3.9 K ohms $\pm 10 \%$ | R95 | 740-0072 | 4.7 K ohms $\pm 10 \%$ |
| R47 | 740-0652 | 100 ohms $\pm 10 \%$ | R96 | 742-1182 | $2.7 \mathrm{M} \pm 10 \% 1$ watt |
| R48 | 740-0692 | 150 ohms $\pm 20 \%$ | R97 | 740-0752 | 68 K ohms $\pm 10 \%$ |
| R49 | 740-0692 | 150 ohms $\pm 20 \%$ | R98 | 740-0412 | 820 ohms $\pm 10 \%$ |
| R50 | 750-0682 | 300 ohms $\pm 10 \% 5$ watt | R99 | 740-0272 | 150 ohms $\pm 10 \%$ |
| R51 | 750-0662 | 3.9 K ohms $\pm 10 \% 4 \mathrm{watt}$ | R100 | 740-0042 | 2.7 K ohms $\pm 10 \%$ |
| R52 | 740-0002 | 390 ohms $\pm 10 \%$ | R101 | 750-0642 | 15 K ohms $\pm 10 \% 4 \mathrm{watt}$ |
| R53 | 740-0532 | 1 megohm $\pm 20 \%$ | R102 | 740-0142 | 100 K ohms $\pm 10 \%$ |
| R54 | 740-0622 | 470 K ohms $\pm 20 \%$ | R103 |  |  |
| R55 | 740-0092 | 15 K ohms $\pm 10 \%$ | R104 | 740-0072 | 4.7K ohms $\pm 10 \%$ |
| R56 | 740-0032 | 2.2 K ohms $\pm 10 \%$ | R105 | 740-0122 | 47 K ohms $\pm 10 \%$ |
| R57 | 740-0382 | 6.8 K ohms $\pm 10 \%$ | R106 | 740-0202 | $2.2 \mathrm{M} \pm 10 \%$ |
| R58 | 740-0022 | $1 \mathrm{~K} \mathrm{ohm} \pm 10 \%$ | R107 | 750-0952 | 270 ohms $\pm 10 \% 4$ watt |
| R59 | 740-0062 | 3.9 K ohms $\pm 10 \%$ |  |  | Metox |
| R60 | 740-0012 | 470 ohms $\pm 10 \%$ | R108 | 740-0102 | 22 K ohms $\pm 10 \%$ |
| R61 | 740-0062 | 3.9 K ohms $\pm 10 \%$ | R109 | 746-0242 | $1 \mathrm{ohm} \pm 10 \%$ |
| R62 | 740-0022 | 1 K ohm $\pm 10 \%$ | R110 | 742-0642 | 180 K ohms $\pm 10 \%$ lwatt |
| R63 | 740-0532 | 1 megohm $\pm 20 \%$ | R111 | 742-0492 | 68 K ohms $\pm 10 \% 1 \mathrm{watt}$ |
| R64 | 740-0782 | 120 K ohms $\pm 10 \%$ | R112 | 740-0852 | 560 K ohms $\pm 10 \%$ |
| R65 | 750-0942 | 39 K ohms $\pm 10 \% 4$ watt | R113 | 740-0852 | 560 K ohms $\pm 10 \%$ |
|  |  | Metox | R114 | 740-0512 | 100 K ohms $\pm 20 \%$ |
| R66 | 740-0792 | 8.2 K ohms $\pm 10 \%$ | R115 | 742-0512 | 2.2 K ohms $\pm 10 \% 1$ watt |
| R67 | 740-0302 | 1.8 K ohms $\pm 10 \%$ | R116 | 742-1192 | 2.7 K ohms $\pm 10 \% 1 \mathrm{watt}$ |
| R68 | 740-0102 | 22 K ohms $\pm 10 \%$ | R117 | 740-0102 | 22 K ohms $\pm 10 \%$ |
| R69 | 740-0102 | 22 K ohms $\pm 10 \%$ | R118 | 740-0732 | 12 K ohms $\pm 10 \%$ |
| R70 | 740-0102 | 22 K ohms $\pm 10 \%$ | R119 | 740-0102 | 22 K ohms $\pm 10 \%$ |
| R71 | 740-0792 | 8.2 K ohms $\pm 10 \%$ | R120 | 740-0412 | 820 ohms $\pm 10 \%$ |
| R72 | 740-0092 | 15 K ohms $\pm 10 \%$ | R121 | 740-0322 | 1.2 K ohms $\pm 10 \%$ |

PARTS LIST - MODEL W1-E1 (continued)


PARTS LIST - MODEL W1-E1 (continued)

| REF. | Part no. | description | REF. | PART NO. | description |
| :---: | :---: | :---: | :---: | :---: | :---: |
| CAPACITORS (continued) |  |  | CAPACITORS (continued) |  |  |
| C79 | 271-0731 | $.047 \mathrm{uF}+80 \%-20 \% 25 \mathrm{~V}$ <br> Ceramic Disc Redcap | Cl 20 | 280-1091 | $.0056 \mathrm{uF} \pm 10 \% 400 \mathrm{~V}$ |
| C80 |  |  |  | 271-0911 | Styroseal <br> 003uF 500V Ceramic Tube |
| C81 | 280-3401 | $470 \mathrm{pF} \pm 10 \%$ 100V Styroseal | Cl20a | 271-0911 | or Disc |
| C82 | 271-0731 | $.047 \mathrm{uF}+80 \%-20 \% 25 \mathrm{~V}$ Ceramic Disc Redcap | Cl 21 C 122 | $\begin{aligned} & 271-1241 \\ & 280-1861 \end{aligned}$ | $\begin{aligned} & 820 \mathrm{pF} \pm 20 \% \text { Ceramic Tube } \\ & 820 \mathrm{pF} \pm 10 \% 400 \mathrm{~V} \end{aligned}$ |
| C83 | 280-3131 | $100 \mathrm{pF} \pm 5 \% 100 \mathrm{~V}$ Styroseal |  |  | Polyester |
| C84 | seal |  | Cl 23 | 283-1581 | $\begin{gathered} .0047 \mathrm{pF} \pm 10 \% 400 \mathrm{~V} \\ \text { Polyester } \end{gathered}$ |
| C85 |  |  | C124 | 283-1661 | $\begin{gathered} .022 \mathrm{uF} \pm 10 \% 400 \mathrm{~V} \\ \text { Polyester } \end{gathered}$ |
| C86 | 269-1211 | 12.5uF 25VW Electro |  | Polyester |  |
| C87 | 271-1571 | $.0022 \mathrm{uF} \pm 10 \%$ Ceramic | C125 | 284-2721 | $\begin{aligned} & .068 \mathrm{uF} \pm 10 \% 1000 \mathrm{~V} \\ & \text { Polyester } \end{aligned}$ |
| C88 | 283-1121 | . $01 \mathrm{uF} \pm 10 \% 160 \mathrm{~V}$ Polyester | C126 | 271-0901 | $\begin{gathered} 68 \mathrm{pF} \pm 20 \% \text { 3KVW } \\ \text { Ceramic Disc } \end{gathered}$ |
| C89 | 283-1201 | $\begin{gathered} .047 \mathrm{uF} \pm 10 \% 160 \mathrm{~V} \\ \text { Polyester } \end{gathered}$ | C127 | 284-2711 | 056uF $\pm 10 \%$ 1000V Dual Dielectric |
| C90 | 271-1631 | 18pF 500V 10\% Ceramic Tube | C128 | 284-1281 | $\begin{aligned} & 22 \mathrm{uF} \pm 20 \% \text { 1000V Dual } \\ & \text { Dielectric } \end{aligned}$ |
| C91 | 269-0931 | 25uF 25 V Electro | C129 | 283-1701 | .047uF 500V Dual Dielectric |
| C 93 \} | 269-1161 | $\left\{\begin{array}{c}16 \mathrm{uF} \\ \text { 8uF } 250 \mathrm{~V} \text { Electro }\end{array}\right.$ | C130 | 271-0911 | .033uF 500V Ceramic Tube or Disc |
| C94 | 283-1121 |  | C131 | 271-0911 | 033uF 500V Ceramic Tube or Disc |
| C95 | 269-0871 | 125uF 16V Electro |  |  |  |
| C96 | 271-0911 | .003uF 500V Ceramic Tube or Disc | C132 | 283-1701 | $\begin{gathered} .047 \mathrm{uF} \pm 10 \% 400 \mathrm{~V} \\ \text { Polyester } \end{gathered}$ |
| C97 | 283-1361 | $1.0 \mathrm{uF} \pm 10 \% 160 \mathrm{~V}$ Polyester |  |  |  |
| C98 | 271-1651 | $.0047 \mathrm{uF}+50 \%-20 \%$ 1000V Ceramic Tube |  | COILS |  |
| C99 | 271-1201 | $0.01 \mathrm{uF}+100 \%-0 \% 50 \mathrm{~V}$ Ceramic | L21 | 259-1711 | IF Input Coil <br> Trap 4 (adjacent sound) Coil <br> Trap 1 (adjacent vision) Coil <br> Trap 2 (sound carrier) Coil |
|  |  |  | L22 |  |  |
| Cl 00 | 283-1201 | $\begin{gathered} .047 \mathrm{uF} \pm 10 \% \quad 160 \mathrm{~V} \\ \text { Polyester } \end{gathered}$ | $\begin{aligned} & \mathrm{L} 23 \\ & \mathrm{~L} 24 \end{aligned}$ | $\begin{aligned} & 259-1771 \\ & 259-1761 \end{aligned}$ |  |
|  |  |  |  |  |  |
| ClOl | 283-1161 | .022uF $\pm 10 \% 160 \mathrm{~V}$ | L25 | 259-1721 | Trap 2 (sound carrier) Coil <br> 1st IF Coil Collector 2nd IF Coil Collector |
|  |  | Polyester | L26 | 259-1731 |  |
| Cl 102 | 283-1581 | .0047pF $\pm 10 \% 400 \mathrm{~V}$ | L27 | 259-1741 | 2nd IF Coil Collector <br> 3rd IF Coil Collector <br> IF Coupling Coil |
|  |  | Polyester | L28 | 259-1751 |  |
| C103) | 269-1371 | \{25uF 300VW Electro | L29 | 259-1871 | IF Coupling Coil Filter Coil |
| C104 ${ }^{\text {c }}$ |  | $\{50 \mathrm{uF} 300 \mathrm{VW}$ Electro | L30 | 259-1801 | Trap 5 (5.5 meg. trap) CoilVideo Collector Coil |
| C105 | $\begin{aligned} & 269-0971 \\ & 283-1241 \end{aligned}$ | 2000uF 25 VW Electro <br> .luF $\pm 10 \%$ 160V Polyester | L31 | 259-1821 |  |
| C106 |  |  | L32 | 259-1781 | Video Collector Coil <br> Trap 3 (noise gate) Coil Filter Coil |
| C107 |  |  | L33 | 259-1812 |  |
| C108 | 271-0961 | $560 \mathrm{pF} \pm 10 \%$ Ceramic Tube | L34 | 259-1881 | Filter Coil <br> Horizontal Oscillator Coil Linearity Coil |
| C109 |  |  | $\begin{aligned} & \text { L35 } \\ & \text { L36 } \end{aligned}$ | 259-1252 |  |
| C110 | 280-3441 | $.0047 \mathrm{uF} \pm 5 \%$ 50V Styroseal $0047 \mathrm{uF} \pm 5 \% 50 \mathrm{~V}$ Styroseal $1 \mathrm{luF} \pm 10 \% 160 \mathrm{~V}$ Polyester |  | 259-0045 | Antiparasitic Coil |
| Clll | $\begin{aligned} & 280-3441 \\ & 283-1241 \end{aligned}$ |  | L37 | 259-0045 | Antiparasitic Coil |
| C112 |  |  |  |  |  |
| C113 |  |  |  | POTENTIOMETERS |  |
| C114 | 283-1141 | $.015 \mathrm{uF} \pm 10 \%$ 160V Polyester | RV1 | 677-1541 | 500 ohms CTS Curve ' ${ }^{\text {D }}$ (linear)-Contrast Range |
| C115 |  |  |  |  |  |
| C116 | 280-5241 | $1.0 \mathrm{uF} \pm 20 \% 50 \mathrm{~V}$ Metalised | RV2 | 677-1631 | 1.5K ohms CTS Curve 'D' <br> (linear)—AGC |
| C117 | 271-0571 | Lacquer <br> $22 \mathrm{pF} \pm 10 \%$ NPO Ceramic Tube | RV3 | 677-1621 | IK ohm CTS Curve 'D' (linear) Discriminator Balance |
| C118 | 283-1361 | $1.0 \mathrm{uF} \pm 10 \% 160 \mathrm{~V}$ Polyester | RV4 | 677-1501 | 500K ohms Curve ' A '-Set Black |
| C119 | 280-1101 | $\begin{aligned} & .0068 \mathrm{uF} \pm 10 \% 400 \mathrm{~V} \\ & \text { Styroseal } \end{aligned}$ | RV5 | 677-1511 | 1K ww Curve 'A'-Picture |

PARTS LIST - MODEL W1-E1 (continued)

| REF. | part no. | description | REF. | part no. | description |
| :---: | :---: | :---: | :---: | :---: | :---: |
| POTENTIOMETERS (continued) |  |  | DIODES |  |  |
| RV6 | 677-1481 | 250K ohms Curve ' C '- | MR1 | 932-0971 | OA90-Video Detector |
|  |  | Volume | MR2 | 932-1071 | OA210-HT Rectifier |
| RV7 | 677-1491 | 500 ohms Curve 'A'- | MR3 | 932-1071 | OA210-HT Rectifier |
|  |  | Vertical Hold | MR4 | 932-2031 | OA91-AGC Stand Off Diode |
| RV8 | 677-1641 | 2 Megohms Curve 'A'- | MR5 | 932-2451 | BA100—Delay Diode |
|  |  | Height | MR6 | 932-2601 | AB1101-Noise Gate |
| RV9 | 677-0172 | 25K ohms Curve 'A'- |  |  | Catcher |
|  |  | Vertical Linearity | MR7 | 932-2271 | AA119-Limiter Diode |
| RV10 | 677-1521 | 100K ohms Curve 'A'- | MR8 | 932-2271 | AAI19-Ratio Detector Diode |
|  |  | Horizontal Hold | MR9 | 932-2271 | AAI19-Ratio Detector Diode |
| RV11 | 677-0891 | 2 Megohms Curve 'A' StripFocus. | MR10 | 932-2601 | AB1101-Sync Clipper |
|  |  |  | MR11 | 932-2451 | BA100-Sync. Gate |
|  |  |  | MR12 | 932-2601 | AB1101-Vertical Drive Catcher |
|  | TRANSFORMERS |  | MR13 | 932-2631 | OA202-Blanking Clamp |
|  |  |  | MR14 MR15 | 932-2601 | AB1101-Phase Discriminator |
| T2 | 905-0661 | Audio Output Transformer | MR15 | 932-2601 | AB1101-Phase Discriminator |

## MISCELLANEOUS

| VC5 | 281-0391 | C004-Capacitor Trimmer |
| :---: | :---: | :---: |
| SW1 | 855-0781 | Switch, Off/On |
| FSI | 431-0071 | Fuse, 1 amp . |
| CHI | 232-0351 | HT Filter Choke |
| VDRI | 750-0691 | Voltage Dependent Resistor, Type E298 ED/A262 |
| VDR2 | 750-0611 | Voltage Dependent Resistor, Type E299 DE/P350 |
|  | 106-0071 | Aerial Assembly Telescopic with MTG and Lug screw |
|  | 148-5751 | Bracket Tuner Mounting |
|  | 148-5761 | Bracket Aerial MTG |
|  | 148-5801 | Bracket Aerial Terminal MTG |
|  | 190-3121 | Cabinet Back |
|  | 224-2041 | Chassis Assembled and Wired MSP Tuner, type TB14 |
|  | 259-1661 | Coil Deflector Yoke Rola TV 2064 with 7" leads |
|  | 403-3081 | Escutcheon Assembly |
|  | 470-0241 | Handle Assembly |
|  | 517-2631 | Knobs |
|  | 517-2661 | Assembly Channel Selector Knob |
|  | 794-1901 | Scale Control Indication |
|  | 831-2601 | Ear Piece with lead and plug |
|  | 824-1161 | Socket, Miniature Jack Type SG1003 |
|  | 831-2511 | BK Speaker, $5^{\prime \prime} \times 3^{\prime \prime}$ MSP, Type 53LB15 15 ohms |
|  | 895-0031 | Terminal MSP 5458 Spring |
|  | 932-2791 | CRT Shelbond 17", Thomas 17RVP4. |

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