

For Trade Use Only

## "HIS MASTER'S VOICE"

## SERVICE MANUAL

for

CHASSIS TYPES

# PF - PG - PH - PJ - PK <br> TELEVISION RECEIVERS 

E.M.I. (AUSTRALIA) LIMITED

HOMEBUSH : : N.S.W.

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## INTRODUCTION

This combined service manual is intended to give the serviceman, within the one cover, a complete coverage of all of the present series of "H.M.V" 110 -degree receivers and provide him with all of the necessary information for servicing these receivers. It is anticipated that by combining this information, that would normally be written in separate manuals, that a more complete understanding of the variations in circuitry between these receivers will result, and that servicing will thus be simplified.

It will be seen that the basic chassis may be divided into 15 - or 16 -valve receivers; that the method of mounting is divided into a console, lowboy or consolette type receivers; and that the remote control facility is confined to 16 -valve receivers. Aerial selection switching is standard on all $\mathrm{R} /$ control models.

The receivers covered in this manual are:


## CAUTION

The normal $\mathrm{B}+$ voltages in these receivers are dangerous. Use extreme caution when servicing. The high voltage at the picture tube anode ( 16,000 volts) will give an unpleasant shock but does not supply enough current to give a fatal burn or shock. However, secondary human reactions to otherwise harmless shocks have been known to cause injury.

Always discharge the picture tube anode to the chassis or to its aquadag coating before handling the tube. The picture tube is highly evacuated and if broken it will violently expel glass fragments. When handling the picture tube, always wear goggles.

## SPECIFICATIONS

POWER SUPPLY:
200, 230, 240, 250 volts, A.C., 50 c.p.s.
CONSUMPTION:
15-valve receivers - 175 watts.
16-valve receivers - 180 watts.
AERIAL INPUT:
300 ohms balanced.
Consolette receivers have provision for a plug-in attenuator.

INTERMEDIATE FREQUENCIES
Vision carrier - $36.875 \mathrm{Mc} / \mathrm{s}$. Sound carrier - $31.375 \mathrm{Mc} / \mathrm{s}$.

FUSES:
Mains - 1.5 amp .
H.T. 1 - 1.5 amp .
H.T. $2-250 \mathrm{~mA}$.

## VALVE COMPLEMENTS

> 15-VALVE RECEIVERS - PH, PJ, PK.

| V1 | 6ES8 |
| :--- | ---: |
| V2 | 6HG8 |
| V3 | 6BY7 |
| V4 | 6BX6 |
| V5 | 6EJ7 |
| V6 | 6DX8 |
|  |  |
| V7 | 6CS6 |
| V8 | 6U8 |
|  |  |
| V9 | 6AU6 |
| V10 | 6GW8 |


| R.F. Amplifiers. <br> Frequency Changer | V11 | 6BM8 |
| :--- | :--- | ---: |
| 1st I.F. Amplifier |  |  |
| 2nd I.F. Amplifier | V12 | 12AU7 |
| 3rd I.F. Amplifier | V13 | 6CM5 |
| Video Amplifier and Noise | V14 | 1S2 |
| Inverter | V15 | 6AL3 |
| Noise Gated Sync. Separator | MR1 | 0A80 |
| Sound I.F. Amplifier and | MR2 | 0A210 |
| $\quad$ MR3 | $0 A 210$ |  |
| Gound Limiter. A.G. | MR4 | M3 |
| Audio Driver and Audio | MR5 | 0A79 |
| Output | MR6 | 0A79 |
|  | MR7 | 0A81 |
|  | MR8 | 0A81 |

Blocking Oscillator and Vertical Output
Horizontal Multivibrator
Horizontal Output
EHT Rectifier
Damping Diode Vision Detector
Mains Rectifier
Mains Rectifier
Clamping Diode
Ratio Detector
Ratio Detector
Phase Discriminator
Phase Discriminator

16-VALVE RECEIVERS - PF, PG.

| V1 | 6ES8 | R.F. Amplifier | V15 | 6AL3 | Damping Diode |
| :---: | :---: | :---: | :---: | :---: | :---: |
| V2 | 6HG8 | Frequency Changer | V16 | 6BL8 | Remote Control Amp. and |
| V3 | 6 BY 7 | 1st I.F. Amplifier |  |  | Relay Operating |
| V4 | 6BX6 | 2nd I.F. Amplifier | MR1 | 0A80 | Vision Detector |
| V5 | $6 \mathrm{EJ7}$ | 3rd I.F. Amplifier | MR2 | 0A210 | Mains Rectifiers |
| V6 | 6DX8 | Video Amplifier and Noise | MR3 | 0A210 | Mains Rectifiers |
|  |  | Inverter | MR4 | M3 | Clamping Diode |
| V7 | 6CS6 | Noise Gated Sync. Separator | MR5 | 0А79 | Ratio Detector |
| V8 | 6U8 | Sound I.F. Amplifier and | MR6 | 0A79 | Ratio Detector |
|  |  | Gated A.G.C. | MR7 | 0 A 81 | Phase Discriminator |
| V9 | 6AU6 | Sound Limiter | MR8 | 0A81 | Phase Discriminator |
| V10 | 6GW8 | Audio Driver and Output | MR9 |  | Bias Rectifier |
| V11 | 6BM8 | Blocking Oscillator and Vertical Output | MR10 <br> MR11 | 1 | Power Rectifiers for Remote |
| V12 | 12AU7 | Horizontal Multivibrator | MR12 |  | Control |
| V13 | 6CM5 | Horizontal Output | MR13 |  |  |
| V14 | 1S2 | EHT Rectifier | MR14 |  | Bias Rectifier |



BLOCK DIAGRAM - 15-VALVE CIRCUITS


## SUMMARY OF FEATURES

These features are common to both types of receivers, unless otherwise stated.

1. The turret tuner has facilities for individual exact alignment, on each channel, of the oscillator tuning so that use of the fine tuning control may be unnecessary.
2. Linear phase treatment of the IF response ensures the best possible definition with freedom from overshoot or smearing, allowing non-critical fine tuning control.
3. The overall frequency response of the system is within 6 db from D.C. up to $4.7 \mathrm{Mc} / \mathrm{s}$.
4. DC coupling from the video detector through to the picture tube ensures that a true black is retained and that all shades retain their true relationship to black. This prevents fading to grey and gives accurate portrayal of night-time scenes.
5. Time-gated A.G.C. is employed, giving immunity from the effects of impulse noise and has a fast action to cope with rapid fading from "aircraft flutter." A variable delay on the tuner is provided to maintain full RF gain on weak to moderate signals, thus minimising frequency converter noise. This delay can be adjusted for best results when the receiver is first installed.
6. A noise inverter is used, before the sync. separator, giving protection to the input circuit of the sync. separator in the presence of impulse noise, preventing paralysis of the sync. separator action following large bursts of impulse noise.
7. The audio amplifier with ample feedback gives excellent quality sound with ample power. A compensated volume control maintains tonal balance at all volume settings.

A variable tone control is fitted and frequency response can be adjusted from full and normal to attenuated high and low frequencies simultaneously. This system is used rather than accentuated or attenuated bass or treble, so that the intelligibility of the signal in "fringe" conditions will be retained.
8. The horizontal hold circuit is a multivibrator employing a stabilising coil in the oscillator anode circuit and this, together with the cathode coupling employed, gives a stable oscillator virtually unaffected by large HT variations. This stability, together with an adequate pull-in range, renders a front horizontal hold control unnecessary. A pre-set control is provided on the back of the receiver.
9. A linearity control of the horizontal deflection circuit that can be adjusted by an indication on a multimeter gives the advantage that the linearity can be set without the need for a transmitted test pattern.
10. Vertical retrace lines are eliminated by Vertical Flyback Blanking.
11. Dustproof seal around picture tube to eliminate dust which would, otherwise, be attracted by static charge. (Models using unbonded face picture tubes only).
12. The user controls are reduced to the minimum necessary to ensure correct operation, which is made as simple as possible. There are no interacting controls, and since the receiver is completely DC coupled then the Brightness control will vary the light output of the picture tube and the Contrast control will vary the depth of shades without any interaction between them.
13. Silicon Junction Diodes are used in a voltage doubler full-wave power supply. These diodes are noted for their robustness, economy of power and high surge rating. Since they have no heated cathode they cannot be damaged by operation on low mains voltage as is the case with valve rectifiers. Thermistor protection is included in the power supply on all models, to ensure that diodes and electrolytic condensers are not subject to large surges when first switching on the receiver.
14. The chassis is hinged and can be swung out in such a manner that almost any repair can be made in the home without removing the whole chassis from the cabinet. It is also possible to remove the whole receiver, complete with the picture tube, from the cabinet in one piece as a complete working unit, and can be operated as such on the workshop bench.
15. A noise-gated sync. separator is used to give the best synchronisation obtainable, necessary for receivers operating under "fringe" conditions.
16. To keep impulse interference to a minimum in the audio output and when operating under adverse conditions, a sound I.F. amplifier is included before the sound limiter. This gives a substantial increase in gain and gives virtually noise-free sound, even under extreme "fringe" conditions.
17. Current feedback to keep a constant deflection current in the coils is used in the vertical deflection circuit. This feature holds the height constant as the deflection coils warm up.
18. Transformer-coupled focusing is employed to ensure good overall edge-to-edge focus. Degradation of definition due to change in spot shape across the tube is thus obviated.
19. Full Remote Control facilities are provided in the 16 -valve, type PF-PG receivers.

The receiver may be switched "on" or "off" from a remote location; channel selection and adjustment of contrast and sound can also be made. The speaker system may be transferred
from the receiver cabinet to the remote control unit and volume adjusted accordingly.

Facilities are also provided in the remote control unit for connection of hearing aids with and without local or remote speakers plus control of volume in the hearing aid.

Muting of the sound and picture is carried out whenever channels are changed.

With the remote control unit connected to the
receiver, normal functioning of the manual controls on the receiver still exist.
20. In models PF and PG, facilities have been provided for the automatic switching of up to four different types of aerials, depending on frequency and transmission modes, to the aerial terminals on the tuner, by means of the multi-aerial connector block and the wafer switches on the channel changing mechanism.

## CIRCUIT DESCRIPTION

## R.F. INPUT

The input to the turret tuner is to a centre tapped transformer which presents an impedance of 300 ohms.
R.F. amplification is achieved with a type 6ES8, double triode (V1), in a cascode circuit. The two sections of this stage are connected in series for DC. The grounded cathode input section is neutralised and is also controllable by A.G.C. from the mains chassis. Because of the series DC connection of the two portions, A.G.C. voltage to one section also effects control on the other section.

Coupling between the two sections of the cascode is direct and the coil between the two maintains amplification on the high frequency channels.

Inductive coupling is used between the cascode and mixer. V2, a type 6 HG 8 , combined triode-pentode, is used as oscillator and mixer. The oscillator is a Colpitts circuit operating above signal frequency. Injection to the mixer input is by inductive coupling. The fine tuning variable capacitor is connected directly across the oscillator inductance. The condenser is spring loaded at one end and adjustment of range is determined by a range determining screw located on the front end of the tuner.

Adjustment on each channel is provided by means of an adjustable screw operating a cam to vary the fine tuning capacitor. The adjustable screw is varied by depressing the fine tuning knob, located within the channel selector knob, and rotating it in either direction. The extent of rotation is approx. 3 to 4 complete turns.

The intermediate frequency output of the tuner (vision $36.875 \mathrm{Mc} / \mathrm{s}$. , sound $31.375 \mathrm{Mc} / \mathrm{s}$.) is coupled to the IF channel of the main chassis through a condenser C10, .001 uF .

The heater circuit is filtered by a Ferrite bead through which a heater wire is passed. The bead concentrates the field around the wire, increasing its self-inductance so that it acts as a choke.
I.F. AMPLIFIER

The tuner IF output is coupled to the grid of the first IF Amplifier V3 via the bottom end of the coil L21. There are three IF amplifying stages and AGC voltage is applied to V3.

V5 is coupled to the video detector MR1 by inductive coupling.

Trap circuits L22, L24 and L27 are coupled to the IF coils L21, L23 and L26. The first attentuates the sound carrier $31.375 \mathrm{Mc} / \mathrm{s}$. and the second attenuates the adjacent vision carrier $29.875 \mathrm{Mc} / \mathrm{s}$. The third trap attenuates the adjacent sound carrier $38.375 \mathrm{Mc} / \mathrm{s}$.

V3 has a small unbypassed cathode resistor R23, to minimise detuning of the grid circuit with varying input levels.

## VIDEO AMPLIFIER

The detected video output of the germanium diode MR1 is amplified in the pentode section of V6. L31, L32, L33 and L34 are peaking chokes which maintain the high frequency components of the vision signal fed to the picture tube. The $5.5 \mathrm{Mc} / \mathrm{s}$. component is removed by the combined transformer and trap, IFT4.

## INTERCARRIER SOUND

The output of IFT4 is fed to the Sound IF amplifier, V8. The output from the limiter is demodulated by the ratio detector, 2-0A79, to provide the audio signal which passes through the volume control to be amplified in the driver triode and output pentode sections of the Audio Output valve. Feedback is applied in both audio circuits.

A full margin of sound gain is provided so that 1.65 watts undistorted output is obtained from sound signals which are not fully modulated. Moreover, the sound output stage has a controlled overload charactertistic which does not "paralyse" but merely clips the peaks and so remains comparatively free from audible distortion.

## NOISE INVERTER

The anode load of the noise inverter is formed by the resistor coupling the sync. separator to the video output. The valve is biased such that it cannot conduct on the positive sync. tips. However, noise pulses appearing more positive at its grid will drive the valve into conduction, causing current to flow and a voltage drop across this resistor. Consequently a noise pulse will appear less positive, at the anode of the noise inverter, than a sync. tip and the sync. separator will not conduct on the noise pulse since the pulse will now fall outside of the sync. separator's grid base.

## NOISE-GATED SYNC. SEPARATOR

Video signal, with sync. tips positive, is applied to the suppressor grid of a 6CS6 from the output of the video amplifier. At the same time, video signal with sync. tips negative, is applied to the control grid of this valve, via the potentiometer R69, R70 and is so arranged that the negative excursion of the signal will not affect the current through the sync. separator valve. However, when a noise pulse, which will sit more negative than the sync. tips, occurs at the control grid, then the current through the valve is cut off and the anode voltage will rise to HT, giving no spurious sync. output. Double protection is thus afforded by the Noise Inverter and the Noisegated Sync. Separator.

## GATED A.G.C.

Video signals with sync. tips positive are fed from the Video Amplifier anode to the grid of the AGC valve, and the valve is biased so that it will only conduct on sync. tips. During line flyback, a positive pulse is applied to its anode via the 68 pfd coupling capacitor and the valve will conduct when this pulse at its anode and a sync. tip at its grid coincide. The valve cannot, therefore, conduct in the period between sync. pulses and is thus immune to noise pulses appearing in the period between sync. pulses.

The current through the valve will depend on the height of the sync. pulses at its grid and the height of these sync. pulses is adjusted by the contrast control. The cathode of the A.G.C. valve is held at about 50 volts. Operation of the Contrast Control will vary the bias applied to the grid of the A.G.C. valve and so increase or decrease the height of sync. tips in respect to the fixed cathode volts. Increasing the height of the sync. tips will cause the valve to conduct harder and will produce more A.G.C. volts, reducing the gain of the receiver and decreasing the voltage available to drive the C.R.T. cathode. Decreasing the height of the sync. tips will reduce the conduction of the A.G.C. valve, thus producing less A.G.C. volts, increase the gain of the receiver and increase the volts available to drive the C.R.T. cathode. Increasing the height of the sync. tips therefore reduces the contrast, and decreasing the height of the sync. tips will increase the contrast.

The ratio of I.F. A.G.C. voltage to Tuner A.G.C. voltage is important and the ratio can be adjusted by means of RV3. If the ratio is too small then, even on large signals, the tuner will be biased back and the I.F. amplifier will be operating at an unnecessarily large gain and converter noise will be evident in the picture. If the ratio is too large, then no controlling bias will be applied to the tuner and it will be held at the clamping voltage and all control will be made in the I.F. amplifiers. This can cause severe overloading of the I.F. amplifier.

## VERTICAL DEFLECTION CIRCUITS

Vertical sync. pulses from the sync. separator are used to synchronise the blocking oscillator, T3, and the triode portion of the valve. "Height" is adjusted by varying the DC potential fed to the blocking oscillator anode and "Vertical Hold" is adjusted by varying the time constant of the blocking oscillator grid circuit. The sawtooth waveform from the blocking oscillator is applied to the grid of the output amplifier and a sawtooth current waveform appears in the vertical output transformer. A feedback voltage is developed across R134, R135, from the current in the deflection coils. This voltage is stepped up to the input grid of the vertical output valve. A potentiometer, RV10 is provided for adjustment of linearity.

## HORIZONTAL OSCILLATOR AND AUTOMATIC PHASE CONTROL

Automatic frequency and phase control is obtained by means of a DC controlled, cathodecoupled, stabilised multivibrator controlled by a germanium diode phase discriminator.

Sync. pulses from the sync. separator are fed into the centre of the discriminator and a sawtooth waveform from the multivibrator output is fed across the diode loads.

Since the negative going sync. pulse is fed to the diode cathodes and the diodes are effectively in parallel, then the discriminator output will be zero volts. The sawtooth is not of sufficient amplitude to cause the diodes to conduct, due to the bias caused by the coupling capacitor, so that the DC components of the sawtooth (average AC) is zero volts. Neither the sawtooth nor the sync. pulses can cause a bias voltage to be developed across the discriminator but that part of the sawtooth that occurs at the instant of the sync. pulses will have an affect on the bias voltage produced. If the sync. pulse occurs in the centre of the sawtooth, then the output is zero volts, and if it occurs before the retrace passes through its zero axis then the oscillator is running slow and the output voltage will be negative. The reverse will be the case if the oscillator is running fast.

The frequency of the Horizontal Multivibrator is controlled by the DC output of the discriminator. If the output voltage of the discriminator is positive it causes the cathode voltage to rise, lengthening the discharge time of the coupling capacitor to the second triode and slows down the firing rate of the multivibrator. A negative output from the discriminator will have the reverse effect.

## HORIZONTAL DEFLECTION CIRCUITS

The horizontal driver valve produces a negative pulse output which is timed to cut off the horizontal output valve at the end of a scan.
When cut off sharply, the magnetic field that has been established in the horizontal output trans-
former during the scan collapses and the oscillatory circuit comprised of the transformer inductance and stray capacitances tends to "ring." However, after one-half cycle of oscillation the damping diode starts to conduct. During the "flyback" time the magnetic energy has established itself in the reverse direction, and the picture tube spot has returned to the left-hand side of the screen.

When the damping diode conducts it permits current to flow at a controlled rate through part of the transformer. This current, passed by the auto-transformer into the deflection coils, forms the initial part of the horizontal scan. As the damper ceases to conduct the line output valve takes over and supplies the necessary current to complete the scan, at which point a further negative pulse on the grid starts the cycle over again.

During flyback a high voltage pulse is produced at the anode of the EHT rectifier, which is peak-rectified and then smoothed by the capacitance between inner and outer bulb coatings of the picture tube, and supplies EHT of approximately 16,000 volts.

Energy recovered by the damping diode produces a boosted HT voltage of 830 volts, which is divided down to 560 volts for supplying the G2 electrode voltage of the picture tube.

The sawtooth scanning current in the primary winding of the focus transformer, T7, produces in the secondary, a large parabolic voltage waveform which is fed direct to the focus electrode of the CRT and the cold end of the secondary is connected to a suitable voltage to give good overall focus.

## REMOTE CONTROL

(16-valve receivers only)
The remote control unit is connected to the receiver by fitting a small 9-pin plug (PL3), into the socket (SKT-3), at the rear of the chassis. With mains power connected and the receiver mains switch "on," the receiver may be switched "on" or "off" by the slide switch on the side of the remote handpiece which completes the circuit of the bridge rectifier, MR10-11-12-13, via a lamp in the handpiece. Power is supplied to RLB relay which closes, "making" contacts B1 and completing the receiver mains transformer primary, and contacts B2 which earths the resistor network in the picture tube grid.

Closing the receiver mains switch supplies power to the remote unit mains transformer, T8, which in turn supplies a bias voltage to V16-T (6BL8) via MR9 and C53. This bias cuts off the plate current of the triode. A tap taken from T8 supplies an AC voltage to the transformers T9 and T10, "indexing transformers." Under normal operating conditions an equal AC voltage is supplied to the grid and cathode of the pentode section of V16 (6BL8), via switches SB and SC,
which are connected to the taps on the indexing transformers. The control under these conditions is "at rest."

## OPERATING SEQUENCE

After selection of the appropriate channel by, the remote control switch, if the "mute-start" push-button in the handpiece is operated, the following steps take place:

PSA-1 makes and shorts the limiter HT to earth, muting the sound.
PSA-2 makes and shorts the cathode of V16-T to earth, causing heavy current to flow in the plate circuit which operates relay RLA.
When relay RLA operates:
Contacts A1 close and supply power to the channel changing motor.
Contacts A2 close and short-circuit B1 contacts in the "hold" position.
Contacts A3 close and short the limiter HT to earth.
Contacts A4 close and short the cathode of V16-T to earth in the "hold" position.
Contacts A5 close and short the picture tube grid to earth via R45, muting the picture.
All actions occur simultaneously.

Since an unequal voltage is appearing at the grid of V16-P to that appearing at the cathode as selected by the channel selector switch in the handpiece, the difference voltage is amplified by V16-P and fed back to the grid of V16-T via C56. This AC voltage is rectified by MR14 and its polarity is such that it cancels the bias already supplied by MR9/C53 combination, and causes heavy current to flow in V16-T and holds the relay RLA in operating condition until the voltage is reduced to zero after the grid of V16-P is adjusted to the same voltage as the cathode by switch SB.

Simultaneously with the application of "bucking" bias to V16-T grid, the grid is shorted to earth by the switch MSB which is cam-operated by the movement of the channel switching motor. This is a sensing device and stops the channel switching motor as it opens at the selected channel and since there will be no "bucking" bias applied to the grid of V16-T at that point, the relay RLA ceases to operate and the ' $A$ ' contacts open. The contacts of MSB open at each channel position but since heavy "bucking" bias still exists on the grid of V16-T the motor will continue until the selected position has been reached.

When the relay RLA ceases to operate:
Contacts A5 open-picture appears on screen.
Contacts A4 open-short and "bucking" bias removed from V16-T grid. Normal "at rest" "cut off" bias is restored.
Contacts A3 open-Limiter HT is restored and sound is heard.
Contacts A2 open and remove the short on B1 contacts.
Contacts A1 open and remove AC power from channel selector motor.
All actions occur simultaneously.
When the "on-off" switch in the handpiece is switched "off" relay RLB operates and opens contacts B2 which remove the earth from the picture tube grid voltage divider, immediately placing a high positive voltage on the grid and preventing a bright spot to appear on the screen, and contacts B1 which remove power from the receiver mains transformer.

A pin in the centre of PL3 which inserted in SKT3 open-circuits two leaf switches MSA-1 and MSA-2, on the main chassis. MSA-1 connects a 82 ohms load resistor across the rectifier

M10-11-12-13 and represents the PLP load when the remote handpiece is disconnected. MSA-2 completes the speaker voice coil circuit when the remote handpiece is disconnected. (Channel selection cannot be achieved until the valves have reached operating temperature).

Under the above conditions, a small amount of power (approx. 1 watt) is still consumed by the transformer T8 until the receiver mains switch is operated to isolate the complete unit.

Volume of the receiver may be adjusted at the handpiece for both local and remote speakers by variation of the limiter HT by RV-15 control.

Two sockets are available on the side of the remote handpiece for hearing aid plugs. Insertion of the hearing aid plug into SKT-4 with the "local remote" speaker switch in the remote position, removes sound from the speaker and supplies sound to the hearing aid only. In both cases the hearing aid sound may be controlled by the hearing aid volume control.

For the remote handpiece controls to be fully effective, the receiver volume and contrast controls should be well advanced. If these controls are so set, removal of the remote control plug PL3, will not disturb the contrast or sound when the receiver is operating normally.

## INSTALLATION

The receiver is shipped from the factory with the picture tube installed and all controls preadjusted for normal operation. For chassis type PH - PJ - PK, it should only be necessary to ensure that the mains tapping is correctly adjusted for the mains voltage existing in the particular area and a suitable aerial connected to the aerial terminals.

For chassis type PF - PG it will be necessary to unpack the remote control unit and fit the plug into the socket at the rear of the cabinet. All adjustments can then be made from the remote control unit after the various controls have been set on the receiver front.

In the case where more than one aerial is intended or installed for reception from diverse directions or from different types of transmissions, It will be necessary to connect the 300 -ohm ribbon leads from the multi-connector block at the rear of the set, to the lugs on the rotary switch for the appropriate channel.

In very strong signal areas it may be necessary to use an attenuator in the aerial lead to avoid overloading the receiver.

The various operating controls should be checked for proper operation, and their use demonstrated to the purchaser as described in the installation manual. It is necessary to remove the back of the cabinet to gain access to the mains adjustment plug or aerial connections to the switch.

## PICTURE SHIFT

Small shifts in position of picture may occur due to the effect of the earth's magnetic field in different locations. The picture may be re-centred by rotating the two shift magnets on the tube neck behind the deflection yoke.

Rotate the centring magnet assembly to shift the picture in the required direction, and move one of the magnets with respect to the other to change the strength of the field and hence the amount of picture shift.

## PICTURE TILT

If the picture is not square with the edges of the mask, the deflection coils should be rotated until the picture is squared up. It may be necessary after this operation to centre the picture by means of the shift magnets.

## A.G.C.

The A.G.C. control is normally preset in the factory but if it is necessary to adjust it at any time the procedure is to turn the control to the maximum anti-clockwise position, then observing the picture, advance the control until the noise or "snow" in the picture is no longer reduced. The receiver should then be checked on all channels to ensure that no overloading is evident, which may be due to the control being adjusted too far in a clockwise position, and that the minimum noise condition has been achieved for all signals.

## FUSES

Three fuses are provided, one in the mains circuit and two in the HT circuits. Ensure that they are replaced with similar types.

## NOISE INVERTER

The cathode bias of the noise inverter can be adjusted on installation (if necessary) by means
of a pre-set control on the rear panel of the receiver. Tune to the strongest signal and turn contrast control to maximum. Turn the Noise Inverter control in an anti-clockwise direction until the picture tends to go out of lock. Turn control slightly clockwise so that picture returns to lock. Check that receiver locks quickly on all channels when changing channels.

## SERVICING

The vertical chassis of this receiver has been especially designed to make servicing as easy as possible. All valves, test points and major components are accessible to the serviceman when the cabinet back is removed. All other components may be serviced by swinging the chassis out so that all of the receiver is accessible.

To do this, remove the EHT lead from its support; slacken off the screws on the right-hand side of the chassis and remove the clamp. Note that one of these screws is intended as a factory transit screw only, and need not necessarily be replaced. Remove screw from below mains transformer. This is also a transit screw and need not necessarily be replaced. The chassis, pivoting
about the left-hand side, may be swung out to an angle of approximately 60 degrees. By disconnecting EHT, yoke and picture tube leads, the chassis may be swung out to a greater angle thus enabling better access to the underside for inspection or repair.

To secure the chassis, reconnect any disconnected leads and replace the screw below the power transformer before the retaining clamp and its screws are replaced.

If the repair or replacement cannot be made without removing the chassis from the cabinet, the receiver can be withdrawn as a complete working unit and can be operated as such on the workshop bench.

## DISMANTLING <br> CHASSIS TYPES PF, PG, PH, PJ.

## REMOVAL OF CHASSIS ASSEMBLY

Remove the bottom screws securing the back cover of the receiver to the cabinet. Ease the back cover down until the top edge is free of the cabinet groove. Withdraw the cover straight back over the picture tube neck.

WARNING: Be careful not to drop the cover on to the neck of the picture tube when the bottom screws are removed.

Pull off the four small knobs from the front of the receiver. Undo the grub screw and remove the collar on the contrast spindle. Pull off the channel selector and fine tuner knobs together. The fine tuner knob may be removed from inside
the channel selector knob by gentle tapping if it becomes tight.

Remove the thumb screw from the T nut holding the tuner chassis to the cabinet side support block. (Chassis PF and PG only) Disconnect the speaker lead plug at the left hand side of the chassis (from rear). Remove two bolts that secure the base board to the cabinet shelf.

Remove two screws that secure the top of the picture tube clamp bracket to the top inside front rail of the cabinet. Slacken off the two screws on the antenna bracket. Slide the bracket toward the rear of the cabinet in its guide grooves and remove the bracket from the cabinet.

The chassis and picture tube may then be withdrawn from the cabinet.

## DISMANTLING

CHASSIS TYPE PK IN CABINETS 96 AND 99

## REMOVAL OF CABINET

Remove the cabinet back by undoing the seven securing screws.

Disconnect the tuner lead from the antenna bracket by withdrawing the lead pins from the antenna socket.

Disconnect the speaker leads.
Pull off the four small knobs from the front of the receiver. Undo the grub screw on the contrast spindle and remove the brass collar. Pull off both the Channel Selector and Fine Tuning knobs.

Remove the two screws that secure the top of the picture tube clamp to the cabinet.

Remove six screws that secure the cabinet to the wooden base board.

Remove the cabinet.

## REMOVAL OF PICTURE TUBE SCREEN

Once the cabinet has been removed, the front screen may be removed by undoing the four corner screws.

The clear, protective picture tube screen and plastic-moulded front may be cleaned with a soft, damp cloth, but avoid the use of chemical and abrasive cleaners. Do not use any preparation normally sold as window cleaning or furniture polishing agents, as these generally prove harmful to those materials.

If the plastic becomes scratched or accidentally marked by a fly-spray, the marks may be removed by polishing gently with a soft cloth moistened with Wattyl or Dupol Cabinet Burnisher. Very deep scratches should be removed first with Water Rubbing Compound and then finished off with Burnisher.

## DEFLECTION YOKE

First remove the picture tube socket. Loosen the clamp-fixing screws on the rear of the yoke assembly, remove the yoke plug from the socket on the rear of the EHT assembly and slide yoke over neck of tube. When replacing yoke, do not use force and do not tighten clamping screws until set has been operated and picture is squared up.

## REMOVAL OF PICTURE TUBE

Having removed the chassis and picture tube assembly, remove the spring which rests against the aquadag coating on the rear of the picture tube. Slacken the nut at the side of the tube, securing the retaining strap and ease the tube out carefully, meanwhile supporting it around the mounting ring. In the case of bonded face tubes, the rubber mounts may be eased over the ears at the tube face corners and then the tube may be carefully withdrawn from the strap.

Note: The tubes are heavy and particular care in handling is necessary. It is recommended that protective goggles, apron and gloves be worn by personnel handling picture tubes to prevent personal injury should an implosion occur due to mishandling. The picture tube should be carefully handled and never placed face-down on a bench. Always ensure that it is placed on a soft, clean surface, such as felt, so that the face does not become scratched. Whenever possible, keep tubes in the original manufacturers' carton.

During the course of production of these receivers, the Company reserves the right, without notice, to make any modifications or improvements in design which may be necessary to meet prevailing conditions.

Information concerning changes, which are likely to be of benefit to retailers and servicemen, will be notified as far as possible by issuing a Technical Data Sheet.

Any further service information may be obtained by addressing an inquiry to "The Service Division", E.M.I. (Australia) Limited, 575-577 Parramatta Road, Leichhardt (Tel. LM 0291).

## ADJUSTMENTS

## HORIZONTAL LINEARITY

A typical multimeter employing a 100 ohm 1 mA fullscale deflection meter, when on 100 mA range, has a total resistance of 1 ohm . If such a meter is connected from pin 8 of the Horizontal Output valve to earth, i.e., across the 1 ohm metering resistor, it will indicate half of the current flowing in the cathode of the valve. The Horizontal Linearity control should be adjusted to reduce this current to a minimum.

## HORIZONTAL HOLD

Disconnect sync. pulses by removing the sync.
separator valve, V7, 6CS6. Short circuit the Horizontal Stablising coil. Adjust the Horizontal hold control so that the picture "floats" or locks weakly. Remove the short across the stabilising coil and adjust the core of this coil so that the picture again floats or locks weakly. Replace the sync. separator valve.

## CONTRAST RANGE

Turn the Contrast Control to its maximum clockwise position and adjust the Contrast Range control to give sync. tips at 190 volts at the Video anode, read on a DC coupled oscilloscope.


Fig. 2.


REAR VIEW 15-VALVE CHASSIS


REAR VIEW 16-VALVE CHASSIS

## ALIGNMENT

VISION I.F.
To align the vision IF a sweep generator and a marker generator, both covering the range 28.5 to $38.5 \mathrm{Mc} / \mathrm{s}$ are required, together with a display unit. The marker generator may be a signal generator and the display unit a C.R.O. These instruments should be interconnected as described in the instructions supplied with the sweep generator. The sweep generator should be terminated with a resistor equal to its output impedance and connected to the receiver as shown in Figure 3.


Fig. 3.
Coils L25, L28 and L29 adjust the bandwidth of the coupling circuits and are adjusted and sealed in the factory. It should only be necessary to adjust these on realignment if IF transformers or coils have been replaced in the circuit.

Before commencing alignment, remove slugs from L22, L24 and L27 and screw the slugs of IFT1 and IFT2 to sit flush with the chassis.

Connect a bias supply of - 6 volts across the IF A.G.C. Connect the display unit across R36. Throughout the alignment the display unit should be adjusted to present a reasonable amplitude display from a signal 2.5 volts peak-to-peak, and the output from the IF strip should be maintained at that level by varying the output from the sweep generator.

Because of the high gain of the receivers, care should be taken to ensure that all components replaced are on short leads and are placed in exactly the same position as the original part. Care must also be taken to prevent feedback in
interconnecting leads of alignment equipment.
The following procedure must be followed step by step, and do not proceed to the next step until sure that each response has been accurately obtained.
(1) Connect the sweep via input as in 3 to pin 2 of V5. Adjust the slugs in IFT3 (slug in position nearest the chassis) and L30 (slug in position farthest from chassis) to achieve a response as shown in Fig. 5A.
(2) Remove sweep from V5 pin 2 and using the same terminating pad, connect to pin 2 of V4. Adjust the slugs of IFT2 (slug in position nearest chassis) and L26 to achieve the response shown in Fig. 5 в.
(3) Remove the sweep from V4 and connect, through the same terminating pad, to V3 pin 2. Adjust the response, with the slugs of IFT1 (slug nearest chassis) and L23 (slug nearest chassis) to that shown in Fig. 5c..
(4) Remove the sweep from V3 and connect to the tuner through Test Point 1, (I.F. alignment) using the same terminating pad with probe. Adjust L21 (with slug nearest chassis) and L10 to produce final response as shown by Fig. 5d.
Note: The correct final response will be obtained only if each stage is accurately aligned. It may therefore be necessary to slightly readjust coils other than L21 and L10, on the final alignment, to produce the response shown in Fig. 5d, exactly.
(5) Insert slugs with retaining rubber, into L22, L24 and L27. Set L22 to 31.375 $\mathrm{Mc} / \mathrm{s}$., L24 to $29.875 \mathrm{Mc} / \mathrm{s}$., and L27 to $38.375 \mathrm{Mc} / \mathrm{s}$. (Fig. 5d).
(6) Check overall response and adjust if necessary. Also, check stability by removing the bias and adjusting the input accordingly. The response should remain substantially unchanged.

## SOUND I.F. ALIGNMENT

The following equipment is necessary to carry out this precdure:
(i) A C.W. Oscillator accurately tuned to $5.5 \mathrm{Mc} / \mathrm{s}$ by a crystal controlled reference.
(ii) A $20,000 \mathrm{ohm} /$ volt meter (Model 8, AVO or similar type).
(iii) A DC V.T.V.M.
(iv) A peak-to-peak detector as shown.


Fig 4: Peak-to-Peak Detector.

## $5.5 \mathrm{Mc} / \mathrm{s}$ NULL TRAP (IFT4)

IFT4 is a combined null trap and transformer, working at $5.5 \mathrm{Mc} / \mathrm{s}$. When tuned in the factory, both primary and secondary cores are tuned together to give a zero output at $5.5 \mathrm{Mc} / \mathrm{s}$. at the video grid, and a maximum transfer to the intercarrier amplifier. This can only be done accurately with a sweep oscillator and a suitable display having a high gain at $5.5 \mathrm{Mc} / \mathrm{s}$. Once set, however, it should not need re-tuning unless quite large circuit alterations have been made.

Should it be necessary to re-tune IFT4, the following procedure should be adopted:
(1) Inject $5.5 \mathrm{Mc} / \mathrm{s}$. at approximately 100 mV between the junction L 31 and L32 and earth (disconnecting the grid peaking choke, L31).
(2) Connect the input of the peak-to-peak detector illustrated (Fig. 4) to CRT cathode, pin 7. Connect the output of the peak-to-peak detector to a 20,000 ohm/volt meter on the 50 micro-amp range.
(3) Adjust primary core of IFT4 (nearest chassis) to give zero reading on meter. If IFT4 is replaced, it is necessary to adjust both cores to give a zero reading at $5.5 \mathrm{Mc} / \mathrm{s}$.
(4) Withdraw both cores from former. Screw in primary core (nearest chassis) to give a minimum reading.
(5) Screw in secondary core until meter reading rises slightly and then adjust primary core until a new minimum is obtained.
(6) Repeat adjustment of primary and secondary cores until meter reads zero.

## SOUND IF AMPLIFIER (IFT5)

With the oscillator connected as in (1) above and a VTVM connected across R97, adjust both primary and secondary cores in IFT5 for maximum response (Negative). This adjustment may be carried out using an "air" signal substituting for the oscillator.

## RATIO DETECTOR TRANSFORMER (IFT6)

With the oscillator connected as above, adjust the secondary core (nearest chassis) so that a positive or negative reading is obtained on a DC VTVM connected between the junction of the diode load resistors and earth. Adjust the primary (top of coil) so that this reading shows a maximum. Then adjust the secondary core so that this reading is zero volts. This adjustment may also be carried out using an "air" signal as previously.

# PICTURE TUBE REPLACEMENT 




Fig. 5.

RESISTORS

| REF． | PART No． | DESCRIPTION | REF． | PART No． | DESCRIPTION |
| :---: | :---: | :---: | :---: | :---: | :---: |
| R21 | 740－0302 | 1.8 K ohms $\pm 10 \%$ 䂞 W ． | R89 | 740－0252 | 1.5 K ohms $\pm 10 \% \frac{1}{2} \mathrm{~W}$ ． |
| R22 | 740－0032 | 2.2 K ohms $\pm 10 \%$ 年 W ． | R90 | 740－0082 | 10 K ohms $\pm 10 \%$ 交 W ． |
| R23 | 740－0482 | 56 ohms $\pm \frac{10 \%}{10} \frac{1}{2}$ W． | R91 | 740－0112 | 27 K ohms $\pm 10 \% \frac{1}{2} \mathrm{~W}$ ． |
| R24 | 740－0653 | 100 ohms $\pm 10 \% \frac{1}{2}$ W．Morganite | R92 | 740－0242 | 33 K ohms $\pm 10 \% \frac{1}{2} \mathrm{~W}$ ． |
| R24a | 742－0712 | 2.2 K ohms $\pm 20 \% 1 \mathrm{~W}$ ． | R93 | 740－0273 | 150 ohms $\pm 10 \%$－${ }^{\frac{1}{2} \text { W．Morganite }}$ |
| R25 | 740－0702 | 56 K ohms $\pm 10 \%$ 岩 W ． | R94 | 740－0572 | 1 K ohms $\pm 20 \% \frac{1}{2} \mathrm{~W}$ ． |
| R26 | 740－0062 | 3.9 K ohms $\pm 10 \%$ 䂞 W ． | R95 | 740－0142 | 100 K ohms $\pm 10 \%{ }^{\frac{1}{2}} \mathrm{~W}$ ． |
| R27 | 740－0273 | 150 ohms $\pm 10 \%$－${ }^{\frac{1}{2} \text { W．Morganite }}$ | R96 | 740－0242 | 33 K ohms $\pm 10 \%$ 交 W ． |
| R28 | 742－0712 | $2.2 \mathrm{~K} \mathrm{ohms} \pm 20 \% 1 \mathrm{~W}$ ． | R97 | 740－0082 | 10 K ohms $\pm 10 \% \frac{1}{2} \mathrm{~W}$ ． |
| R29 | 740－0062 | 3.9 K ohms $\pm 10 \% \frac{1}{2} \mathrm{~W}$ ． | R98 | 749－0052 | 47 K ohms $\pm 20 \% 2 \mathrm{~W}$ ． |
| R30 | 740－0273 | 150 ohms $\pm 10 \% \frac{1}{2} \mathrm{~W}$ ．Morganite | R99 | 740－0032 | 2.2 K ohms $\pm 10 \% \frac{1}{2} \mathrm{~W}$ ． |
| R31 | 742－1012 | 3.3 K ohms $\pm 20 \% 1 \mathrm{~W}$ ． | R99a | 740－0022 | 1 K ohms $\pm 10 \% \frac{1}{2} \mathrm{~W}$ ． |
| R32 | 740－0292 | 270 ohms $\pm 10 \% \frac{1}{2} \mathrm{~W}$ ． | R100 | 740－0062 | 3.9 K ohms $\pm 10 \% \frac{1}{2} \mathrm{~W}$ ． |
| R33 | 742－1012 | 3.3 K ohms $\pm 20 \% 1 \mathrm{~W}$ ． | R101 | 740－0112 | 27 K ohms $\pm 10 \% \frac{1}{2} \mathrm{~W}$ ． |
| R34 | 740－0792 | 8.2 K ohms $\pm 10 \%$ 在 W ． | R102 | 740－0112 | 27 K ohms $\pm 10 \% \frac{1}{2} \mathrm{~W}$ ． |
| R35 | 740－0242 | 33 K ohms $\pm 10 \%$ 在 W ． | R103 | 740－0122 | 47 K ohms $\ddagger 10 \%$ 立 W ． |
| R36 | 740－0043 | 2.7 K ohms $\pm 10 \%$－$\frac{1}{2} \mathrm{~W}$ ．Morganite | R104 | 740－0082 | 10 K ohms $\pm 10 \% \frac{1}{2} \mathrm{~W}$ ． |
| R37 | 740－0022 | 1 K ohms $\pm 10 \% \frac{1}{2} \mathrm{~W}$ ． | R105 | 740－0082 | 10 K ohms $\pm 10 \% \frac{1}{2} \mathrm{~W}$ ． |
| R38 | 750－0472 | 3.6 K ohms $\pm 5 \% 4 \mathrm{~W}$ ．Metox | R106 | 740－0152 | 150 K ohms $\pm 10 \%$ 古 W ． |
| R39 | 740－0653 | 100 ohms $\pm 10 \%$ 年 W ．Morganite | R107 | 740－0152 | 150 K ohms $\pm 10 \%$ 这 W ． |
| R40 | 740－0622 | 470 K ohms $\pm 20 \% \frac{1}{2} \mathrm{~W}$ ． | R108 | 740－0702 | 56 K ohms $\pm 10 \% \frac{1}{2} \mathrm{~W}$ ． |
| R41 | 740－0732 | 12 K ohms $\pm 10 \%$ 古 W ． | R109 | 740－0092 | 15 K ohms $\pm 10 \% \frac{1}{2} \mathrm{~W}$ ． |
| R42 | 740－0142 | 100 K ohms $\pm 10 \%$ 直 W ． | R110 | 742－0132 | 220 K ohms $\pm 10 \% 1 \mathrm{~W}$ ． |
| R43 | 742－0132 | 220 K ohms $\pm 10 \% 1 \mathrm{~W}$ ． | R111 | 740－0052 | 3.3 K ohms $\pm 10 \%$ 䂞 W ． |
| R44 | 742－0162 | 390 K ohms $\pm 10 \% 1 \mathrm{~W}$ ． | R112 | 740－0292 | 270 ohms $\pm 10 \%$ 䨖 W． |
| R45 | 742－0712 | 2.2 K ohms $\pm 20 \% 1 \mathrm{~W}$ ． | R113 | 740－1052 | 330 K ohms $\pm 20 \% \frac{1}{2} \mathrm{~W}$ ． |
| R45a | 750－0541 | 2.7 ohms special wire wound | R114 | 740－1062 | 680 K ohms $\pm 20 \%$ 立 W． |
| R46 | 750－0291 | $250 \mathrm{ohms} \pm 5 \% 5 \mathrm{~W}$ ．Cemcoat | R115 | $740-0052$ | 3.3 K ohms $\pm 10 \%$ 年 ${ }^{\frac{1}{2}} \mathrm{~W}$ ． |
| R47 | 749－0142 | 1 K ohms $\pm 20 \% 2 \mathrm{~W}$ ． | R116 | 750－0532 | $470 \mathrm{ohms} \pm 10 \% 5 \mathrm{~W} . \mathrm{PW} 5$. |
| R48 | 749－0252 | 12 K ohms $\pm 10 \% 2 \mathrm{~W}$ ． | R117 | 740－0082 | 10 K ohms $\pm 10 \%$ 在 W ． |
| R49 | 740－0112 | 27 K ohms $\pm 10 \%$ 霛 W ． | R118 | 740－0663 | 82 ohms $\pm 10 \%$ 㖘 W．Morganite |
| R50 | 740－0653 | 100 ohms $\pm 10 \%$ 在 W．Morganite | R119 | 742－0112 | 100 K ohms $\pm 10 \% 1 \mathrm{~W}$ ． |
| R51 | 740－0582 | 47 K ohms $\pm 20 \% \frac{1}{2} \mathrm{~W}$ ． | R120 | 740－0112 | 27 K ohms $\pm 10 \% \frac{1}{2} \mathrm{~W}$ ． |
| R5 2 | 740－0022 | 1 K ohms $\pm 10 \%$ 年 ${ }^{\frac{2}{2}} \mathrm{~W}$ ． | R121 | 740－0082 | 10 K ohms $\pm 10 \%$ 立 W． |
| R53 | 742－1043 | 220 ohms $\pm 10 \% 1 \mathrm{~W}$ ． | R122 | 740－0082 | 10 K ohms $\pm 10 \%$ W． |
| R54 | 740－1062 | 680 K ohms $\pm 20 \%$ 年 ${ }^{\frac{1}{2}} \mathrm{~W}$ ． | R123 | 740－0122 | 47 K ohms $\pm 10 \%$ 年 W ． |
| R55 | 740－0542 | 150 K ohms $\pm 20 \%$ 年 W ． | R124 | 740－0082 | 10 K ohms $\pm 10 \%{ }^{\frac{1}{2}} \mathrm{~W}$ ． |
| R56 | 740－0542 | 150 K ohms $\pm 20 \% \frac{1}{2} \mathrm{~W}$ ． | R125 | 742－0172 | 470 K ohms $\pm 10 \% 1 \mathrm{~W}$ ． |
| R57 | 740－1052 | 330 K ohms $\pm 20 \%$－ | R126 | 740－0082 | 10 K ohms $\pm 10 \%$ 交 W ． |
| R58 | 740－0532 | 1 M ohms $\pm 20 \% \frac{1}{2} \mathrm{~W}$ ． | R127 | 740－0232 | 39 K ohms $\pm 10 \% \frac{\frac{1}{2}}{} \mathbf{W}$ ． |
| R59 | 742－0412 | 100 K ohms $\pm 20 \% 1 \mathrm{~W}$ ． | R128 | 742－0022 | 4.7 K ohms $\pm 10 \% 1 \mathrm{~W}$ ． |
| R60 | 740－0022 | 1 K ohms $\pm 10 \%$ 茬 W ． | R129 | 740－0202 | 2.2 M ohms $\pm 10 \%$ 冎 W ． |
| R61 | 742－0092 | 47 K ohms $\pm 10 \% 1 \mathrm{~W}$ ． | R130 | 740－0582 | 47 K ohms $\pm 20 \%$ 老 W ． |
| R62 | 740－0522 | $82 \mathrm{ohms} \pm 10 \% 5 \mathrm{~W}$. PW 5. | R131 | 740－0302 | 1.8 K ohms $\pm 10 \% \frac{1}{2} \mathrm{~W}$ ． |
| R63 | 742－0342 | 330 K ohms $\pm 20 \% 1 \mathrm{~W}$ ． | R132 | 750－0482 | 1 K ohms $\pm 5 \% 4 \mathrm{~W}$ ．Metox |
| R63a | 740－0142 | 100 K ohms $\pm 10 \%$ 直 W． | R133 | 742－0823 | 270 ohms $\pm 10 \% 1 \mathrm{~W}$ ．Morganite |
| R64 | 740－0162 | 220 K ohms $\pm 10 \% \frac{1}{2} \mathrm{~W}$ ． | R134 | 740－1043 | 27 ohms $\pm 10 \%$ 寺 W．Morganite |
| R65 | 740－0162 | 220 K ohms $\pm 10 \%$－${ }^{\frac{1}{2} \mathrm{~W}}$ ． | R135 | 740－1043 | 27 ohms $\pm 10 \%$ W Morganite |
| R66 | 740－0242 | 33 K ohms $\pm 10 \%{ }^{\frac{1}{2}} \mathrm{~W}$ ． | R136 | 740－0172 | 270 K ohms $\pm 10 \% \frac{1}{2} \mathrm{~W}$ ． |
| R67 | 740－0162 | 220 K ohms $\pm 10 \% \frac{1}{2} \mathrm{~W}$ ． | R137 | 740－0392 | 330 K ohms $\pm 10 \% \frac{1}{2} \mathrm{~W}$ ． |
| R68 | 740－0822 | 33 K ohms $\pm 20 \%$ 者 W ． | R138 | 740－0043 | 2.7 K ohms $\pm 10 \%{ }^{\frac{1}{2}} \mathrm{~W}$ W．Morganite |
| R69 | 740－0122 | 47 K ohms $\pm 10 \% \frac{1}{2} \mathrm{~W}$ ． | R139 | 740－0182 | 470 K ohms $\pm 10 \% \frac{1}{2} \mathrm{~W}$ ． |
| R70 | 740－0112 | 27 K ohms $\pm 10 \%$ 䢒 W． | R140 | 740－0142 | 100 K ohms $\pm 10 \% \frac{1}{2} \mathrm{~W}$ ． |
| R71 | 742－0772 | 3.9 M ohms $\pm 10 \% 1 \mathrm{~W}$ ． | R141 | 740－0102 | 22 K ohms $\pm 10 \%$ 年 W ． |
| R72 | 740－0202 | 2.2 M ohms $\pm 10 \%$ 古 W ． | R142 | 742－0042 | 15 K ohms $\pm 10 \% 1 \mathrm{~W}$ ． |
| R73 | 742－0102 | 82 K ohms $\pm 10 \% 1 \mathrm{~W}$ ． | R143 | 742－0472 | 1.8 K ohms $\pm 10 \% 1 \mathrm{~W}$ ． |
| R74 | 749－0022 | 15 K ohms $\pm 10 \% 2 \mathrm{~W}$. | R144 | 740－0702 | 56 K ohms $\pm 10 \% \frac{1}{2} \mathrm{~W}$ ． |
| R75 | 742－0052 | 22 K ohms $\pm 10 \% 1 \mathrm{~W}$ ． | R145 | 740－0112 | 27 K ohms $\pm 10 \%$ 交 W ． |
| R76 | 742－0172 | 470 K ohms $\pm 10 \% 1 \mathrm{~W}$ ． | R146 | 742－0092 | 47 K ohms $\pm 10 \% 1 \mathrm{~W}$. |
| R77 | 742－0772 | 3.9 M ohms $\pm 10 \% 1 \mathrm{~W}$ ． | R147 | 742－0172 | 470 ohms $\pm 10 \% 1 \mathrm{~W}$ ． |
| R78 | 742－0772 | 3.9 M ohms $\pm 10 \% 1 \mathrm{~W}$ ． | R148 | 740－0572 | 1 K ohms $\pm 20 \%$ 者 W ． |
| R79 | 742－0892 | 2.2 M ohms $\pm 10 \% 1 \mathrm{~W}$ ． | R149 | 750－0362 | 2.7 K ohms $+10 \% 5 \mathrm{~W}$. PW 5. |
| R80 | 742－0192 | 1 M ohms $\pm 10 \% 1 \mathrm{~W}$ ． | R150 | 746－0242 | $1 \mathrm{ohm} \pm 10 \% \mathrm{BW} \frac{1}{2}$ W／W． |
| R81 | 740－0502 | 15 K ohms $\pm 20 \%{ }^{\frac{1}{2}} \mathrm{~W}$ ． | R151 | 742－0262 | 2.7 K ohms $\pm 10 \% 1 \mathrm{~W}$ ． |
| R82 | 740－0782 | 120 K ohms $\pm 10 \%$ 交 W． | R152 | Part of |  |
| R83 | 740－0702 | 56 K ohms $\pm 10 \%{ }^{\frac{1}{2}} \mathrm{~W}$ ． |  | 908－0382 | 1.5 ohms wire resistor． |
| R84 | 740－0782 | 120 K ohms $\pm 10 \%$ 年 W ． | R153 | 742－0492 | 68 K ohms $\pm 10 \% 1 \mathrm{~W}$ ． |
| R85 | 740－0142 | 100 K ohms $\pm 10 \%$ 交 W ． | R154 | 742－0112 | 100 K ohms $\pm 10 \% 1 \mathrm{~W}$ ． |
| R86 | 740－0222 | 180 K ohms $\pm 10 \%$ 砏 W． | R155 | 740－0492 | 1.5 M ohms $\pm 20 \%$ 年 W ． |
| R87 | 749－0022 | 15 K ohms $\pm 10 \% 2 \mathrm{~W}$ ． | R156 | 740－0252 | 1.5 K ohms $\pm 10 \%$ 年 ${ }^{\frac{1}{2}} \mathrm{~W}$ ． |
| R88 | 740－0792 | $8.2 \mathrm{~K} \mathrm{ohms} \pm 10 \%$ \％ |  |  |  |

## CAPACITORS

| REF． | PART No． | DESCRIPTION | REF． | PART No． | DESCRIPTION |
| :---: | :---: | :---: | :---: | :---: | :---: |
| C21 | 273－0591 | $68 \mathrm{pF} . \pm 2 \frac{1}{2} \%$ Mica． | C31 | 271－0731 | ． $047 \mathrm{uF} .+80 \%-20 \%$ Disc |
| C22 | 271－0031 | .0033 uF．$+100 \%-0 \% 500 \mathrm{~V}$ ． Ceramic Disc | C32 | 271－0591 | B Red Cap． $.0027 \mathrm{uF} . \pm 20 \% \mathrm{~K} 2000$ Style |
| C23 | 271－0031 | ． $0033 \mathrm{uF} .+100 \%-0 \% 500 \mathrm{~V}$ ． |  |  | －Ceramic Disc． |
|  |  | Ceramic Disc． | C33 | 273－0591 | $68 \mathrm{pF} . \pm 2 \frac{1}{2} \% \mathrm{Mica}$ ． |
| C24 | 271－0031 | $.0033 \mathrm{uF} .+100 \%-0 \% 500 \mathrm{~V}$. Ceramic Disc． | C34 | 271－0031 | $\begin{aligned} & .0033 \mathrm{uF}+100 \%-0 \% 500 \mathrm{~V} \text {. } \\ & \text { Ceramic Disc. } \end{aligned}$ |
| C25 | 271－0031 | $\begin{aligned} & .0033 \mathrm{uF}+100 \%-0 \% 500 \mathrm{~V} . \\ & \text { Ceramic Disc. } \end{aligned}$ | C35 | 271－0731 | $\begin{aligned} & .047 \mathrm{uF}+80 \%-20 \% \text { Disc } \\ & \text { B Red Cap. } \end{aligned}$ |
| C26 | 271－0731 | $.047 \mathrm{uF}+80 \%-20 \% \text { Disc }$ <br> B Red Cap． | C36 | 271－0031 | $.0033 \mathrm{uF}+100 \%-0 \% 500 \mathrm{~V}$ <br> Ceramic Disc． |
| C27 | 271－0281 | $.022 \mathrm{uF}+100 \%-0 \% 100 \mathrm{~V}$ <br> Ceramic Disc． | C37 | 271－0591 | $.0027 \mathrm{uF} . \pm 20 \% \mathrm{~K} 2000$ Style Ceramic Disc． |
| C28 | 271－0591 | $.0027 \mathrm{uF} . \pm 20 \%$ K 2000 Style Ceramic Dise． | C38 | 271－0621 | 1000 pF ．Feed Thru Ducon <br> CAC 100 |
| C29 | 273－0591 | $68 \mathrm{pF} . \pm 2 \frac{1}{\mathrm{~L}} \% \mathrm{Mica}$ ． | C39 | 271－0121 | 5.6 pF ．$\pm \frac{1}{4} \mathrm{pF}$ ．Ceramic Tube NPO |
| C30 | 271－0031 | $.0033 \mathrm{uF} .+100 \%-0 \% 500 \mathrm{~V}$ ． Ceramic Disc． | C 40 C 41 | $271-0131$ $271-0181$ | 8.2 pF ．$\pm \mathrm{pF}$ ．Ceramic Tube NPO <br> $15 \mathrm{pF}, \pm \frac{1}{2} \mathrm{pF}$ ．Ceramic Tube NPO |

CAPACITORS - continued


COILS

| REF. | PART No. | DESCRIPTION | REF. | PART No. | DESCRIPTION |
| :---: | :---: | :---: | :---: | :---: | :---: |
| L21) | 1 | 1st I.F. Grid Coil $31.375 \mathrm{Mc} / \mathrm{s}$. | L31 | 259-0954 | Grid Peaking Choke |
| L22) | 1 | Trap | L32 | 259-0954 | Grid Peaking Choke |
| L23) | 259-1171 | 1st I.F. Anode Coil $29.875 \mathrm{Mc} / \mathrm{s}$ | L33 | 259-1082 | Peaking Coil, Shunt |
| L24) | 259-1171 | Trap | L34 | 259-1092 | Peaking Coil, Series |
| L25 | 259-0672 | 1st I.F. Coupling Coil | L35 | 259-0993 | Horizontal Stabiliser Coil |
| L26 ) |  | 2nd I.F. Anode Coil $38.375 \mathrm{Mc} / \mathrm{s}$ | L36 | 259-0044 | Anti-Parasitic Coil |
| L27) | 259-1181 | Trap | L37 | 259-0903 | Width Coil |
| L28 | 259-0672 | 2nd I.F. Coupling Coil | L38 | 259-0044 | Anti-Parasitic Coil |
| L29 | 259-0672 | 3 rd I.F. Coupling Coil | L39 | 259-0044 | Anti-Parasitic Coil |
| L30 | 259-0931 | Detector Input Coil | L40 | 259-0923 | Horizontal Linearity Coil |

POTENTIOMETERS

| REF. | PART No. | DESCRIPTION | REF. | PART No. | DESCRIPTION |
| :---: | :---: | :---: | :---: | :---: | :---: |
| RV1 | 677-0641 | 500 K ohms Curve A, Type Q Brightness | RV8 | 677-0921 | 50 K ohms Curve A, Type ECHeight |
| RV2 | 677-0171 | 25 K ohms Curve A, Type EC Noise Inverter | RV9 | 677-0641 | 500 K ohms Curve A, Type QVertical Hold |
| RV3 | 677-0911 | 1M ohms Curve A, Type EC A.G.C. | RV10 | 677-0511 | 10 K ohms Curve A, Type ECVertical Linearity |
| RV4 | 677-0601 | 25 K ohms Curve A, Type Q Contrast | RV11 | 677-0631 | 50 K ohms Curve A, Type PTUHorizontal Hold |
| RV5 | 677-0611 | 50 K Curve C, Type EC-Contrast Range | RV12 <br> RV13 | $\begin{aligned} & 677-0891 \\ & 677-0971 \end{aligned}$ | 2 Megohms $\pm 25 \%$ - Focus 1.5 K ohms CurveF, Hearing |
| RV6 | 677-1001 | 1M ohms Reversed C, Type PTU-Tone | RV14 | 677-0981 | Aid Volume <br> 250 K ohms Curve A, Remote |
| RV7 | 677-0621 | 1 M ohms Tapped 500 K Curve A with DPPP-Switch, Volume | RV15 | 677-1011 | Contrast <br> 250 K ohms Curve G, Remote Volume |

PARTS LIST ... MODELS PF, PG
TRANSFORMERS

| REF. | PART No. | DESCRIPTION | REF. | PART No. | DESCRIPTION |
| :---: | :---: | :---: | :---: | :---: | :---: |
| IFT1 | 906-0451 | Vision IFT | T3 | 908-0321 | Blocking Oscillator Transformer |
| IFT2 | 906-0451 | Vision IFT | T4 | 905-0226 | Vertical Output Transformer |
| IFT3 | 906-0252 | Vision IFT | T5 | 908-0352 | Vertical Feedback Transformer |
| IFT4 | 906-0263 | Vision IFT | T6 | 908-0382 | Horizontal Output Transformer |
| IFT5 | 906-0382 | Sound IFT | T7 | 908-0393 | Focus Transformer |
| IFT6 | 906-0323 | Ratio Discriminator Transformer | T8 | 904-0331 | Power Supply Transformer |
| T1 | 904-0254 | Mains Transformer | T9 | 908-0571 | Indexing Transformer |
| T2 | 905-0462 | Audio Output Transformer | T10 | 908-0571 | Indexing Transformer |
| VALVES |  |  |  |  |  |
| REF. | PART No. | DESCRIPTION | REF. | PART No. | DESCRIPTION |
| V1 | 932-1161 | 6ES8 - R.F. Amplifier | V10 | 932-1771 | 6GW8- Audio Driver and Output |
| V2 | 932-1921 | 6HG8 - Frequency Changer | V11 | 932-0511 | 6BM8- Blocking Oscillator and |
| V3 | 932-0881 | 6BY7 -- 1st I.F. Amplifier |  |  | Vertical Output |
| V4 | 932-0521 | $6 \mathrm{BX} 6-2 \mathrm{nd}$ I.F. Amplifier | V12 | 932-0481 | 12 AU 7 - Horizontal Multivibrator |
| V5 | 932-1221 | ${ }_{6} \mathrm{EJJ} 7-3 \mathrm{rd}$ I.F. Amplifier | V13 | 932-0531 | 6 CM 5 - Horizontal Output |
| V6 | 932-1081 | $6 \mathrm{DX8}$ - Video Amplifier and | V14 | 932-0771 | 1S2-EHT Rectifier |
|  |  | Noise Inverter des6 - Syncer | V15 | 932-1151 | 6 AL3 - Damping Diode |
| V 7 V8 | 932-1091 | ${ }^{6 C S 6}$ - Sync. Separator | V16 | 932-0501 | ${ }_{6} \mathrm{BL} 8$ - Remote Control |
| V8 | 932-1101 | 6U8- Sound T.F. Amplifier and | PLP | $\begin{aligned} & 932-1791 \\ & 932-1851 \end{aligned}$ | 12V. 2W. Philips, 12829 <br> 6V. 3W. Festoon Lamp, Philips, |
| V 9 | 932-0441 | 6AU6 - Limiter |  |  | 6849 or Lucas, 255 |

DIODES

| REF. | PART No. | DESCRIPTION | REF. | PART No. | DESCRIPTION |
| :---: | :---: | :---: | :---: | :---: | :---: |
| MR1 | 932-1541 | Diode OA80 | MR9 | 932-0791 | Diode OA81 |
| $\begin{aligned} & \text { MR2 } \\ & \text { MR3 } \end{aligned}$ | 932-1071 | Diode OA $210,1 \mathrm{~N} 1763$ or 1N2094 | MR10 ) | 932-1811 | Rectifier sTC Type B420-1-1. |
| MR4 | 932-0991 | Diode M3 | MR11) |  |  |
| MR5 ) | 932-0601 | Diodes 20A79 | MR12) |  |  |
| MR6 MR7 | 932-0791 | Diode OA 81 | MR13 ) MR14 | 932-1801 | Diode Type Q3/3. |
| MR8 | 932-0791 | Diode OA 81 | -R14 | 93-1801 | Diode Trpe $23 / 3$. |



RESISTORS

| REF． | PART No | DESCRIPTION | REF． | PART No． | DESCRIPTION |
| :---: | :---: | :---: | :---: | :---: | :---: |
| R21 | 740－0302 | 1.8 K ohms $\pm 10 \% \quad \frac{1}{2} \mathrm{~W}$ ． | R84 | 740－0062 | 3.9 K ohms $\pm 10 \%$ 年 W ． |
| R22 | 740－0032 | 2.2 K ohms $\pm 10 \% \frac{1}{2} \mathrm{~W}$ ． | R85 | 740－0112 | 27 K ohms $\pm 10 \% \frac{1}{2} \mathrm{~W}$ ． |
| R23 | 740－0482 | 56 ohms $\pm 10 \% \frac{1}{2} \mathrm{~W}$ ． | R86 | 740－0112 | 27 K ohms $\pm 10 \% \frac{1}{2} \mathrm{~W}$ ． |
| R24 | 740－0653 | 100 ohms $\pm 10 \%{ }^{\frac{1}{2}} \mathrm{~W}$ ，Morganite | R87 | 740－0122 | 47 K ohms $\pm 10 \%$ 交 W． |
| R24a | 742－0712 | 2.2 K ohms $\pm 20 \% 1 \mathrm{~W}$ ． | R88 | 740－0082 | 10 K ohms $\pm 10 \%$ \％ |
| R25 | $740-0702$ $740-0062$ |  | R89 R 90 | $740-0082$ $740-0152$ | 10 K ohms $\pm 10 \%$ ohms $\pm 10 \%$ ． |
| R26 <br> R 27 <br> 1 | $740-0062$ $740-0273$ | 3.9 K ohms $\pm 10 \%$ 150 ohms $\pm 10 \%$ $\frac{1}{2}$ W W | R90 R91 | $740-0152$ $740-0152$ | 150 K ohms 150 K ohms $\pm 10 \%$ $\pm 10 \%$ |
| R28 | 742－0712 | 2.2 K ohms $\pm 20 \% 1 \mathrm{~W}$ ． | R92 | 740－0702 | 56 K ohms $\pm 10 \%$ 这 ${ }^{\text {W }} \mathrm{W}$ ． |
| R29 | 740－0062 | 3.9 K ohms $\pm 10 \% \frac{1}{2} \mathrm{~W}$ ． | R93 | 740－0092 | 15 K ohms $\pm 10 \% \frac{1}{2} \mathrm{~W}$ ． |
| R30 | 740－0273 | $150 \mathrm{ohms} \pm 10 \% \frac{1}{2} \mathrm{~W}$ ．Morganite | R94 | 742－0132 | 220 K ohms $\pm 10 \% 1 \mathrm{~W}$ ． |
| R31 | 740－1012 | $3.3 \mathrm{Kohms} \pm 20 \% 1 \mathrm{~W}$ ． | R95 | 740－0052 | 3.3 K ohms $\pm 10 \%$ 年 W ． |
| R32 | 740－0292 | 270 ohms $\pm 10 \% \frac{1}{2} \mathrm{~W}$ ． | R96 | 740－0292 |  |
| R33 | 742－1012 | 3.3 K ohms $\pm 20 \% 1 \mathrm{~W}$ ． | R97 | 740－1052 | 330 K ohms $\pm 20 \% \frac{1}{2} \mathrm{~W}$ ． |
| R34 | 740－0792 | 8.2 K ohms $\pm 10 \%$ 年 $\frac{\mathrm{W}}{}$ W． | R98 | 740－1062 | 680 K ohms $\pm 20 \% \frac{1}{2} \mathrm{~W}$ ． |
| R35 | 740－0242 | 33 K ohms $\pm 10 \%$ 宕 W ． | R99 | 740－0052 | 3.3 K ohms $\pm 10 \%$ 年 ${ }^{2} \mathrm{~W}$ ． |
| R36 R37 | $740-0043$ $740-0022$ | 2.7 K ohms $\pm 10 \%$ 1 K ohms $\pm 10 \%$ | ${ }_{\text {R100 }}$ | 750－0532 | $470 \mathrm{ohms} \pm 10 \% 5 \mathrm{~W}$. PW5 |
| R38 | 750－0472 | 3.6 K ohms $\pm 5 \%{ }^{4} \mathrm{~W}$ ．Metox | R102 | $740-0663$ $742-0112$ | 82 ohms $\pm 10 \% \frac{1}{2} \mathrm{~W}$ ．Morganit 100 K ohms $+10 \% 1 \mathrm{~W}$ ． |
| R39 | 740－0653 | 100 ohms $\pm 10 \%$ 曾 W．Morganite | R103 | 740－0112 | 27 K ohms $\pm 10 \%$－ 12 W ． |
| R40 | 740－0622 | 470 K ohms $\pm 20 \% \frac{1}{2} \mathrm{~W}$ ． | R104 | 740－0082 | 10 K ohms $\pm 10 \% \frac{1}{2} \mathrm{~W}$ ． |
| R41 | 740－0732 | 12 K ohms $\pm 10 \%{ }^{\frac{1}{2}} \mathrm{~W}$ ． | R105 | $740-0082$ | 10 K ohms $\pm 10 \% \frac{1}{2} \mathrm{~W}$ ． |
| R42 | 740－0142 | 100 K ohms $\pm 10 \%$ 年 | R106 | 740－0122 | 47 K ohms $\pm 10 \% \frac{1}{2} \mathrm{~W}$ ． |
| R43 R44 | $742-0162$ $740-0122$ | 390 K ohms $\pm 10 \% 1 \mathrm{~W}$. | R107 | 740－0082 | 10 K ohms $\pm 10 \% \frac{1}{2} \mathrm{~W}$ ． |
| R45 | 750－0541 | 2.7 ohms Special Wire Wound | R108 | 742－0172 | 470 K ohms $\pm 10 \% 1 \mathrm{~W}$ ． |
| R46 | 750－0291 | 250 ohms $\pm 5 \% 5 \mathrm{~W}$ ．Cemcoat | R109 R110 | 740－0082 | 10 K ohms $\pm 10 \%$ 12 ${ }^{\frac{1}{2}} \mathbf{W}$ ． |
| R47 | 749－0142 | 1 K ohms $\pm 20 \% 2 \mathrm{~W}$ ． | R111 | 740－02022 | 39 K ohms $\pm 10 \%$ ¹ $\frac{1}{} \mathrm{~W}$ ． |
| R48 | 740－0252 | 12 K ohms $\pm 10 \% 2 \mathrm{~W}$ ． | R111 | $742-0022$ | 4.7 K ohms $\pm 10 \% 1 \mathrm{~W}$ ． |
| R49 | 740－0112 | $27 \mathrm{~K} \mathrm{ohms} \pm 10 \%$ 年 W ． | R113 | 740－0582 | 47 K ohms $\pm 20 \%{ }^{2}$ |
| R50 | 740－0142 | 100 K ohms $\pm 10 \% \frac{1}{2} \mathrm{~W}$ ． | R114 | $740-0302$ | 1.8 K ohms $\pm 10 \%{ }^{2} \mathrm{~L}$ W． |
| R51 | 740－0162 | 220 K ohms $\pm 10 \% ~ \frac{1}{2} \mathrm{~W}$ ． | R115 | 750－0482 | 1 K ohms $\pm 5 \% 4 \mathrm{~W}$ ．Metox |
| R52 | $740-0162$ $740-0242$ |  | R116 | $742-0823$ | 270 ohms $\pm 10 \% 1 \mathrm{~W}$ ．Morganite |
| R53 R 54 | $740-0242$ $740-0162$ | 33 K ohms $\pm 10 \%{ }^{\frac{1}{2}} \mathrm{~W}$ ． 220 K ohms $\pm 10 \%$ | R117 | 740－1043 | 27 ohms $\pm 10 \%$ 年 ${ }^{\text {d }}$ W．Morganite |
| R55 | 740－0822 | 33 K ohms $\pm 20 \%{ }^{\frac{1}{2}} \mathrm{~W}$ ． | R118 | 740－1043 | $27 \mathrm{ohms} \pm 10 \%$ 年 ${ }^{\frac{1}{2}} \mathrm{~W}$ ．Morganite |
| R56 | 740－0122 | 47 K ohms $\pm 10 \%$ 年 W． | R119 R120 | $740-0172$ $740-0392$ | 270 K ohms $\pm 10 \%$ 年 $10 \%$ ． |
| R57 | 740－0112 | 27 K ohms $\pm 10 \%$ 㑑 W ． | R120 R 121 | $\begin{aligned} & 740-0392 \\ & 740-0043 \end{aligned}$ | ${ }_{2}^{330 \mathrm{~K}}$ ohms $\pm 10 \% \mathrm{~K}^{1} \mathrm{~K}$ W．Morganite |
| R58 | 742－0772 | 3.9 M ohms $\pm 10 \% 1 \mathrm{~W}$ ． | R122 | 740－0182 | $470 \mathrm{~K} \text { ohms } \pm 10 \% ~ \frac{1}{2} \mathrm{~W}$ |
| R59 | 740－0202 | $2.2 \mathrm{M} \mathrm{ohms} \pm 10 \%$ 宕 W． | R123 | 740－0142 | 100 K ohms $\pm 10 \%$ 年 10. |
| R60 | 742－0102 | 82 K ohms $\pm 10 \% 1 \mathrm{~W}$ ． | R124 | 740－0102 | 22 K ohms $\pm 10 \% \frac{1}{2}^{2} \mathrm{~W}$ ． |
| R61 | 749－0022 | 15 K ohms $\pm 10 \% 2 \mathrm{~W}$ ． | R125 | 742－0042 | 15 K ohms $\pm 10 \% 1 \mathrm{~W}$ ． |
| R62 | $742-0052$ $742-0172$ | 22 K ohms $\pm 10 \% 1 \mathrm{~W}$ | R126 | 742－0472 | 1.8 K ohms $\pm 10 \% 1 \mathrm{~W}$ ． |
| R63 | $742-0172$ $742-0772$ | 470 K ohms $\pm 10 \mathrm{M}$ ohms $10 \% 1 \mathrm{~W}$. | R127 | 740－0702 | 56 K ohms $\pm 10 \% \frac{1}{2} \mathrm{~W}$ ． |
| R65 | 742－0772 | 3.9 M ohms $\pm 10 \% 1 \mathrm{~W}$ ． | R128 | 740－0112 | 27 K ohms $\pm 10 \%$ 年 W． |
| R66 | 742－0892 | 2.2 M ohms $\pm 10 \% 1 \mathrm{~W}$ ． | R129 | 742－0092 | 47 K ohms $\pm 10 \% 1 \mathrm{~W}$ ． |
| R67 | 742－0192 | 1 M ohms $\pm 10 \% 1 \mathrm{~W}$ ． | R130 | 742－0172 | 470 K ohms $\pm 10 \% 1 \mathrm{~W}$ ． |
| R68 | 740－0502 | 15 K ohms $\pm 20 \%$ 交 W ． | R131 | 740－0572 | 1 K ohms $\pm 20 \%$ 年 ${ }^{2} \mathrm{~W}$ ． |
| R69 | $740-0782$ | 120 K ohms $\pm 10 \% \frac{1}{2} \mathrm{~W}$ ． | R132 R13 | 750－0362 | $1 \mathrm{ohm} \pm 10 \% \mathrm{BW}{ }^{\frac{1}{2}} \mathrm{~W} / \mathrm{W}$ |
| R70 | $740-0702$ $740-0782$ | 56 K ohms $\pm 10 \%$ 㿾 $\frac{\mathrm{W}}{}$ ． | R134 | 742－0262 | 2.7 K ohms $\pm 10 \% 1 \mathrm{~W}$ ． |
| R72 | $740-0782$ $749-0182$ | 120 K ohms $\pm 10 \%$ 年 ${ }^{\text {d }}$ W． 22 K ohms $\pm 10 \% 2 \mathrm{~W}$. | R135 | Part of |  |
| R73 | 740－0252 | 1.5 K ohms $\pm 10 \%$ 䂞 W ． |  | 908－0382 | 1.5 ohms Wire Resistor |
| R74 | 740－0082 | 10 K ohms $\pm 10 \%$ 年 $10 \%$ ． | R136 R137 | $\begin{aligned} & 742-0492 \\ & 742-0112 \end{aligned}$ | 68 K ohms $\pm 10 \% 1 \mathrm{~W}$ ． 100 K ohms $\pm 10 \% 1 \mathrm{~W}$ ． |
| R75 | 740－0112 | 27 K ohms $\pm 10 \% \frac{1}{2} \mathrm{~W}$ ． | R138 | $740-0492$ | 1.5 M ohms $\pm 20 \% \frac{1}{2} \mathrm{~W}$ ． |
| R76 | 740－0242 | 33 K ohms $\pm 10 \%$ 年 W ． |  | ts list | chassis having Philips Deflection |
| R77 | 740－0273 | 150 ohms $\pm 10 \% \frac{1}{2} \mathrm{~W}$ ．Morganite | Above |  | hassis having Philips Deflection |
| R78 R79 | $740-0572$ | 1 K ohms $\pm 20 \%$ 䂞 W． | Wher | P Deflec | ponents are used，the following |
| R80 | 740－0242 |  |  | utions are |  |
| R81 | 740－0082 | 10 K ohms $\pm 10 \%$ 年 W ． | R139 | 742－0012 | 1.2 K ohms $\pm 10 \% 1 \mathrm{~W}$ ．for R134 |
| R82 | 742－0092 | 47 K ohms $\pm 10 \% 1 \mathrm{~W}$ ． | R140 | Part of |  |
| R83 | 740－0022 | 1 K ohms $\pm 10 \% \frac{1}{2} \mathrm{~W}$ ． |  | 908－0561 | 1.5 ohms Wire Resistor for R135 |
| CAPACITORS |  |  |  |  |  |
| REF． | PART No． | DESCRIPTION | REF． | PART No． | DESCRIPTION |
| C21 | 273－0591 | $\begin{aligned} & 68 \mathrm{pF} . \pm 2 \frac{1}{2} \% \text { Mica } \\ & .0033 \mathrm{uF}+100 \%-0 \% 500 \mathrm{~V} . \\ & \text { Ceramic Disc } \end{aligned}$ | C36 | 271－0031 | $.0033 \mathrm{uF}+100 \%-0 \% 500 \mathrm{~V}$ |
| C22 | 271－0031 |  | C37 | 271－0591 | $.0027 \mathrm{uF} . \pm 20 \%$ K2000 Style Ceramic Disc |
| C23 | 271－0031 | $.0033 \mathrm{uF}+100 \%-0 \% 500 \mathrm{v}$ |  |  |  |
|  |  | Ceramic Disc | C38 | 271－0621 | 1000 pF ．Feed Thru Ducon CAC 100 |
| C24 | 271－0031 | ． $0033 \mathrm{uF} .+100 \%-0 \% 500 \mathrm{~V}$ ． |  |  |  |
|  |  | Ceramic Disc | C39 | 271－0121 | $5.6 \mathrm{pF} . \pm \frac{1}{4} \mathrm{pF}$ ．Ceramic Tube NPO |
| C25 | 271－0031 | ． $0033 \mathrm{uF} .+100 \%-0 \% 500 \mathrm{~V}$ ． | C40 | 271－0131 | 8.2 pF ．$\pm \frac{1}{4} \mathrm{pF}$ ．Ceramic Tube NPO <br> 15 pF ．$\pm \frac{1}{2} \mathrm{pF}$ ．Ceramic Tube NPO |
|  |  | Ceramic Disc | C41 | 271－0181 |  |
| C26 | 271－0731 | $\begin{aligned} & .047 \mathrm{uF}+80 \%-20 \% \text { Disc 'B' } \\ & \text { Red Cap } \end{aligned}$ | $\mathrm{C} 42^{\mathrm{C} 4}{ }^{\text {d }}$ | $271-0691$ $271-0311$ | 3.9 pF ．$\pm \frac{1}{4} \mathrm{pF}$ ．Ceramic Disc NPO <br> $27 \mathrm{pF} . \pm 5 \%$ Ceramic Tube NPO |
| C27 | 271－0281 | $.022 \mathrm{uF} .+100 \%-0 \% 100 \mathrm{~V}$ ． | C44 | 279－1701 | $.047 \mathrm{uF} . \pm 20 \% 400$ V．W．Paper $.0022 \mathrm{uF} . \pm 10 \% 400 \mathrm{~V}$ ．Polyester |
|  |  | Ceramic Disc | C45 | 282－0541 |  |
| C28 | 271－0591 | ． $0027 \mathrm{uF} . \pm 20 \% \mathrm{~K} 2000$ Style | C46 | 282－0661 | $\begin{aligned} & .0022 \mathrm{uF} . \pm 10 \% 400 \mathrm{~V} \text {. Polyester } \\ & .022 \mathrm{uF} . \pm 10 \% 400 \mathrm{~V} \text {. Polyester } \\ & 8 \mathrm{uF} .300 \mathrm{~V} . \text { W. Electro Type ET2D } \end{aligned}$ |
|  |  | Ceramic Dise | C47 | 269－0211 |  |
| C29 | $\begin{aligned} & 273-0591 \\ & 271-0031 \end{aligned}$ | $68 \mathrm{pF} . \pm 2 \frac{1}{2} \% \mathrm{Mica}$ | C48 | 269－0521 | 100 uF． 150 V．W．Insulated Electro |
| C30 |  | $.0033 \mathrm{uF} .+100 \%-0 \% 500 \mathrm{~V}$ ． Ceramic Disc | C49 | 269－0521 | Type EMG1014 SFE <br> 100 uF． 150 V．W．Insulated Electro <br> Type EMG1014 SFE |
| C31 | 271－0731 | ． $047 \mathrm{uF} .+80 \%-20 \%$ Dise＇B＇ |  |  |  |
|  |  | Red Cap |  | 269－0511 | Type EMG1014 SFE <br> $80 \mathrm{uF} .+40$ uF． 300 V．W．Electro |
| C32 | 271－0591 | $.0027 \mathrm{uF} . \pm 20 \%$ K2000 Style | $\begin{aligned} & \mathrm{C} 51) \\ & \mathrm{C} 52 \end{aligned}$ | 271－0111 | Ducon Type EMC4830 1000 pF ．CDS Hi－K K1200 |
| C33 | $\begin{aligned} & 273-0591 \\ & 271-0031 \end{aligned}$ | 68 pF ．$\pm 2 \frac{1}{2} \%$ Mica |  |  | 1000 pF ．CDS Hi－K K1200 <br> Ceramic Disc |
| C34 |  | $\begin{aligned} & .0033 \text { uF. }+100 \%-0 \% 500 \mathrm{~V} . \\ & \text { Ceramic Disc } \end{aligned}$ | C53 | 271－0111 | ```1000 pF. CDS Hi-K K1200 Ceramic Disc .022 uF. \pm 10% 400 V.W. Paper 4 uF. 300 V.W. Electro Type ET2D``` |
| C35 | 271－0731 | ． 047 uF ．$+80 \%-20 \%$ Disc＇B＇ | C54 | 279－4661 |  |
|  |  | Red Cap | C55 | 269－0611 |  |

## PARTS LIST ... MODELS PH, PJ, PK

CAPACITORS - continued


COILS

| REF. | PART No. | DESCRIPTION | REF. | PART No. | DESCRIPTION |
| :---: | :---: | :---: | :---: | :---: | :---: |
| L21) | 259-1191 | 1st I.F. Grid Coil $31.375 \mathrm{Mc} / \mathrm{s}$. | L31 | 259-0954 | Grid Peaking Choke |
| L22) | 259-1191 | Trap | L32 | 259-0954 | Grid Peaking Choke |
| L23) | 259-1171 | 1st I.F. Anode Coil $29.875 \mathrm{Mc} / \mathrm{s}$. | L33 | 259-1082 | Peaking Coil-Shunt |
| L24) | 259-1171 | Trap | L34 | 259-1092 | Peaking Coil-Series |
| L25 | 259-0672 | 1st I.F. Coupling Coil | L35 | 259-0993 | Horizontal Stabliser Coil |
| L26 ) | 259-1181 | 2nd I.F. Anode Coil $38.375 \mathrm{Mc} / \mathrm{s}$. | L36 | 259-0044 | Anti-Parasitic Coil |
| L27 L28 | 259-0672 | 2nd Trap I.F. Coupling Coil | L37 L38 | 259-0903 | Width Coil Anti-Parasitic Coil |
| L29 | 259-0672 | 3 rd I.F. Coupling Coil | L39 | 259-0044 | Anti-Parasitic Coil |
| L30 | 259-0931 | Detector Input Coil | L40 | 259-0923 | Horizontal Linearity Coil |

POTENTIOMETERS

| REF. | PART No. | DESCRIPTION | REF. | PART No. | DESCRIPTION |
| :---: | :---: | :---: | :---: | :---: | :---: |
| RV1 | 677-0641 | 500 K ohms Curve A Type Q Brightness | RV7 | 677-0621 | 1 M ohm Tapped 500 K Curve A with DPPP-Switch, Volume |
| RV2 | 677-0171 | 25 K ohms Curve A Type EC Noise Inverter | RV8 | 677-0921 | 50 K ohms Curve A Type EC Height |
| RV3 | 677-0911 | 1M ohms Curve A Type EC - | RV9 | 677-0641 | 500 K ohms Curve A Type Q Vertical Hold |
| RV4 | 677-0601 | 25 K ohms Curve A Type Q Contrast | RV10 | 677-0511 | 10 K ohms Curve A Type EC Vertical Linearity |
| RV5 | 677-0611 | 50 K ohms Curve C Type EC Contrast Range | RV11 | 677-0631 | 50 K ohms Curve A Type PTU Horizontal Hold |
| RV6 | 677-1001 | 1M ohms Reversed C Type PTU Tone | RV12 | 677-0891 | 2 M ohms $\pm 25 \%$ - Focus |

TRANSFORMERS

| REF. | PART No. | DESCRIPTION | REF. | PART No. | DESCRIPTION |
| :---: | :---: | :---: | :---: | :---: | :---: |
| IFT1 | 906-0451 | Vision IF'T | T3 | 908-0321 | Blocking Oscillator Transformer |
| IFT2 | 906-0451 | Vision IF'T | T4 | 905-0226 | Vertical Output Transformer |
| IFT3 | 906-0252 | Vision IFT | T5 | 908-0355 | Vertical Feedback Transformer |
| IFT4 | 906-0263 | Vision IF'T | T6 | 908-0382 | Horizontal Output Transformer |
| IFT5 | 906-0382 | Sound IFT | or |  | Philips AT2016T/92 or NT3101 |
| IFT6 | 906-0323 | Ratio Discriminator Transformer | T6 | 908-0561 | Horizontal Output Transformer |
| T1 | 904-0254 | Mains Transformer |  |  | MSP 43211 |
| T2 | 905-0462 | Audio Output Transformer | T7 | 908-0393 | Focus Transformer |

PARTS LIST ... MODELS PH, PJ, PK
VALVES

| REF. | PART No. | DESCRIPTION | REF. | PART No. | DESCRIPTION |
| :---: | :---: | :---: | :---: | :---: | :---: |
| V1 | 932-1161 | 6ES8-R.F. Amplifier | V10 | 932-1771 | 6GW8-Audio Driver and Audio |
| V2 | 932-1921 | 6HG8-Frequency Changer |  |  | Output |
| V3 | 932-0881 | 6BY7-1st I.F. Amplifier | V11 | 932-0511 | 6BM8-Blocking Oscillator and |
| V 4 | 932-0521 | $6 \mathrm{BX} 6-2$ nd I.F Amplifier |  |  | Vertical Output |
| V5 | 932-1221 | $6 \mathrm{EJ} 7-3 \mathrm{~d}$ d I.F. Amplifier | V12 | 932-4811 | 12AU7-Horizontal Multivibrator |
| V6 | 932-1081 | $6 \mathrm{DX} 8-V i d e o$ Amplifier and Noise Inverter | $\begin{aligned} & \text { V13 } \\ & \text { V14 } \end{aligned}$ | $\begin{aligned} & 932-0531 \\ & 932-0771 \end{aligned}$ | 6CM5-Horizontal Output 1S2-E.H.T. Rectifier |
| V7 | 932-1091 | 6CS6-Sync, Separator | V15 | 932-1151 | 6AL3-Damping Diode |
| V8 | 932-1101 | 6U8-Sound I.F. Amplifier and AGC |  | 932-1851 | 6V. 3W. Festoon Lamp Philips |
| V9 | 932-0441 | 6AU6-Limiter |  |  | 6849 or Lucas, 255 |

DIODES

| REF. | PART No. | DESCRIPTION | REF. | PART No. | DESCRIPTION |
| :---: | :---: | :---: | :---: | :---: | :---: |
| MR1 | 932-1541 | $\begin{aligned} & 0 \mathrm{~A} 80 \\ & 0 \mathrm{~A} 210,1 \mathrm{~N} 1763 \text { or } 1 \mathrm{~N} 2094 \\ & \text { M3 } \end{aligned}$ | MR5 ) | 932-0601 |  |
| MR2 | 932-1071) |  | MR6 ) | 932-0601 | 20A79 |
| MR3 | 932-1071) |  | MR7 | 932-0791 | 0 A 81 |
| MR4 | 932-0991 |  | MR8 | 932-0791 | 0 A 81 |

MISGELLANEOUS

| REF. | PART No. | DESCRIPTION | REF. | PART No. | DESCRIPTION |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| CH1 | 232-0124 | Choke, 300 mA |  | 932-1261 |  | AW5 9-30-K |
| RT1 | 752-0061 | Brimister, CZ11 |  | 932-1261 | 23WP4 ) |  |
| VDR1 | 750-0281 | Voltage Dependent Resistor, Type E298GD/A260 (Blue Spot) |  | $932-1261$ $932-1261$ | $\begin{aligned} & 23 \mathrm{MP} 4-\mathrm{K} \\ & 2351 \mathrm{~B} \end{aligned}$ | PJ-PK |
| FS1 | 431-0071 | Fuse, 1 A. |  | 932-1261 | 23ARP4 ) | PJ-PK |
| FS2 | 431-0081 | Fuse, 1.5 A. |  | 932-1621 | AW59-90, |  |
| Fs3 | 431-0031 | Fuse, 250 mA . |  | 932-1621 | 23MP4-J ) |  |
| Yoke | 259-1051 | Philips AT1009T/93 or AT1009T/96 |  | 932-1621 | 2354 B ) |  |
| or | 259-1161 | MSP 42309 | Tuner | 224-1511 | Philips, NT3009 |  |
| CRT | $932-1591$ $932-1591$ | $\left.\begin{array}{l} 23 \mathrm{HP} 4 \\ 23 \mathrm{CRP} 4 \end{array}\right\} \quad \mathrm{PH}$ |  |  |  |  |

H. CLARK PTY. LTD.


TUNER TYPE NT3009

## " H.M.V " OHASSIS TYPE PF \& PG



TUNER TYPE NT3009

## " H.M.V " CHASSIS TYPE PH, PJ \& PK




