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# DIGITAL STORAGE OSCILLOSCOPE OS 1420

Instruction | Manual

For Service Manuals
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www.mauritron.co.uk TEL: 01844 - 351694 FAX: 01844 - 352554 Introduction Section 1

The Gould OS1420 provides a combination of Digital Storage and Real-time facilities, and caters for measurements from DC to 20MHz with a flicker-free display of a full cycle down to 0.002Hz. The digital method of storage provides many advantages, notably the facilities for pretrigger viewing and the ability to store a waveform indefinitely.

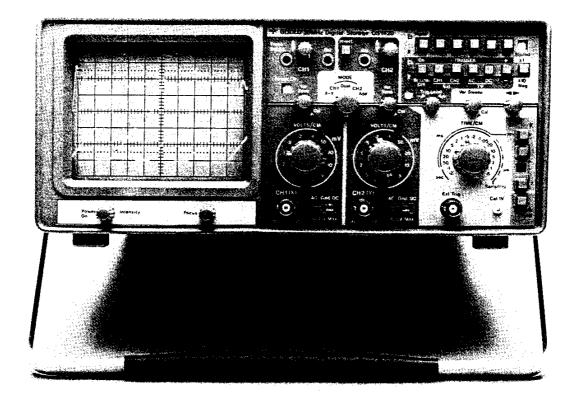
It features two identical input channels with a maximum sensitivity of 2mV/cm and a bandwidth from DC up to 20MHz. The channels may be displayed separately or together in both STORE and the conventional NORMAL modes. The ability to display the sum or difference of the channels and an X-Y mode operation are available in NORMAL mode. The timebase ranges from  $0.005\mu s/cm$  to 0.25/cm in NORMAL mode with additional ranges down to 50s/cm m STORE mode. A x 10 facility expands the upper limit to 50ns/cm. In NORMAL and certain of the STORE modes, inde-

pendent variable sensitivity and separate controls are provided.

The trigger facilities available are comprehensive, with DC and AC coupling available and a bright-line-free run facility to enable true location in the absence of a trigger. An active TV sync. separator is provided for viewing video waveforms.

Many additional facilities are provided with the OS1420 such as a plot option fitted as standard, a 1KHz calibrator, a DC coupled Z modulation input and a trace rotation control.

The instrument is readily portable and the use of an uncommitted logic array has reduced both the number of components and board area. This has additional benefits in terms of reliability, power consumption and ease of maintenance.



### Amendment for OS1420 Instruction Manual.

### Page 5

### Specification

Para. Trigger 'Sensitivity'
Amend as follows:-

Line 1 2mm to read 3mm

Line 3 2mm to read 3mm

Line 5 100mV to read 150mV

Line 6 400mV to read 600mV

Line 7 100mV to read 150mV

Line 8 400mV to read 600mV

Para. Display Modes.

Dual Trace

Line 3 0.2ns to read 0.2ms/cm

Line 5 0.2ns to read 0.2ms/cm

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Specification Section 2

DISPLAY

CRT 8 x 10cm rectangular mono-accelerator

EHT 2kV (Trace rotation by front panel preset).

#### **VERTICAL DEFLECTION**

Two identical input channels CH1 and CH2.

Bandwidth -3db

d.c. to 20MHz (2Hz to 20MHz on a.c.)

Sensitivity 2mV/cm to 10V/cm in 1-2-5 sequence.

Accuracy ±3%.

Variable Sensitivity >2-5:1 range allows continuous adjustment of sensitivity 2mV/cm to 25V/cm.

Input Impedance:  $1M\Omega/28pF$ . Input Coupling DC-GND-AC.

Input Protection 400V d.c. or pk a.c.

#### HORIZONTAL DEFLECTION

Normal Mode Sweep Rate  $0.5\mu s/cm$  to 0.2sec/cm, 18 ranges in 1-2-5 sequence

Accuracy ±3% (to 200ns/cm).

Variable Sweep >2.5:1 allows continuous coverage from  $0.5\mu$ s/cm to 0.5sec/cm.

Store Modes Sweep Rate  $0.5\mu s/cm$  to 50sec/cm, 25 ranges in 1-2-5 sequence.

Accuracy  $\pm 3\%$  (to 200ns/cm).

Variable Sweep >2.5:1 allows continuous coverage from 0.5µs/cm to 50µs/cm (sampling only).

X Expansion X10 push button gives fastest speed of 50ns/cm. Accuracy ±3% (50ns ±5%).

### TRIGGER

Variable level control with Bright Line ON/OFF facility. With Bright Line on, the timebase free-runs when insufficient signal (20Hz to 20MHz) is present or when the selected level is outside the range of the input signal.

Source Internal CH1 or CH2 External.

Slope Positive or negative.

Coupling DC, AC or TV (active sync separator with line/ frame selected by timebase switch between 50 and 100µs/cm).

Sensitivity Internal: DC coupled 2mm to 2MHz, 1cm to 20MHz.

AC coupled 2mm, 10Hz - 2MHz. 1cm, 4Hz - 20MHz.

External: DC coupled 100mV to 2MHz, 400mV to 20MHz.

AC coupled 100mV, 10Hz to 2MHz. 400mV, 4Hz to 20MHz.

External Input Impedance  $100k\Omega/10pF$  .

External Input Protection 250V d.c. or pk a.c.

### **DISPLAY MODES**

Single trace CH1 or CH2.

Dual trace In Normal, Chopped or Alternate Modes automatically selected by the timebase switch. Between 0.5µs/cm and 0.2ns/cm the Alternate Mode is selected whilst on ranges slower than 0.2ns/cm Chop Mode is selected. The chop frequency is 500kHz.

(In store modes simultaneous capture).

Add CH1 and CH2 added to give the algebraic sum of the two channel inputs (Normal mode only).

Invert CH2 CH2 may be inverted. When used in conjunction with Add mode it gives the algebraic difference of the two channels.

X-Y CH1 input gives X deflection and CH2 input gives Y deflection. (Normal mode only).

### ADDITIONAL FACILITIES

Calibrator 1V ±2% square wave at approx. 1kHz.

Z Mod Input DC coupled, 2V visible mod.

Sensitivity +40V cut off sensitivity. Input impedance  $10k\Omega/10pF$  approx. Maximum input 100V d.c. or pk a.c.

### **DIGITAL FACILITIES**

Store Size 1024 x 8-bits per channel.

Vertical Resolution 1 in 256 approx. 30 steps/cm.

Horizontal Resolution 1 in 1024 approx. 100 samples/cm. (0.05ms/cm range on Dual is 50 samples/cm).

**Expansion** X10 reduces the resolution by ten on all ranges.

Sample Rate: 2MHz (0.5 $\mu$ s) reducing in proportion with timebase.

Dot Joining Linear interpolation between samples.

### **DISPLAY MODES**

Roll Stored data and display updated continually. (timebase ranges 50sec/cm to 0,05ms/cm).

Refreshed Stored data and display updated by triggered sweep. (timebase ranges 50sec/cm to 0.05 ms/cm).

Sampling Stored data and display updated from trigger point in single shot mode.

Single Shot Freezes store at end of triggered sweep.

Display Hold Freezes store immediately.

Pretrigger Storage Available in Roll mode only, switchable fro 0%, 25%, 75% and 100% of full store pre-trigger.

### **PLOT OUTPUT**

Analogue output of the stored display.

Y Output Channel 1 or Channel 2 selected by Plot 1 or Plot 2 push switch for the respective channel via 4mm socket. Amplitude 100mV/cm (nominal).

Specification Section 2

X Output X ramp via 4mm socket.
Amplitude 100mV/cm (nominal).

Output Sweep Rate Selected by Time/cm (main timebase) range 50sec/cm to 50ms/cm in 1-2-5 sequence.

Output Impedances  $100\Omega$ .

Pen Lift Output High output to indicate penlift. TTL open collector. Maximum Voltage 15V. Maximum Sink Current 8mA.

Supply 100V, 120V, 220V and 240V  $\pm$ 10%. 45 to 400Hz, 40VA approx.

Safety Designed for IEC 348 Cat 1.

Operating Temperature Range 0 to 50°C (+15°C to 35°C for full accuracy).

Dimensions 140 x 305 x 460mm. (5.5") x (12.0") x (18.1")

Weight 6kg approx.

Accessories Supplied Handbook PN 450770. Mains Lead PN 402001 Optional Accessories

Probe Kit PB12

A passive probe kit with switched X1 and X10 attenuators .

X10 attenuation input impedance is  $10M\Omega/11.5pF$ .

Probe Kit PB13

A X10 passive probe with 1.5m of cable. Input impedance 10m/11.5pF.

Probe Kit PB17

A X100 passive probe with 1.5m of cable. Input impedance 100M $\Omega$ //4.5pF. Working voltage 1.5kV inc pk a.c.

Viewing Hood PN450401 Front Panel Cover PN450240 Rack Mount Kit PN450070

Trolley Type TR7 General Purpose

Protective Carrying Case PN42610 — A strong case which completely encloses the oscilloscope with 3 thicknesses of padded material covering the front panel.

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### INTERNATIONAL SAFETY WARNING

(as required for I.E.C. 348 Class I)

This instruction manual contains information and warnings which must be observed by the user to ensure safe operation and retain the apparatus in a safe condition. The instrument has been designed for indoor use within the specified limits of temperature. It should not be switched on if there are obvious signs of mechanical damage and it should not be used under wet conditions.

### **EARTHING**

The instrument must be operated with a protective earth connected via the appropriate (yellow/green) conductor of the supply cable. This is connected to the instrument before the line and neutral supply connections when the supply socket is inserted into the plug on the back of the instrument. If the final connection between the instrument and the supply is made elsewhere, the user must ensure earth connection is made before line and neutral.

If any supply cable other than that supplied with the instrument is used, it must carry an adequate protective earth conductor.

Any interruption of the protective earth conductor inside or outside the instrument is likely to make the instrument dangerous. Intentional interruption is prohibited.

Signal connections into the instrument should be connected after and disconnected before the protective earth connection is made, i.e. the supply lead must be connected at all times that signal leads are connected.

### LIVE PARTS

The instrument is safe to operate with the covers fitted and these must not be removed under normal usage. The covers protect the user from live parts and they should be removed only by suitably qualified personnel for maintenance or repair purposes. (see maintenance section).

### **VENTILATION**

The OS1420 relies on convection cooling and must not be operated in a position which restricts the external circulation of air.

### 3.1 CONNECTION TO THE SUPPLY

Before connecting the OS1420 to the supply, check that the supply range switches are set to suit the supply voltage to be used and that the correct fuse is fitted. Note that the fuse has to be changed when switching between the 100V and 220V ranges. The switches and fuse holder are mounted on the back panel of the instrument. Do not operate the range selection switches while the OS1420 is switched on.

### 3.2 OBTAINING A TRACE

 After connection to the supply, switch on by turning the INTENSITY control clockwise away from the OFF position. Check that the POWER indicator l.e.d. lights.

#### Set the:

Set NORM/STORE switch to NORM. MODE switch to CH1.

CH1 Y shift control (vert. arrows) to approx. mid setting.

CH1 VAR SENS control fully clockwise to the CAL position.

CH1 input coupling switch to GND. BRIGHT LINE button out (ON).

X MAG, button out (X1).

X shift control (horiz, arrows) to approx mid setting.

TIME/CM switch to  $5\mu$ s.

A horizontal trace should appear on the screen as the INTENSITY control is advanced.

- 3. Adjust the INTENSITY control to obtain a display of the required brightness.
- Adjust the FOCUS control to obtain a sharply defined trace.
- 5. Adjust the CH1 Y shift control and the X shift control to centralise the trace on the screen.
- 6. Adjust the TRACE ROTATE preset control if necessary to align the trace with the centre graticule line. It may be necessary to re-adjust this control only when the instrument is repositioned as the beam deflection can be affected by Earth's magnetic field or other sources of magnetic radiation.

NOTE: The OS1420 should not be operated close to sources of alternating magnetic field such as large transformers as these may interfere with the trace.

### 3.3 SETTING UP THE Y CHANNELS

- Using a coaxial input signal lead, connect a signal to the CH1 or CH2 input socket.
- 2. For
  - (a) Direct connection of the input signal, set the associated AC-Ground-DC slide switch to
  - (b) Capacitative coupling of the input signal through an internal 0.1µF 400V capacitor, set the slide switch to AC.

NOTE: When examining low amplitude a.c. signals superimposed on a high d.c. level, the slide switch should be set to AC and the sensitivity of the Y amplifier increased as in (4).

 To locate the base line, set the slide switch to the GND setting. At this setting, the input signal is open circuit and the input to the amplifier is connected to ground.

4. To select sensitivity, set the VOLTS/CM switch to the required range. For calibrated operation, the VARiable SENsitivity control should be set fully clockwise to the CAL position. This control can be used however to reduce the gain of the relevant amplifier and obtain any intermediate sensitivity between the calibrated switched ranges. To set to any particular calibrated sensitivity, the actual variation from the calibrated range can be set by viewing the CAL 1 Volt o/p on the 0.1V/cm or 0.2V/cm ranges. If the VAR SENS control is not moved, the sensitivity will differ from the calibrated value by approximately the same proportion on all settings of the VOLTS/CM switch.

To minimise pick-up at sensitive settings, it is essential to ensure that the ground lead connection is near to the signal point.

- 5. For vertical movement of the trace, adjust the Y shift controls (identified by the vertical arrows).
- Any trace movement under no-signal conditions, when the setting of the VOLTS/DIV switch is altered, can be overcome by adjustment of the relevant preset front panel balance control.

This control will only need adjustment at infrequent intervals. Before adjusting the BAL control, however, ensure that the input coupling switch is set to GND.

No adjustment should be made until a minimum of 15 min. warm-up time has elapsed after switch-on, or immediately after any large change of ambient temperature.

### 3.4 DISPLAY MODES

The mode switch determines the form of the display. In the STORE mode some of the display modes are not available. These will be indicated in the relevant paragraph.

### 3.4.1 SINGLE CHANNEL

For single trace display of one Y input against the timebase this switch should be set to CH1 or CH2 and the input signal applied to the appropriate input connector.

### 3.4.2 DUAL CHANNEL

For dual trace simultaneous display of both Y inputs against the timebase, this switch should be set to DUAL.

In the NORMal operating mode, two modes of beam switching are used and are selected automatically by the sweep rate selected by the TIME/CM switch. The alternate mode is used at fast sweep rates between 0.2ms/cm and 0.5µs/cm. At the slower rates from 0.2s/cm to 0.5ms/cm the chop mode operates at approx. 500kHz.

In the STORE mode the display is beamswitched alternately at a fixed rate of 200Hz.

#### 3.4.3 ADD

In the ADD mode, which is only available in the NORMAL operating mode, the single trace generated against the timebase is the algebraic sum of the CH1 and CH2 deflections.

If the INV CH2 button is operated the direction of the Y deflection for that channel is reversed. If used in the ADD mode, this facility allows the difference between the CHI and CH2 inputs to be displayed. The INV CH2 button has no effect on the polarity of internal CH2 trigger.

When examining small differences between large signals, the effect of small errors between the sensitivities of the two channels can be overcome by first connecting one input to both channels simultaneously and adjusting one or other of the VARiable SENSitivity controls to obtain a straight line.

In the STORE mode, the ADD position of the MODE switch is equivalent to the CH2 position.

#### 3.4.4 X-Y

In the X-Y mode, which is only available in NORMAL operating mode, the timebase is disabled and the CH2 input is displayed as the vertical Y deflection against the CH1 input displayed as horizontal X deflection. The CH1 shift control is inoperative and X position is determined only by the X shift control. The X10 MAG facility is also inoperative. X deflection sensitivity being determined by the CH1 controls only. The X bandwidth is limited to 1MHz and relative phase shift between X and Y delections may exceed 3° above 50kHz.

In the STORE mode selection of X-Y is equivalent to the selection of CH1.

### 3.5 TIMEBASE AND X-EXPANSION

The calibrated sweep speed of the internal timebase is determined by the setting of the TIME/CM switch and additionally in STORE mode by the ms—s button. When this button is in, the milliseconds section of the TIME/CM switch is converted to seconds, for example Ims/cm becomes 1s/cm. In NORMAL operation and in STORE mode on the SAMPLING section of the TIME/CM switch, the sweep rate may be varied by the VARiable SWEEP control, enabling intermediate sweep rates between the calibrated ranges to be obtained.

For horizontal shift of the trace, adjust the X shift control (horizontal arrows). If close examination of any portion of the trace is required, X10 expansion can be introduced by operation of the MAG Button. This provides an effective trace length of 100cm and any portion of this may be selected for viewing on the screen by operation of the X shift control.

### 3.6 TRIGGER

The timebase may be triggered internally from the CH1 or CH2 signals by operation of the corresponding

TRIGGER button, irrespective of whether the selected channel is being displayed. Alternatively, the timebase may be triggered from an external signal applied to the EXT TRIG sockets when both CH1 and CH2 buttons are operated simultaneously.

The + — button selects the slope, positive or negative going, which causes triggering when the signal passes through the level set by the TRIGGER LEVEL control. Presence of a TRIGGER signal is indicated by the associated TRIGGER l.e.d. This will flash at low trigger repetition rates and remain on at faster rates. Normally triggering can be obtained from internal deflection signals greater than 2mm pk/pk up to about 2MHz but the sensitivity reduces to about 1cm pk/pk at 20MHz. Corresponding external sensitivity is 0.25V pk/pk to 2MHz and 1.25V pk/pk at 20MHz.

With AC coupling, the low frequency sensitivity reduces to 1cm pk/pk at about 2Hz.

The Ext Trig input impedance is approx.  $100k\Omega/10pF$  and care should be taken not to apply more than 250V d.c. or pk, a.c. to this socket.

When the BRIGHT LINE ('BR LINE') button is out or ON, the timebase will free run in the absence of a correct trigger signal, to display a bright line or unsynchronised display until the level control is adjusted and/or the amplitude of the trigger signal is increased. This free-run action in the absence of correct trigger, helps in finding the trace and leads to ease of operation. If the timebase is required to free-run continuously, the LEVEL control should be set to either end of its rotation.

It is expected that the BRIGHT LINE OFF mode will be selected only when the instrument is to be used to display signals at repetition rates less than 40Hz or faster than 2MHz. This will prevent additional free-run sweeps from occuring between correctly triggered low frequency sweeps or erratic high frequency operation.

The coupling of the trigger signal may be selected as a.c. or d.c. by operation of the corresponding TRIGGER button. When both are pressed, an active synch. separator circuit is introduced to provide line or frame triggering for video waveforms. Field trigger occurs at low sweep rates up to  $100\mu$ s/cm and line trigger is automatically selected at fast sweep rates from  $50\mu$ s/cm. The trigger polarity should be selected for the polarity of the synch. pluses. At least 2mm pk/pk of synch. pulse amplitude is required with internal triggering, or 0.25V with external.

Summarising the use of the trigger controls for most applications:

- (a) With BRIGHT LINE ON (button out), select the trigger source CH1, CH2 or EXT and the coupling required, AC or DC.
- (b) Select the trigger slope + or and adjust the trigger level control to obtain a trace which is triggered at the required point.

#### 3.7 STORE CONTROL

STORE mode is selected by depressing the NORM/ STORE button. The various STORE modes are selected by operation of the buttons on the right hand side of the NORM/STORE control, and by the buttons on the right hand side of the TIME/CM switch. All controls associated with the STORE mode are labelled in blue.

#### 3.7.1 NORM/STORE

With this button out, NORMal operation is obtained. The instrument behaves like a conventional 20MHz oscilloscope. All controls associated with STORE mode have no effect.

With the button in, STORE mode is selected and the display is produced by the reading out of a digital store. Acquisition of data for this store, and the subsequent display of this data is controlled by the controls labelled in blue.

#### 3.7.2 ROLL/REFRESH

Selection of ROLL provides a form of free running timebase not found on a conventional oscilloscope. Incoming data is fed continuously to the store. As the display is thus updated, the trace appears to be moving or rolling to the left, in appearance, similar to the view through a 10cm window of a strip chart recorder trace.

As information is being continuously written into the store, at a trigger instant the store will only contain pretrigger information. Thus by using the single shot facility (see 3.7.3, 3.7.5) pre-trigger information even for transient signals may be stored and displayed.

The rate of rolling is controlled by the TIME/CM switch and ms-s button. At high roll speeds the display becomes meaningless to the user, so for the top three ranges of roll mode, 0.2ms/cm, 0.1 ms/cm, 0.05ms/cm, the display is blanked while information is stored in the memory. Once the information has been acquired ready for display, the store is read out once, and then, if release mode has been selected, the store is again updated and the display again blanked; the cycle of acquisition then display repeating until an alternative mode is selected. If trigger signals are not present and BRIGHT LINE is off the display will be blank on these three ranges until a trigger signal is present. The display on these three ranges still has a pretrigger facility in the released roll mode. Roll mode can be used on ranges 50sec/cm up to 0.05ms/cm.

If REFRESH is selected, the display obtained is similar to that obtained on a conventional oscilloscope but with the advantage of flicker-free operation at low timebase speeds. The display updates from the left hand side of the screen on receipt of a trigger as in conventional operation. If the instrument is in single shot mode (see 3.7.5) or the trigger is not present the display retains indefinitely the information captured on the previous sweep until a trigger is received in released mode or the instrument is rearmed. On the top three ranges of the TIME/CM switch for which refresh is applicable

0.2ms/cm, 0.1ms/cm, 0.05ms/cm, the display is blanked while the store is filled and then read out once when the acquisition is complete; this cycle repeating if in released mode, or if in single shot mode readout is then continuous. As in roll mode the display will be blanked if a trigger signal is not present, unless the display has been held or stored. Refresh mode is only used on ranges of 50s/cm to 0.05ms/cm of the TIME/CM switch.

#### 3.7.3 PRETRIGGER/25% + 75%

These two buttons select the amount of pretrigger required when using the Roll mode single shot facility (see 3.7.2 and 3.7.5). With both buttons out, 0% PRETRIGGER is selected, with only the 25% button depressed 25% PRETRIGGER is selected, similarly for the 75% button, and with both buttons depressed 100% PRETRIGGER is selected.

The amount of pretrigger selected determines the percentage of the display which is acquired before the trigger point, and hence the position of the trigger point on the display. For example, if a trace is stored with 25% Pretrigger selected, the trigger point is 2.5cm from the left hand side of the display, the first 2.5cm of the display is pretrigger information, and the last 7.5cm is posttrigger information.

Pretrigger as mentioned earlier is available in the roll single shot mode, but on the three top ranges of the TIME/CM switch for which roll is available, 0.2ms/cm, 0.1ms/cm and 0.05ms/cm, the pretrigger facility is available in the released roll mode also (see 3.7.2 and 3.7.4). On these ranges a 'refresh' type display is obtained but with the position of trigger point being selected by these buttons.

### 3.7.4 RELEASE

Operation of this button puts the instrument into its continuous acquisition mode. In ROLL this means that the display 'rolls' continuously and ignores triggers except on the ranges 0.2ms/cm 0.1ms/cm and 0.05ms/cm (see 3.7.2). In REFRESH the display updates until the display is filled with new information and then updating ceases until a trigger is received. The display will again begin updating from the left hand side of the screen. This cycle of refreshing the display, then awaiting a trigger, repeats indefinitely in the released refresh mode.

Release does not separate on timebase ranges of  $20\mu s/cm$  to  $0.5\mu s/cm$ .

### 3.7.5 ARM

This button when operated initiates the single shot storage facility of this instrument. On arming, in ROLL mode, the trace will roll across the screen, and the ARMED/STORED l.e.d. will begin flashing.

When a trigger is received the l.e.d. will cease flashing and switch off. Meanwhile the trace continues rolling, and and after the required amount of pretrigger information is obtained, the instrument will accept a trigger, and when the required amount of post trigger information has been acquired the trace will cease rolling and the ARMED/STORED I.e.d. comes on continuously. The display will not now alter unless rearmed, or put into release mode by operating the release button. In refresh, operation of the ARM button stops the display updating if currently occurring and initiates flashing of the ARMED/STORED I.e.d. On receipt of a trigger the display will begin updating from the left hand side of the screen and the I.e.d. will cease flashing. When the display has been fully refreshed the STORED I.e.d. will come on. This display will now not alter unless rearmed or released

In this single shot mode of operation there is an extra facility, SAMPLING, available on timebase ranges  $20\mu s/cm$  to  $0.5\mu s/cm$ . By using a repetitive sampling method it is possible to digitise waveforms which are repetitive in nature, up to the full bandwidth of the oscilloscope. Operation of ARM will blank the previous previous display and initiate a store cycle.

The store is then updated, one store location per channel per sweep of the timebase. During this process a dot is displayed which moves across the screen as the store is filled. Lack of triggers will cause the dot to halt and the TRIGGER l.e.d. to extinguish until triggers are again present. Once the store is full the stored l.e.d. will come on and a display of the stored waveform will occur until rearmed. Note that RELEASE, PLOT 1, PLOT 2 have no effect of these timebase ranges.

### 3.7.6 ms-

When this button is out the TIME/CM milliseconds ranges remain correct. However, when the button is depressed this multiplies the TIME/CM millisecond ranges by one thousand converting the millisecond/cm ranges to second/cm. It has no effect on other timebase ranges.

### 3.7.7 PLOT 1 PLOT 2

These two buttons initiate the plotting of the channel selected, PLOT 1 initiating a plot of the CH1 display, and similarly PLOT 2 initiating plot of CH2. Plot can only be initiated if a display is STORED (see 3.7.5) or DISPLAY HOLD is operated (see 3.7.8) and the TIME/CM switch is set on a milliseconds/cm range. The plotting speed is then a one-thousandth of the reciprocal of the TIME/CM range selected, for example a selection of 0.2ms/cm on the TIME/CM switch gives a plotting speed of

 $\frac{1}{0.2}$  x 1000 cm/ms which is 5cm/s,

The plot X and Y outputs are on the back panel of the instrument. A penlift signal is also available which is an open collector TTL o/p that goes high to indicate a pen lift if required.

### 3.7.8 DISPLAY HOLD

Operation of the DISPLAY HOLD freezes the display so that no further modification of the display can occur.

It can be used in ROLL mode to freeze the display if a feature of interest appears on the screen. Alternatively it can lock the display in REFRESH mode. Once the trace is frozen it can be plotted using PLOT 1 or PLOT 2 as required.

When the button is released, the instrument returns to a RELEASE mode. Hence operating HOLD will clear and ARM condition.

It should be noted that movement of the function switches after a display has been locked can disturb the display, particularly shifting the start point of the trace.

### 3.8 ADDITIONAL FACILITIES

Calibrator

This output pin on the front panel provides a positive going 1V flat topped square wave at approx. 1kHz. It can be used to check the sensitivity of the instrument or to set to any particular calibrated sensitivity (see section 3.3.4). The rise time is approx.  $2\mu$ s and the output impedance is approx.  $470\Omega$ , providing approx. 2.3mA when shorted to ground.

The CAL output may be used also to set up passive probes (see section 3.7.4).

Z mod.

This socket on the real panel allows modulation of the brightness. The input is d.c. coupled into approx.  $10k\Omega/10pF$ . The sensitivity at normal brightness setting requires about 2V to provide visible modulation. Approx. +40V is required to provide full trace blanking.

Care should be taken not to apply more than

100V d.c. or pk, a.c. to this socket.

3. Use of the Passive Probe

A X10 passive probe may be used to extend the voltage range and increase the input impedance of the Y amplifiers. The input resistance of a Y channel is 10M ohms, shunted by approximately 28pF. The effective capacitance of the input lead must be added to this and the resultant impedance can often load the signal source. Therefore it is advisable to use a 1M ohms, X10 probe such as PB12 or PB13. This reduces the input capacitance and increases the input resistance, at the expense of a 10X reduction in sensitivity. The probe inserts a shunt RC network in series to form a 10:1 attenuator with the input RC of the Y channel. To obtain a flat frequency response it is necessary to adjust the capacitance of the probe to match the input capacitance of the Y channel as follows:

- 1. Set the Y channel VOLTS/CM switch to 20mV, the TIME/CM switch to 500µs and trigger from the appropriate channel.
  - Connect the probe to the CAL socket.
- Adjust the probe compensation to obtain a level trace, i.e. flat top without overshoot or undershoot.

#### 4. Camera.

A camera may be used with the oscilloscope to record waveforms. This facility is particularly useful at slow timebase sweep rates. Suitable camera utilising Polaroid film may be obtained from Shackman and hand held against the tube face. Other oscilloscope cameras may be used but suitable adaptors must be obtained and should be discussed with the camera manufacturer.

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### Section 4

To aid component location, circuit references have been allocated in the following general pattern.

1	_	99	Components not mounted on printed
			circuit boards.

- 100 199 Components mounted on the attenuator assemblies.
- 200 299 Pre-amplifier and Ramp Generator components mounted on the daughter board.
- 300 399 Y Pre-amplifier and Beam Switch components mounted on the main board.
- 400 499 Y Amplifier and Y Output Amplifier components mounted on the main board.
- 500 599 Timebase and X Output Amplifier components mounted on the main board.
- 600 699 Trigger circuit components mounted on the main board.
- 700 799 Power Supply and Modulation Circuit components on the main board.
- 800 999 Digital Storage Board and associated components.
- 1100 1199 Function Switch Board and associated components.
- 1200 1299 Auxiliary Power Supply Board and associated components.
- 1300 1399 Pick off Board and associated components.
- 1400 1499 Plot switch Board and associated components.

### 4.1 GENERAL

With the NORMal/STORE button out the instrument behaves as a conventional oscilloscope. Referring to the block diagram (Fig. 1) signals applied to the CH1 and CH2 input sockets pass into their respective attenuators and amplifiers. The VOLTS/CM switch controls the gain of the pre-amplifier in steps 1.2.5 sequence to cover the ranges from 2mV/cm to 0.1V/cm and a  $\div 100$  attenuator is introduced before the amplifier on the ranges 0.2V/cm to 10V/cm.

The Variable Gain control adjusts the amplifier gain to give 1 to 2.5 times reduction of gain on all settings of the Volts/cm switch. The fast electronic beam switch selects either CH1 or the CH2 signal to be applied further and passed to the Y deflection plates of the c.r.t.

A sample of each signal is taken and passed to the trigger switch bank where selection of CH1, CH2 or Ext trig source is made.

The selected signal is amplified and passed to the Schmitt trigger, the output of which clocks the timebase bistable "on". The ramp generator then begins to

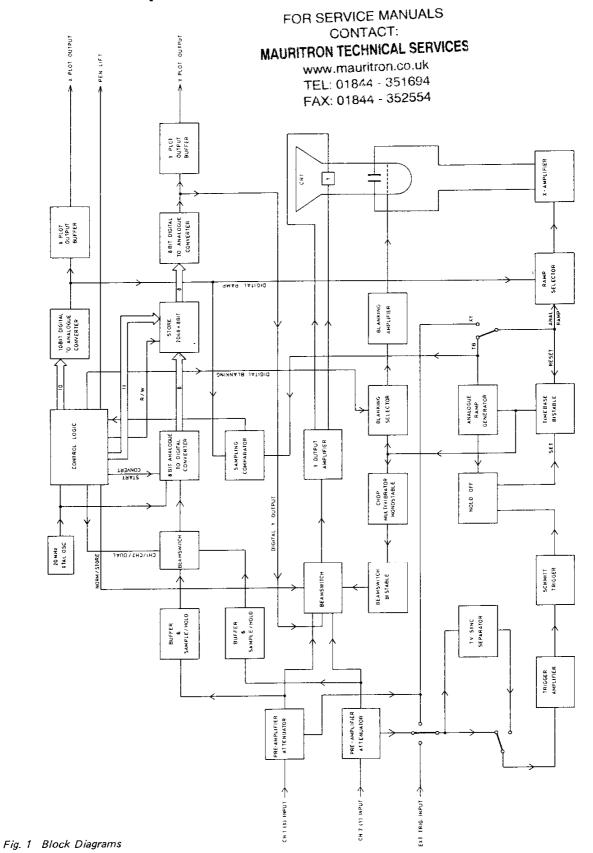
generate its linear ramp, which, after passing through the X amplifier, is applied to the X deflection plates of the c.r.t. and drives the electron beam linearly across the tube face. A portion of the signal from the ramp generator is fed back to the hold-off circuit, shutting the gate to prevent any further pulses from the Schmitt trigger from reaching the timebase bistable during the ramp period. When the ramp has reached the necessary maximum level, the timebase bistable is reset, and the ramp is quickly returned to its quiescent state. A timeconstant in the hold-off circuit retains this signal to inhibit another ramp from being initiated for a short period, until the ramp timing capacitor is discharged fully. Thus a ramp is generated at a rate set by the TIME/CM switch when the trigger signal reaches a predetermined level. This ramp sweeps the beam across the c.r.t. face, returns and waits for the next input cycle to reach the set trigger point, so producing subsequent ramps. The timebase bistable is connected to a blanking amplifier whose function is to turn on the electron beam during the sweep and blank it off during the fly-back and subsequent waiting period.

At fast sweep rates for a dual trace display, the TIME/CM switch automatically selects the alternate sweep mode of control for the beam switch. At the end of each sweep, the signal from the timebase reverses the state of the beam switch bistable, causing alternate displays of the CH1 and CH2 signal on successive sweeps of the timebase. At slow sweep rates, the chop mode is selected, when the chop multivibrator free runs independently, causing the beam to switch or chop between CH1 and CH2 levels during the sweep.

A signal from the multivibrator also blanks the trace during each switching transition. With CH1 or CH2 only selected, the beam switch bistable is held to select that channel only. In the X-Y mode, the bistable is held to select CH2 as the Y deflection signal, while an additional switch diverts the output from the CH1 pre-amplifier to the X output amplifier, as the X deflection signal in place of the normal ramp signal. The blanking amplifier is held in the bright-up state. When TV trigger mode is selected, an additional synch, separator circuit is introduced into the signal path leading into the trigger amplifier.

When the NORM/STORE button is in the instrument becomes a digital storage oscilloscope. The output of the Y dot joiner is routed through to the Y output amplifier. Analogue signals from the Y preamp are picked off, buffered, then fed into two sample and hold circuits. The outputs of the sample and holds are beamswitched into the Analogue to Digital Converter (ADC). This produces an 8 bit binary code representing the amplitude of the instantaneous signal input at 500 nanosecond intervals. The data produced is loaded into the store under control of the timing logic. The store can hold 2048 8 bit words and the data is entered at such a rate that the information contained in each of the two 1024 bytes of memory represents one complete sweep of each channel.

### Section 4



This data is then read out (non destructively) at a fixed rate and reconstructed as an analogue signal by the Digital to Analogue Converter (DAC), and applied to the Y output to give a continuous display of the store contents. Since the output of the DAC is in the form of discrete levels a dot joiner is included to join these levels and provide a continuous display.

In all the digital storage modes the timebase sweep is controlled by a ten bit counter which provides an increasing ten bit code which is reconstructed by a ten bit DAC and dot joiner to give an analogue ramp. This ramp is synchronised to the readout of the Y data from the store. This ramp is used to display the two sections of 1024 bytes of store alternately, or just one section if in a single channel mode, the lower 1024 bytes containing CH1 data, and the upper 1024 bytes CH2 information. The trigger is now entirely dissociated from the timebase since the latter runs continuously. The function of the trigger now is, in REFRESH to initiate a write cycle, during which a screen full of new information is entered into the store, and in ROLL to define the amount of pretrigger and post trigger information held in the store.

The trigger is still used to produce an analogue ramp: this is used by the sampling mode circuitry used to digitise repetitive waveforms on the top six ranges of the TIME/CM switch, and it defines the rate at which data is loaded into the store. In ROLL and REFRESH the rate at which data is entered into the store is defined by a programmable digital divider which divides the master 20MHZ clock under control of the TIME/CM switch to provide 100 data samples per cm unexpanded on the display. This is also the resolution obtained in the SAMPLING mode. Expansion of the display is carried out in the X amplifier by analogue means and this gives a resolution of 10 samples/cm.

### **4.2** THE Y AMPLIFIERS AND BEAM SWITCH These circuits are shown in Fig. 7, Fig. 10.

The attenuators and pre-amplifiers of channel 1 are identical to those of channel 2 and accordingly only channel 1 is described.

The input signal is applied to SKA and then to the attenuator via the 3 position slide switch, S101. This allows the input signal to be directly coupled through in the DC position or coupled via C105 in the AC position. In the central GND position, the input signal from SKA is left open circuited while the input to the attenuator is grounded.

On the most sensitive ranges, 2mV/cm to 100mV/cm, the VOLTS/CM switch, \$102, couples the signal through directly to the pre-amplifier, and the network resistor, RN101c, provides the input impedance. On the remaining ranges, \$102 introduces R101a into the signal path to form a 100:1 attenuator with RN101b in parallel with RN101c.

High frequency compensation of the attenuator is provided by C101 and C104, while C102 with C106 allows the input capacitance of the attenuator to be set to equalise that of the unattenuated ranges.

Diodes, D201 and D202, with R207 provide input protection by limiting the input voltage applied to the amplifier to the voltages of zener diode, D203 and the positive supply line.

The input stage of the pre-amplifier is formed by the f.e.t. source followers, TR201 and TR202, and emitter followers, TR204 and TR203. Unbalance in this stage is corrected by the BAL control potentiometer, R301.

The input stage drives the divider network, RN201. The VOLTS/CM switch second wafer, S201, selects the necessary output, either directly via RN201 on the 2mV or 200mV ranges, or attenuated by 2.5, 10, 25 or 50 times on the subsequent ranges. This network presents a constant output impedance and further attenuation is introduced by the shunt action of the VARIABLE sensitivity control, R217. The resultant signal is amplified by the integrated amplifier, IC301. The amplifier gain is determined by R309 and the preset, R302. The differential output is balanced by the bias through R308 from the preset, R307.

The differential outputs from IC301 (CH1) and IC351 (CH2) are then split. High impedance amplifiers buffer the signals to the Analogue to Digital Converter (ADC) and convert the differential signals to single ended outputs (see Analogue to Digital Converter). The differential outputs also feed R316 and R317, which provide defined signal currents to the beamswitch, and these are summed with the Y shift currents defined by R318 and R319 from the CH1 shift control, R315. The corresponding components for channel 2 are R366, R367, R368, R369 and R365. Channel 2 only differs for channel 1 by the addition of the double pole changover switch, S301, which reverses the output signals from IC351 in the INVERT mode.

The signals currents from IC301, and IC351 are fed into a 3 way beamswitch with the stored signal from the Digital to Analogue Converter (DAC). The beamswitch is formed by diodes, D301, D302, D303, D304, D351, D352, D353, D354, D811, D812, D813, D814. In NORMal mode the output of inverter U826e is low, switching off Q806 and Q807, it also takes the junctions of D811 and D813 low, diverting the signal currents from R823 and R824 reverse biasing D812, D814. The junctions of D301, D302 and D351, D352 are then both under control of IC501b. The bistable controls the beamswitching of the two Y channels into the Y output amplifier (see 4.5 Mode Control Circuits). In STORE mode the output of the inverter U826e is high. This forces the junctions of D301, D302 and D351, D352 low via Q806, Q807, diverting the Y preamplifier signal from the Y output amplifier.

At the same time, the junction of D811, D813 is taken high, forward biasing D812 and D814 and allowing the

signal from the Y DAC to drive the bases of TR401 and TR402 in the Y output amplifier. The outputs from the differential shunt feedback amplifier stage formed by TR401 and TR402, are fed to the ground emitter amplifier stage, TR403, and TR404. This in turn feeds the differential cascode Y output stage TR405, TR406, TR407 and TR408 to drive the Y deflection plates of the crt

High frequency compensation of the output amplifier is provided by networks between the emitters of TR403 and TR404 and those of TR405 and TR406. Adjustment of this compensation is by C402 and C405.

### 4.3 TRIGGER CIRCUITS

These circuits are shown in Figs. 8 and 10.

The Trigger Source switches, S502 and S503, connect the required trigger signal via the Trigger Coupling switches, S504 and S505, to the trigger buffer amplifier formed by TR601 and TR602. S502 selects the differential CH1 signal via R313 and R314 from IC301 (Fig. 4). S503 selects the equivalent CH2 signal via R363 and R364 from IC351. Where both S502 and S503 are selected, both of the above signals are disconnected and the single-sided input from the EXT TRIG input socket SKC is selected.

When the AC coupling switch, S504, is out, the trigger signals are directly coupled-through, but when this switch is in, AC coupling is introduced via C603 and C604 (C601 on External). TR601 and TR602 form a differential buffer amplifier with the DC balance controlled by the TRIGGER LEVEL control, R602. The differential output from this stage is applied to the comparator, IC602, which has positive feedback applied by R623 to form a Schmitt trigger circuit. The change-over switch, S506, reverses the output from TR601 and TR602 to determine the trigger slope.

When both S504 and S505 are "in" (AC and DC in for TV mode), the junction of R603 and C610 is connected to the -11V supply, D601 and D608 are brought into conduction while D602 and D604 are reverse biased. This diverts the output of the trigger amplifier away from IC602, into TR605, which amplifies the positive tips of the video waveform only. TR605 is prevented from saturation by feeding back the peak detected synch. pulses via TR607 and TR606 to the emitter of TR605. These pulses are amplified by IC601b and applied via R617 and D603 to the Schmitt trigger, IC602. IC601a is used in conjunction with S504 and S505 to disable the synch. separator when AC or DC is selected.

At the fast timebase sweep speeds, \$262a is open and TR603 is cut off. However, at speeds of 100µs/cm and slower, R608 is connected to +11V and TR603 is switched on. This effectively grounds C609 to introduce an RC integrating time constant into the synch. pulse

signal time path in the TV mode to separate out frame trigger.

The output of IC602 is used by the timebase generator (see next section).

### 4.4 ANALOGUE TIMEBASE GENERATOR AND X AMPLIFIER

The square wave trigger output from IC602 is applied (with d.c. bias of zener diode, D605) as the clock to the D type TTL flip-flop, IC501a. A positive-going trigger edge will clock the bistable driving  $\overline{Q}$  low. In the waiting state.  $\overline{Q}$  was high (+4.5V), turning on TR261 via R507 and R262, holding the input, and hence the output of the operational amplifier, IC261 at 0V. This timebase amplifier is connected as a direct voltage follower.

When the trigger signal sends  $\vec{Q}$  of IC501a low, the timebase clamp transistor, TR261, is turned off. Part of the constant current generated by TR264 flows through the resistor network, RN272, to charge C263 at a constant rate. The resultant positive-going linear ramp voltage generated at the input of IC261 is buffered by that amplifier to generate the low impedance ramp output.

The timebase range switch, \$262, selects the tap point on the network, RN272, to vary the ramp slope in the 1.2.5 sequence over a range of three decades. On all fast sweep ranges, TR262 is biased-off but on ramps 0.5ms/cm and slower, \$262c connects R263 to +11V. TR262 is turned on and C264 is effectively connected in parallel with C263 to slow the sweep rate 1000 times.

The constant current into the ramp generator is derived from the current mirror circuit formed by TR262 and TR264. The variable gain control, R261, provides an approximate 3:1 range of variation in this current, R506 provides a preset calibration control on the slow sweep rates, only when S262c is closed.

When the ramp reaches its maximum level the negative bias, introduced by R521 and R519, is overcome and TR503 turns on, driving the reset input of the timebase bistable low. As the bistable switches,  $\overline{Q}$  returns high and TR261 conducts to discharge the timing capacitor(s) and the sweep is complete. However, a hold-off action takes place to inhibit trigger signals during sweep and this remains for a short period after a sweep to ensure that the ramp potential is fully reset before the next sweep can be triggered. As the ramp goes positive, D506 conducts to charge C502, reverse biasing D503 and turning on TR502. At the end of the sweep when the timebase bistable is reset, Q goes low and the D input follows via the action of D508 and R511. The ramp output returns rapidly towards 0V but TR502 remains in conduction for a period determined by C502 and R518. Only when TR502 turns off can R516 and D507 take the D input high for the bistable to respond to the next clock input.

TR501 acts in a way similar to TR262 (described above) to introduce additional hold-off time through C501 on the slower half of the timebase ranges.

The bright line facility causes the timebase to free-run in the absence of trigger signals. The square wave output from the Schmitt trigger, IC602, is coupled via C615 into the peak detector diodes, D606 and D607, to generate a positive-going signal into the —ve input of IC601c driving its output negative. In the absence of such trigger signals for a period determined by C618 with R627 and R626, the output of IC601c goes positive. When TR502 turns off at the end of the hold-off period, D509 conducts to turn on TR504, driving the set input low to initiate another sweep.

This free-run condition is removed as soon as IC601c detects an output from the Schmitt trigger. When the o/p of IC601c is low it indicates the presence of a trigger signal. Q815 is then switched on, lighting Trigger l.e.d. D1

This free run condition can be inhibited by operation of the BRIGHT LINE OFF switch S501 which takes the junctions of D509 and D505 low via R562.

The output of the ramp generator IC251 is fed to the analogue multiplexer U821b. The other input of the multiplexer comes from the output of the sample and hold U830 in the digital ramp generator (see digital ramp generator). In NORMal mode the ramp output from IC261 is selected by the output of U826e going low. The ramp is then buffered by U827, a unity gain buffer amplifier, and drives the X output amplifier via R821 and C820. In STORE mode, the output of the digital ramp generator is selected and as in NORMal mode

drives the X output amplifier via amplifier U827, R539, and C515.

The X output amplifier is formed by the shunt feedback stage of TR509/TR511 driving single sided into the amplifier stage, TR513 and TR514. The collector output of this stage drives the X deflection plates of the c.r.t. directly from TR514 and via emitter follower TR515 and TR513. The gain introduced by TR509/TR511 is defined in the X10 magnification mode by the input resistance, R539, and the feedback resistance, R552, with the preset, R553. In this mode the transistor switch, TR512, is biased off. However, in the normal X1 magnification mode S507 is open and the current in R548 turns on TR512, introducing R544 with preset, R511, as additional feedback to reduce the gain of the amplifier accordingly.

The X shift control, R271, introduces an additional bias input via R541 and emitter follower TR506, through the potential divider R569/R545.

### 4.5 MODE CONTROL CIRCUITS

The display mode is controlled by S261 (fig.8) and the NORM/STORE button S.

S261 defines the state of three control lines L1, L2, L3. The state of these control lines is then further defined by the gating U822a, f, d, e, U823a, b, c, d U832a, b, c, U833a, d. The outputs of this gating DL1, DL2, DL3 are level shifted by Q808, Q809, Q810, and these outputs drive the mode control circuitry.

In NORMal mode, the state of DL1, DL2, DL3 follow L1, L2, L3 but in STORE mode these outputs do not follow L1, L2, and L3 (see table below).

### NORMAL MODE

							1C5	01b
DISPLAY MODE S261		L2	L3	DL1	DL2	DL3	Q	5
X-Y FOR SERVICE MANUALS	+11V	0	+11V	+11V	0	+11V	L	Н
CHI CONTACT:	0	+11V	0	0	+11V	0	Н	L
DUAMAURITRON TECHNICAL SERVIC	ESIIV	+11V	0	+11V	+11V	0	SWIT	CHING
CH2 www.mauritron.co.uk	+11V	0	0	+11V	0	0	L	Н
ADD TEL: 01844 - 351694	0	0	0	0	0	0	Н	Н
FAX: 01844 - <b>352554</b>	STOR	E MODE						
							IC5	01Б
DISPLAY MODE S261		L2	L3	DLI	DL2	DL3	Q	Q
X-Y	11V	0	+11V	+11V	0	0	L	H
CHI	0	+11V	0	+11V	0	0	L	Н
DUAL	+11V	+11V	0	+11V	0	0	L	Н
CH2	+11V	0	0	+11V	0	0	L	Н
ADD	0	0	0	+11V	0	0	L	Н

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Section 4.2 described the action of beamswitching diodes, D301 to D304, D351 to D354 and D811 to D814, and as mentioned then in NORMal mode the diodes D301, D302 and D351, D352 are controlled by the outputs of beam switch bistable, IC501b. In the CH1 mode, DL1 is low allowing R525 to take the set input of the bistable low, Q is high and  $\overline{Q}$  is low, selecting the channel 1 signal for Y display. In the CH2 and X-Y modes. DL1 is at +11V and R514 takes the set input high but L2 is open and R524 takes the reset input low to reverse the bistable and select the channel 2 signal.

In the Add mode, both DL1 and DL2 are low so that both set and reset are applied to the bistable, Q and  $\overline{Q}$  are high and both channel signals are added into the shunt feedback stage of the Y amplifier (Fig. 4). In this mode only, DL1, DL2, and DL3 are open, removing the bias through D401, D402 or D403 and defined by R401 and R402 via D405 and D406. This offsets the additional bias introduced by the selection of both channel signals.

Only in the X-Y mode, DL3 is held at +11V to turn on the diode gate of D515 and D514, so coupling the channel 1 preamplifier signal of IC301, via TR506 and R547 into the X output amplifier. At the same time D504 conducts to turn off the gain switching transistor, TR512 thereby selecting x10 X magnification irrespective of the positive of S507.

D501 conducts allowing current through R509 to turn on TR261, clamping the ramp generator so that no signal is fed into the X amplifier via R539. Finally, current through R512 turns on TR504, holding the timebase bistable set "on" to provide continuous bright-up of the trace.

In the Dual mode, both DL1 and DL2 and held at +11V so that the beam switch bistable, IC501b, is free of set or reset signals. Thus it can respond to clock signals and as its D input is connected to its Q output its state reverses on each clock input.

On the fast sweep ranges (0.2ms/cm and above), the clock input is derived via emitter follower, TR505, directly from the Q output of the timebase bistable. Thus the beam switch operates in the alternate mode. The Y deflection is switched between channels at the end of each sweep. TR507 and TR508 form a free-running emitter coupled multivibrator but on the above ranges, S262 f is open such that R534 is disconnected and the multivibrator is disabled.

On the slow ranges (0.5ms/cm and below), R534 is connected to +11V and the multivibrator runs. During each sweep period, the multivibrator provides continuous clock inputs to the beam switch bistable so that the beam deflection signal is made to chop between the two channel signals. The beam switching is inhibited between sweeps as the emitter follower, TR505, clamps high the clock input to the beam switch bistable. In all modes but Dual,

DL1 or DL2 are low and D512 or D513 conducts to inhibit the action of the multivibrator.

Ic601d is used for the IkHz calibrator. It is connected as an oscillator with positive feedback via R629 and negative feedback via R633. This with C617 defines the frequency as approx. 1kHz. The output is buffered by the transistor switch, TR604, which defines the calibrator output amplitude via the potential divider of R638 and R643 with preset, R641.

In the STORE mode DL1, DL2, DL3, as shown in the table above, force all selections on S261 to be effectively CH2. The beamswitch bistable, IC501b then behaves as described above for this mode. However, since both outputs from the Y preamplifiers are disabled the beamswitch bistable does not control the input to the Y amplifier, and the Y amplifier is driven by the Y DAC.

### 4.6 THE ANALOGUE TO DIGITAL CONVERTER These circuits are shown in Fig. 9, 10.

As described in Section 4.2 the differential CH1 and CH2 Y Preamplifier outputs are picked off and converted into a single output on the pick-off board.

The CHI outputs of IC301 are fed into a differential amplifier formed by Q1301, Q1302, whose gain is adjusted by R1329. On the normal DSO ranges, 50ms/cm to 0.5ms/cm Q1355 is turned on by the output of U805a. This output only goes high for timebase ranges of 20µs/cm to 0.5µs/cm. Q1356, when switched on connects C1351 across the roll off capacitor C1302, producing an high frequency roll off of approximately 1MHz.

A sample of the shift amount set by R315 is also differentially amplified by U1301a. The gain of this stage is adjusted by R1323 and the offset by R1325, adjustment of these two presets enables matching of the shift signals and the Y signals. The output of U1301a is added into the output of the differential amplifier Q1301 and Q1302. The resultant signal is buffered by emitter follower Q1304.

The circuitry of CH2 is identical to that for CH1. The circuit references for CH2 can be obtained by adding 50 to those of CH1, except for the CH1 components R1311, R1329, R1328, R1312, C1309, C1351, Q1355. The corresponding CH2 components for these are R1327, R1377, R1376, R1326, C1357, C1353 and Q1353.

The outputs of the emitter followers, Q1304 for CH1, Q1354 for CH2, drive a sample-and-hold.

The output Q1304 feeds the sample gate formed by D801, D802, D803 and D804. Normally the diodes, D803, D804 are held reverse biased by the zener diodes, D803 and D804. The control circuitry produces a 50ns sample pulse, when a conversion is required at the output of U803c. This pulse is amplified and converted into a differential signal by a long tail pairs, Q803 and Q804. The

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differential output of Q803, Q804 is applied to T801 pulsing the Shottky diodes D804 and D803 on for the duration of the sample pulse. These diodes conduct and allow C803 to follow the analogue input from Q1304. When the sampling pulse ends the capacitor holds the instantaneous value of the input. The diodes have a very low leakage and the hold capacitor C803 is buffered by a very high impedance amplifier formed by Q801a, b and Q802. The capacitor therefore has a low droop rate and the output of the amplifier will be held for long enough for the successive approximation converter (SAC) to convert the analogue signal accurately into a digital representation.

The sample-and-hold for CH2 behaves in exactly the same way as outlined above for CH1, with all circuit references being 9XX instead of 8XX (except U803c).

The two sample-and-holds hold the value of analogue signal at the sampling instant and their outputs are beamswitched by the switch formed by Q803 and Q804.The beamswitch is controlled by the  $Q \overline{Q}$  outputs of the bistable U835a. The Q high, Q805 is switched off and D909 is reverse biased. Hence Q905 is conducting and the output of the CH2 sample-and-hold is presented to the input of the SAC. With the Q output low the CH1 output is routed to the SAC. The D input to the bistable is the CH1 signal from U831. (see Section 4.7 for details of timings). This is clocked by the Start Convert signal from U803b, delayed by U801a, b by approximately 10ns, which initiates the conversion cycle of the SAC U815. The SAC has a 20MHz Xtal oscillator to control its internal logic. This is formed by U801f, U801e, C847, R867, R868 and XL801. The output of this oscillator is gated by U805b, so that the clock can be disabled externally and by the NORM/STORE button, thus reducing the amount of breakthrough in NORMal mode. If the 20MHz clock is disabled and external clock can be used via U802a.

The SAC conversion cycle is initiated as stated above by Start Convert. The conversion takes 9 20MHz clock cycles, i.e. 450ns, and it takes approximately 50ns for Start Convert to initiate the conversion. The complete conversion cycle takes 500ns. At the end of the conversion cycle the digital word representing the analogue input is latched onto the D0-D7 outputs. The SAC will nominally produce a code of 00000000 for an analogue input of OVand 11111111 for -0.5V the reference level input. However to compensate for the variation in gain of the pick-off buffer amplifier and sample-and-hold, the reference input to the SAC can be adjusted by R842 to -0.5V ±0.1V. This ensures that a CH1 or CH2 input signal that should cause a full screen deflection produces a range of codes from the ADC of 00000000 to 11111111.

### 4.7 TIMING AND CONTROL LOGIC

The timing signals used by the SAC are produced by the relatively high speed logic circuits around U807, a four bit decade counter. This counter is clocked by the

20MHz clock. Outputs QA QB, and QC which is inverted by U829d feed gate U805c which resets the bistable U806b on a count of three. This reset takes the Q output high. When the count reaches eight, QD goes high, clocking the bistable U806b, taking  $\overline{Q}$  output low. Thus the WE input to U831 is high from a count of three to eight, which is a period of time of 250ns.

A counter output of eight is detected by U804a, the output of which goes low. On the next ninth clock this low is clocked through bistable U806a producing a positive going edge on the Q output. On the tenth clock the Q output remains low. This output therefore is a 50ns pulse that occurs on a count of nine of the counter U807. This pulse passes through two inverting gates U802c, U803b and is further delayed by U801a and U801b. This pulse clocks bistable U835d and also initiates a conversion cycle of the S.A.C.

The QD output of the counter goes high on a count of eight and low on a count of ten, producing a 100ns pulse to U831 at a 2MHz repetition rate.

The LD input on Pin 9 of U807 is driven by U804c. One input of this gate will high when RESET STORED and/or STORED (PIN 3 U831) are low. The other input of this gate will be high when RESCH1 (Pin 51 U831) is high. RESCH1 is driven high by U835b which is clocked by EWRITE (Pin 50 U831). The reset input of this bistable is controlled by the TIME/CM SWITCH. A four bit code, D1, D2, DIV2, DIV5 is derived from this switch, from a double wafer on the pick-off board (See Fig. 9). The outputs are as shown in the table below:

TIMEBASE SPEED	TIMEBASE CODE			
SELECTED	DIV2	DIV5	DI	D2
50ms/cm	1	0	0	0
20	0	1	0	0
10	0	0	1	0
5	1	0	1	0
2	0	1	ī	0
I	0	0	0	1
0.5	1	0	0	1
0.2	0	1	0	1
0.1	0	0	1	1
0.05	1	0	1	1
20μs/cm	1	1	1	1
10	1	1	1	I
5	1	1	1	1
2	1	1	1	1
1	1	1	i	1
0.5	1	1	1	1

The output of gate U805a is high for all but the top six ranges when an all ones code is detected. This output is inverted by U826c. The output of this inverter is the

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SAMPLE signal. When SAMPLE is low, this takes the output of U809b high and hence the reset input of U835b low forcing RESCH1 high.

SAMPLE controls the selector formed by U802d, U802b and U803c. When SAMPLE is low, the Q output of U806a is routed through to the SAMPLE AND HOLDS, via U802c and U803b. U806a hence controls the sampling of the input signals, the sample pulse being the same width and timing on the clock to the beamswitch bistable U835a described earlier in this section. When SAMPLE is high the sample pulse is derived from the outputs of U904a. Again the pulse is approximately 50ns wide but its occurrence is controlled by the sampling circuitry described later (Section 4.11).

The waveforms described above are shown in Fig. 4.

#### 4.8 STORE CONTROL

The data from the ADC is stored in a 2048 x 8 static random access memory. The timing signals controlling the writing of data into this store are produced by U831, an uncommitted logic array (U.L.A.). This U.L.A. produces a Read/Write control signal NMWE (see Fig. 5 for timing). This signal consists of double pulses, each 250ns in length at a rate determined by the TIME/CM switch by the Sampling Pulse produced by U904a (see Section 4.11 for descriptions of relevant circuitry. This signal latches the data from the ADC into a TRISTATE buffer U816 and controls the Output Enable line of this buffer. When NMWE goes low the data held in this latch appear on the outputs Qo to Q7. Simultaneously the output buffers of the memory are put into a high impedance state by this signal eliminating contention on the data bus. Meanwhile U831 has produced a write address on lines A0 to A9 (U831 PINS 39, 38, 37, 36, 35, 34, 32, 31, 30, 29). For the first of the two negative going pulses of NMWE A10 (U831 PIN 28) is low and when NMWE goes high again the data held in the buffer is stored in the address selected by A0-A9 and A10. When NMWE goes low a second time, the new data from the ADC is latched into the buffer and again the stores' data lines go to high impedence. The lines A0-A9 still contain the same write address but A10 now has gone high so the new data is stored into the upper half of the store. When NMWE remains high in this way CHI and CH2 data is stored at a rate selected by the NMWE signal into their respective halves of the store.

When NMWE goes high the second time, the memory buffers are enabled and the stores will contain data from the address selected by A0-A10. Within the U.L.A. data lines, the write address is incremented after the second write. Reading of this data is again controlled by the U.L.A. U831. On all ranges below 0.2ms/cm reads are interleaved with writes of a 200kHz rate. Thus the address lines A0-A9 contain alternatively a write 'slot' and a read 'slot', each 'slot' lasting 2.5µs, enabling continuous reading and writing to occur. For the 3 ranges above 0.5ms/cm, the store is completely filled with new

data, writing prevented and store read out. This process repeats, so that a complete write followed by a complete read occurs continuously, unless in a single shot mode when reads continue indefinitely after a complete write cycle.

The read and writes are interleaved continuously at 200kHz. rate so that for each new read 'slot' there is a new read address. This address is presented to the store which then places on its data lines the data contained at this address. At the end of the read slot RWCLK goes low, latching the Read Data into latch U819. The output of this latch drives the DIGITAL TO ANNALOGUE CONVERTER (see section 4.9). Note that in Roll mode, for ranges of the TIME/CM below 0.2ms/cm the read address will increment by two if a write has occurred in the previous write slot. This causes the continuous 'rolling' effect visible on the display in this mode.

The waveforms associated with the store control circuitry described above are shown in Fig. 5.

Once a 'read' of the lower 1024 addresses of the store is complete, A10 goes high for the next 1024 'read' slots so that the upper half of the store is read.

The writing to and reading from the two halves of store are controlled by the DISPLAY MODE switch, S261. The three signal lines L1, L2, L3 derived from this switch are decoded and level shifted by gates, U822a, d, f, b and U823b, c, d. (see table in Section 4. for L1, L2, L3 codes). This gating produces two signals NCH1, and NCH2. NCH1 is low if X-Y or CH1 is selected and NCH2 is low if CH2 or ADD is selected on the MODE switch. If both lines are high, Dual channel operation is selected. The operation of the Dual Channel mode has been described earlier in this section.

If however either NCH1, or NCH2 is low the U.L.A. U831, forces line A10 to the memory low for NCH1 low and high for NCH2 low. Thus writing and reading of only the relevant half of the store occurs. One of the NMWE double pulses is also inhibited if either CH1 or CH2 is low, 'NCH1 low' inhibiting the first of the two pulses enabling only relevant information from the A.D.C. to be latched into the store and its latch. The beamswitch bistable is also controlled by NCH1, and NCH2. If NCH1 goes low, the bistable is RESET and the beamswitch forced over to CH1, and vice versa if NCH2 goes low.

The process of converting and storing data has been described above. However, the selection of when a write cycle should occur and the associated operating mode are controlled by ARM RELEASE, 25% and 75% PRETRIGGER, ROLL/REFRESH and DISPLAY HOLD. ARM AND RELEASE control and when the data is captured in a single shot mode or in a continuous mode. The ARM button S1101 initiates a single shot acquisition of data. S1101 when operated, takes low the reset input of bistable, U814C, producing a low on the output R892 and R893 introducing hysteresis onto the reset input. The bistable

output is inverted by U826d, and the resultant high level triggers one half of dual monostable, U1101, via input 2B, and allows timer, U1102, to oscillate at a period of 2Hz, set by R1107, R1106, R1108 and C1104, causing l.e.d. D1101, to flash at this rate. The time constant of this half of dual monostable, U1101, is set by C1102 and R1105 to be 100us, and so on triggering, the Q output of this monostable will go low for 100us. This negative going 100us pulse arms the ULA U831. If the STORED output of this device was high, it will now go low. If REFRESH is selected by pushing in the ROLL/REFRESH button, the address lines of the U.L.A., during the write slots as described earlier in this section, remain at zero, until a trigger occurs. TRIGGER signals are disabled initially on ARM by latch, U835a. The latch is held set by S1101 and the Q output is low, disabling U812a and preventing triggers passing through this gate. When \$1101 is released, the set input of U838a goes high after the length of the time constant set by C854 and R872. When the TRIG input next goes low it resets U838a taking the  $\overline{\mathbf{Q}}$  output high, enabling gate U812a and allowing triggers to reach U813a. When not in SAMPLING mode, the output of U805a is high, taking PIN1 of U813a high and PIN 11 low. The output of U812a will then be inverted by U813a, and triggers the U.L.A. when the TRIG input goes high. The output of U813a also drives U812b. The other input of this gate is high, again since RELEASE is high, taking low the output of U826f and forcing the output of U812c high. The inverted TRIG signal will thus take low the SET input of bistable U814c, forcing high the Q output, and low the output of U826d. This will take high the RESET on timer U1102 resetting the output, and switching off Q1101. The l.e.d. D1101 will extinguish.

Once the U.L.A. has received a trigger signal, the write addresses will increment from zero, at a rate determined by the TIME/CM switch, and at each successive store location, data from the ADC will be stored, as described earlier. When all 1024 store locations in each half or in one half of the store have been updated, the stored output of U831 will go high, taking low the output of U8046, high the output of U809a, and low the output of U829e. The STORED LED D1101 on the functions switch board will now light indicating that acquisition of data has now ceased and the display is now stored.

The operation of ARM in the ROLL mode is essentially as described above except that the write addresses begin incrementing immediately after the ARM to U831, and the ULA U831 ignores TRIG signals. When a sufficient amount of data has been entered into the store to satisfy the pretrigger requirements, the U.L.A. will now accept a TRIG signal. When the required amount of post trigger information has been stored, writing will cease and the STORED output of the U.L.A. will go high, as in REFRESH. As data is written into the store the read address increments so that an increasing offset occurs between the Read Address to the STORE

and the address lines to the DAC, U818, causing a 'rolling' effect on the display. The display ceases rolling when the STORED indication occurs, since writing ceases.

When ARM is operated, it also clocks bistable, U836a. The D input of this bistable is driven by gate, U824a. If the TIME/CM switch is selecting ranges 0.05 ms/cm, 0.1 ms/cm and 0.2 ms/cm, the output of either U833b or U833c will be low, taking high the output of U824a. If ROLL mode is selected the output of U824c will be low, again forcing high the output of U824a. The output of U824a therefore indicates that either one of the three timebase ranges mentioned above, or ROLL mode has been selected by S1105. Therefore the Q outputof bistable U836a will be low if ARM is operated and the output of U824a is high, forcing high the output of U824b, selecting ROLL mode to the U.L.A. until RELEASE or RESET or hold goes low, when the output of U824b will follow the state of the ROLL/REFRESH signal from \$1105.

Operation of the RELEASE button triggers monostable, U1101, on the function switch board. The monostable has a time constant of 100 us set by R1104 and C1101. The monostable will thus produce a negative-going 100µs pulse which clears the STORED condition and resets U836a which enables the ROLL/REFRESH signal to the U.L.A. to follow the ROLL/REFRESH button. In refresh, the operation of RELEASE essentially enables continuous recycling of the write cycle described above for ARM. The write address holds at zero until a trigger occurs, at which point, the write address begins incrementing, data being stored in each successive location. When the STORE has been filled with new data, writing ceases until another trigger is received when the writing process begins again. This cycle repeats indefinitely until the operating mode is altered.

In ROLL after operation of the RELEASE button, the write addresses to the store begin incrementing immediately, new data being stored at each location in succession. Again as in the ARMed mode the read address to the store increments by one extra count after each write, causing the rolling effect on the display. The write process occurs continuously and is unaffected by the TRIGGER signal, and the display as a result will roll continuously, new data appearing on the right-hand end of the screen and rolling across the screen to the left-hand side.

On the top three ranges of the TIME/CM switch for which ROLL and REFRESH are applicable, 0.2ms/cm, 0.1ms/cm and 0.05ms/cm, the display is blanked while data is being acquired and then after acquisition is complete the new data is displayed. The rolling effect on both ARM and RELEASE is therefore not present on these ranges. However data is acquired in exactly the same fashion as described above.

The amount of pretrigger information stored in ROLL mode is controlled by the two button 25%, 75% PRE-

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TRIGGER. When both buttons, S1103 and S1104, are out the signals PER 25 and PER 75 are both low, and with either S1103 or S1104 operated the relevant signals PER 25 or PER 75 will go high to indicate 25% or 75% PRETRIGGER has been selected. With both switches operated both signals will go high indicating 100% PRETRIGGER selected. These two control signals PER 25 and PER 75 are used by the U.L.A. U831, to control the acquisition of data with respect to the trigger point. If REFRESH mode is selected control signals PER 25 and PER 75 will both be low, indicating 0% PRETRIGGER, regardless of the state of the two PRETRIGGER buttons, S1105 forcing a low output from both S1103 and S1104.

Operation of Display hold freezes the display, holding the information present on the screen. When the DISPLAY HOLD button, S1404 is out, the set input of bistable U814b is high, and the reset input is low. The Q output of U814b is therefore low, taking the output of U826b high. The D input of U836b is thus high and so when DACIO of U831 goes high, halfway through a read cycle the Q output will be clocked high, producing a low of the output of U824d, and taking N HOLD on U831 and one input of U809c high. The U.L.A. U831 will take a high level as indicating a NOT HOLD signal. The NMWE signals will reach the memory enabling data to be written to the STORE as described earlier.

If DISPLAY HOLD is operated, i.e. pushed in, the set input of U814b will go low and the reset input will now be high taking the  $\overline{Q}$  output high. The D input of U836b will go low and when DAC 10 next goes high, during a read cycle the Q output will go low. This produces, a positive clock edge at U836a, latching either the state of the ROLL/REFRESH, or if the TIME/CM switch is on the ranges 0.2ms/cm, 0.1ms/cm and 0.05ms/cm, as described earlier. The N HOLD input of U831 is taken low, freezing the write address produced by the U.L.A. for the memory, preventing further locations in the store being updated. Gate U809c is also disabled driving high  $\overline{\text{NMWE}}$ , and hence preventing data being altered at the current write address.

### 4.9 DIGITAL TO ANALOGUE CONVERTER

The Y data present on the output of latch, U834, is converted into an analogue form by U820, a monolithic eight bit digital to analogue converter. A reference current is fed into this device and the Io and Io outputs produce a differential current output proportional to the product of this reference current and the digital code present on its data inputs Do to D7. Resistors, R886 and R887, set a reference current of ImA, giving Io and Io a range of 0→1 mA depending on the digital code selected. The reference current is derived from a 6V2 voltage reference formed by Zener Diode D821 and R885 decoupled by C859. Approximately one quarter of the Io and Io currents are fed into the differential amplifiers, U827a and U827d, which convert the currents into a voltage output of approx. +280mV.

A time constant of  $1\mu$ s, set by C822 R830 and R831, is

applied to this differential output. This matches the time constant of the digital ramp generator, and provides a dot joining effect on the display, the dot moving linearly between the data points, though the brightness increases non-linearly as the dot moves between the data points. An adjustment of the relative d.c. offset of the differential Y output signals is provided by R829 enabling the two Y output signals to be balanced. The outputs of this amplifier is fed into Y beamswitch via R823, R824, R371, R372 as described in section 4.2.

#### 4.10 DIGITAL RAMP GENERATOR

The U.L.A. provides a linearly incrementing address bus DAC1 to DAC10 to drive a 10 bit digital to analogue converter (DAC). The lines DAC1 to DAC10 increment from 0 to 1024 as the Y data is read out of the store, 0 corresponding to the left hand edge of the screen, and 1024 the right hand edge of the display. These ten signals are fed into U818, a monolithic 10 bit D.A.C. This produces the differential current outputs Io and Io which represents the product of the digital word on the data inputs and the reference current into the device. The reference current is set at 1mA by R845 and R846 which are connected to 0V(A) and the 6V2 voltage reference mentioned in the previous section.

The current  $\overline{10}$  which flows to U818 pin 2 derives from R844, the difference current feeding into R847. The voltage of 0 to +1V generated across R847 is buffered by the unity gain buffer, U825b (see Plot section 4.12).

The Io current output of U818 pin 4 is fed to amplifier, U825a, which converts it to a voltage output. The gain of this amplifier is set by preset, R834. A time constant of Lus on the output is set by R833, R822 and C821 to match the time constant in the Y D.A.C. output amplifier (a small analogue ramp is added into the amplifier input in sampling if necessary. See 4.11) The output of the D.A.C. has a glitch at the changeover of the m.s.b. To reduce this a sample of the m.s.b. is fed into the inverting input of the output amplifier via R849 and C830. The output of the amplifier drives one input of the multiplexer U821b via R833. The other input of this multiplexer is the analogue ramp output from IC261. When NORMal is selected the analogue ramp is fed through to the X output amplifier, and in STORE mode the digital ramp is fed to the X output amplifier, U826e controlling the multiplexer.

The U.L.A. U831 produces a digital blanking signal which lasts for the first four counts of the count on lines DAC1 to DAC10, i.e. 20us wide. This digital blanking signal is multiplexed with the analogue blanking signal from TR507 collector. In NORMal mode, the analogue blanking signal is selected and in STORE mode the digital blanking signal is selected, the selected signal driving the

Bright-up amplifier described in section 4.13, which provides blanking of the display when the c.r.t. beam flies back from the right hand side of the screen to the left hand side.

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### Section 4

### 4.11 SAMPLING

These circuits are shown in Figs. 10.

On the top six ranges,  $20\mu s/cm$  to  $0.5\mu s/cm$ , a repetitive sampling method is used to obtain a digital representation of the input waveform.

This technique uses the analogue ramp described in Section 4 and the digital ramp generator formed by U831 and U818 described in Section 4.10.

The aim of this technique is to obtain 1024 samples of the waveform in the time, selected by the TIME/CM switch, necessary to sweep 10.24cm across the screen. In the following discussion a TIME/CM selection of 1µs/cm will be used to illustrate this technique. The time taken to sweep 10.24cm is, using this figure of Lus/cm, 10.24µs. If we need 1024 samples of the waveform in this time, the samples must be taken at intervals of 10ns. Now the analogue timebase ramp must have the necessary slope to sweep the beam across 10.24cm of display in 10.24µs. If the amplitude of the ramp required to produce 10.24cm of deflection is A Volts, this slope is A/10240 V/ns. Therefore if the samples are taken at intervals of 10ns, this corresponds to a voltage interval of  $\frac{A}{10,240}$  x 10, or  $\frac{A}{1024}$  Volts

The slow ramp level in fact must increment at A/1024 Volt intervals to produce 10.24cm of display at full scale. Hence a comparator driven by the fast analogue ramp, (which starts at a defined point on the input waveform) and the output of the digital ramp, will produce pulses every time the fast ramp crosses the slow ramp. If the slow ramp after every crossing, increments by one level, i.e. A/1024V, the crossing point will increment at intervals of 10ns. If a sample of the input waveform is taken at each crossing the required objective of taking a sample at 10ns intervals from the trigger point is achieved, each successive sample occurring on successive fast ramps. The circuitry necessary to implement the above method will now be described in detail.

The sampling process is initiated by operating the ARM button. This takes low the reset on U814C, producing a high on the output of U826d. This will enable U812d, allowing the TRIG signals from IC501a pin 5 in the analogue timebase circuitry to clock counter U902. This TRIG signal goes high at the beginning of fast ramp and low during the fast ramp holdoff. Since U812d inverts the TRIG signal the counter is clocked at the end of the fast ramp.

To ensure that the slow ramp starts above the fast ramp, and hence ensure that the comparator will produce a positive going output, a Start-up circuit is incorporated which offsets the slow ramp until a crossing is obtained.

When the instrument is armed, the Q output of bistable, U904a, is low, and bistable U904b is reset. Counter U902 is then enabled by the Q output of U904b so that the counter will increment at the end of each fast ramp.

R921, R922, R923, R924, R925, R926 on the outputs of this counter produce a current into R836 on the non inverting input of amplifier, U825a, proportional to the count on the counter. Therefore as the counter increments, the output of U825a will be offset in a positive direction. The output of U818 is, at this time, constant and the data input from DAC1 to DAC10 is zero. The line DAC1 to DAC10 are incremented by the TRIG signal to the U.L.A. U831 which, at this time, are disabled at gate U813b pin 9, by the output of U904b.

When the output of amplifier, U825, is offset sufficiently so that the non inverting input of comparator, U903, is at a higher level than the lowest point of the fast analogue ramp, which is fed into the inverting input of this comparator from the output of IC261, the comparator will produce a positive going edge at its output. This output is fed back into the non-inverting input via R919 to ensure a sufficient amount of hysteresis at the switching point, preventing oscillation at this point. This positive-going output clocks a 'high' through bistable, U904a. The D input of this bistable has a time constant ensuring that for a short time after an ARM, the D input remains low, so that comparator crossings are ignored until the D.A.C., U818, has settled. The Q output of the bistable, U904a, will go high, once the comparator has produced a positive edge, and the D input has gone high. The Q output of U904a remains high for approx. 50ns after the Q output has gone high, producing a 50ns pulse at the output of U804d. As described in section 4.6, this pulse drives the sample and holds at the inputs to the SAC beamswitch. The Q output of U904a going high clocks bistable U904b, producing a high on the Q output, and a low on the Q output.

The enable to counter, U902, goes low, the counter stops incrementing, holding a fixed offset on the output of U825a U831 pin 47. Note that the TRIG input to U813 pin 10 has a time constant formed by C853 and R871. This ensures that the positive going output of U813b is delayed by approximately 2µs after the fast ramp finishes. This positive going output causes the D.A.C. outputs of U831 to increment, thus increasing the level of the slow ramp at U903 pin 2. When that fast ramp rises again, the comparator produces another positive going edge, delayed by one sample interval from the previous edge. Meanwhile when the fast ramp reset, and TRIG went low, bistable U904a was reset, and so this edge from the comparator will clock U904a and so produce another sample pulse. This sequence of events will repeat until 1024 sample pulses have been produced and the output of D.A.C. U818 has reached its maximum value. At this point the STORED output of U831 will go high. This produces a low at the input U808c setting flip-flop, U814c, disabling the clock input to counter, U902, taking low the D input of U904a and resetting U904b. The output of U809a will also go high, resetting counter, U902, and driving low the output of U82e, which switches on the STORED L.E.D. DI 101. The U.L.A. U831, outputs (DAC1 to DAC10) now increment at the read rate as described section 4.10.

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The 1024 negative-going sample pulses which are produced by U804d during the sampling process, not only drive the sample-and-holds in the A.D.C. but also initiate a conversion and store cycle for each sample taken that initiates conversion of the samples and then ensures the data produced by the A.D.C. is stored correctly.

In the Sampling mode, the output of U805a is low, taking high the output of U826c, this being the SAMPLE signal. SAMPLE, the reverse of this signal, is produced by U826a. U804d produces the 50ns sample pulses. When SAMPLE is high, these pulses are gated through U801c U803d and U803c to the sample-and-hold circuitry (described in Section 4.6). These pulses are inverted by U809b which is enabled in SAMPLE, and again inverted by U829c, and resets bistable, U835b, taking low the Q output. The Q output was previously high, and so the LD input of counter U807 was low, presetting the counter outputs to 7, the value determined by the A,B,C,D, preset inputs. The Q outputs of U835b going low clears the LD input on U807, and so on the next 20MHz clock, the counter will increment to a count of eight. Referring to Fig. 5, the counter and associated circuits will produce a WE signal at the Q output of U806b, a MHZCLK to U831 pin 54 and a Start convert signal to the SAC U815, as described in Section 4.7.

The timing logic will produce four start convert pulses, four write enables and four MHZCLK signals, at which point a positive edge is produced by U831 pin 50, clocking bistable U835b so that the Q output returns high, setting the  $\overline{LD}$  input of U807, which presets the counter to a count of 7 and holds the count until  $\overline{LD}$  returns high.

As the timing logic produced these pulses, U831 produces an A10 signal to determine which half of the store is to be written, an address on lines A0 to A9 to determine which location is to be written and a NMWE signal which writes the data into the store. A10 is clocked low by the first of the MHZCLK input to U831, and alternates after each MHZCLK ending high after the fourth MHZCLK signal. Address lines A0-A9 remain constant for the whole of this cycle and increments only when the TRIG input to U831 goes high, at the end of each analogue ramp, NMWE is delayed and inverted version of the WE input to U831, hence four of these signals occurs, each going low 50ns approximately after A10 changes, latching the address on the store address bus into the store. When NMWE returns high 250ns later, the data at the store data bus is latched into the store. The data latch U816, latches data from S.A.C. U815, and enables its output buffers when NMWE goes low, so that the memory receives new data from the A.D.C.

This cycle repeats for each of the 1024 sample pulses, with A0 to A9 incrementing after each cycle when TRIG goes high. After a full store of data is acquired, the STORED signal from U831 goes high, as described earlier, ending the data acquisition. Reading of this data will now continue until another single shot capture is requested via the ARM button.

#### 4 12 PLOT

A plot facility is provided as standard on this instrument which enables a waveform captured on either CH1 or CH2 is plotted on an X-Y or T-Y pen recorder.

Plot for CH1 is initiated by generating the PLOT1 button. The set input of bistable, U814a, is taken low, and the reset taken high driving the Q output high. When the button is released, the Q output will remain low. The Q output going high initiates the plot mode for CH1 via the PLOT 1 input of the U.L.A. 831. The PLOT output of U831 will go high, thus switching the analogue multiplexer U821a so that the output of U821b is routed through to the X ramp output, and after the first four Y data samples have been read out enables the output of U827c to pass through multiplexer, U821c, to the plot Y output. The plot signal is inverted by U829a which will switch on the PLOT L.E.D. on the front panel and also drive into the A input of monostable, U828a. The B input driven by the TSTMON output of U831 is already high, and the monostable fires, driving high the Q output, and low the Q output for approx. 500ms, the period set by R852 and C838. The CEP input of counter, U807, is taken low and so the counter halts, holding up the plot operation 500ms. The set input of bistable, U838b, is driven low for 500ms, taking high the Q output, and taking low the penlift via open collector gate U832d. After 500ms plot continues and the data is readout from the store and reconstructed by DAC U820. The current output of U820 is converted into a bipolar voltage output by amplifier U827c, at approx. an output level of 100mV/cm.

The X ramp output is produced by D.A.C. U818, in synchronism with Y data readout. One of the current outputs of this D.A.C. drives amplifier, U825b, which converts this current into unipolar, voltage output at a level of approximately 100mV/cm. When the data has been plotted TSTMON pin 18 of U831, having been low during the plotting, returns high. The A input of U828 is still low at this time and so U828 is retriggered, again halting counter, U807, for 500ms, holding the Plot outputs at the last point plotted. The reset input of U8 will also go low for 500ms, taking high the penlift output, U832d. After 500ms the plot mode will be disabled and the display will return to the normal readout rate.

Operation of PLOT 2 is the same as PLOT 1, bistable U814d being replaced by U814a in the above description.

### 4.13 POWER SUPPLIES AND C.R.T. CIRCUITS

Circuits for the power supplies are shown in Figs. 10, 11. The following D.C. supples are generated in the power supply circuits from secondary windings on the supply transformer, T.l.

+ 210V, + 11V, + 12V, + 7V, + 5V, - 5V, - 11V - 1850V.

The + 210V line is used primarily in the X and Y output amplifiers. The -1850V line is the cathode supply for the c.r.t. An additional 5V line is generated in the timebase from the + 11V line by IC552 (Fig. 8).

### Section 4

The incoming a.c. supply from the supply connector, PLM, is switched by S1 and fuse protected by FS1 before reaching the two supply range switches, S2 and S3. S2 connects the two primary windings of T1 in series or in parallel for 120V or 240V operation while S3 selects the necessary tap for 100V or 220V operation.

The output from the 210V secondary is bridge rectified by the four bridge-connected diodes, D722 to D725, into the reservoir capacitor, C705. The resultant d.c. voltage protected by FS701 feeds the h.t. regulator for the +210V supply. D730 is the reference for this supply, buffered by emitter follower, TR711, and the Darlington pair, TR713. The return of the rectified 210V supply is via the 11V line to balance load currents in the low voltage supplies.

The four low supplies +11V, +7V, -5V (used on the main p.c.b. assembly), and -11V are derived from a single 25V secondary of transformer, T1. Its output is bridge-rectified by bridge connected diodes, D726 to D729, into the reservoir capacitor, C704.

The distribution with respect to the 0V line of the voltage across this capacitor is determined by the -11V shunt regulator and the +11V series regulator. The -11V reference is provided by the sener diode, D711, with temperature compensation diodes, D713 and D714, and the shunt transistor, TR712, conducts to maintain the -11V line at the correct potential.

The -5V line is derived from this -11V line by the zener diode, D712, with the compensation diode, D720, followed by the emitter follower, TR709.

With the negative side of the unstabilised supply across C704 defined at -11V by that stabiliser, the positive side is applied to the series regulator, IC702, which takes up all variation in the unstabilised supply to define the +11V line. This is a 15V regulator with 'low' pin 3, returned to a -4V potential defined from the -5V supply by R735 and R734.

The +7V supply is provided from the +11V supply by a further 12V series regulator, IC701, operating with respect to the -5V line.

All the above outputs are connected to the subsequent oscilloscope circuitry via split pads in the copper track pattern. These are normally bridged by solder but can be used to isolate each line to assist fault finding.

The +12V, +5V and -5V supplies are derived from secondary windings on T1 of 14V, 8.5V and 8.5V respectively. The 14V output is bridge-rectified by D1205, D1206, D1207 and D1208 and smoothed by C1204 and C1205. A 12V regulator U1202 provides a regulated supply of 12V, which is decoupled by C1206. The +5V and -5V supplies are produced in a similar manner, the relevant components being D1201, D1202, D1203, D1204, C1201, C1202, U1201, C1203 and D1209, D1210, D1211, D1212, C1207, C1208, U1203 and C1209.

The grid and cathode supplies for the c.r.t. are derived via the voltage doubler circuit D718, D719, C711 and C712,

from the 950V secondary of T1. The negative side of the unstabilised supply developed across C711 and C712 is held at approx. -200V with respect to 0V by the series zener diode, D706, which is returned to the stabilised cathode potential of -1850V. Subsequent variations in the unstabilised supply are developed across the series regulator, TR707, of the e.h.t. regulator. The feedback path of this regulator uses the current from the -1850V line defined by the resistors R715, R714 in parallel with R744 (the Focus pot.) and RN720e. The latter being within the e.h.t. network. This current is returned to the +7V line via R731, R725 and R726. If the resultant potential of the tap point defined by the preset, R725, is not at approx. -4.5V, the current in transistor, TR706 will change to correct the stabilising voltage across TR707, TR706 and TR707 are connected in cascode.

The heater of the c.r.t. is supplied directly from an independent 6.3V secondary winding of T1.

The OS1400 employs a novel modulation circuit to control the grid potential with respect to the cathode potential. The transistor pair, TR703 and TR704, generate an essentially constant current from the collector of TR703. This generates a constant voltage across RN720 and preset, R713, and is returned to ground via the output of the bright-up amplifier. Thus signal variations from this amplifier which operates with respect to 0V are transferred with the large negative d.c. offset to the collector of TR703, to be applied to the grid of the c.r.t. via the emitter follower, TR716.

In more detail, the constant current from TR703 is defined by the emitter resistance, RN720c and the base potential, from the divider, RN720a and RN720b.

This constant current source is returned to the -200V line (negative of D706) so that the collector of TR703 (the c.r.t. grid) can move negative from the cathode. The collector potential is protected by D705 against excessive swing during switch-on or switch-off conditions. While RN720d and R713 generate the necessary large d.c. potential to couple the bright-up signals to the grid, the high frequency components are by-passed through C702.

The bright-up signal amplifier is formed by the cascode transistor pair, TR701 and TR702, with shunt feedback via R704. It responds to the sum of three inputs. The first is a d.c. bias via R707 from the INTENSITY control, R745. The second is the external Z Modulation signal from SKG, via R703. The third is the signal from the blanking selector, U813a, which in NORMAL provides bright-up during each timebase sweep with blanking of each chop transition if appropriate, and in STORE mode provodes bright-up on each readout sweep. Diodes, D701 and D702, provide protection against excessive external inputs and with R702, prevent saturation of TR702.

The focus electrode of the c.r.t. is supplies from the focus control potentiometer, R744, with a portion of the -1850V supply. The astig. electrode is supplied from

### Section 4

preset, R708 driven from the +210V supply via the divider network R746, R747.

Minor angular misalignment of the gun assembly of the c.r.t. or the effects of externally applied magnetic fields,

axial to the c.r.t., can be corrected by the trace rotation coil. This coil is round the neck of the c.r.t. and the current is determined by the TRACE ROTATION control, R737, connected between the ±11V supplies and driving emitter followers, TR714 and TR715.

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#### 5.1 GENERAL

Fig. 2 and 3 show the internal location of the major components, subassemblies and preset controls. No regular maintenance is required apart from the routine recalibration. The construction of the instrument is such that full access to all calibration controls and to most components can be obtained once the two halves of the case have been removed (See section 5.2).

Supply voltage adjustment is made by the two selector switches on the rear panel. The supply fuse is mounted adjacent to these switches and the supply connector. This connector should be removed or the instrument switched off before operating the switches. For 100 or 120V operation a 500mA, 20mm slo-blo fuse is required (Part No. 33685), for 200 or 220V operation a 250mA, 20mm slo-blo fuse is required (Part No. 33684). The internal H.T. fuse is a 100mA, 20mm fuse (Part No. 32958).

### 5.2 REMOVAL OF THE CASE AND SUB-ASSEMBLIES

WARNING

DANGEROUS VOLTAGES ARE EXPOSED ONCE THE CASE IS REMOVED. MAINTENANCE SHOULD BE CARRIED OUT ONLY BY QUALIFIED PERSONNEL. PARTICULAR CARE SHOULD BE TAKEN ON THE C.R.T. AND THE E.H.T. AREA OF THE MAIN PRINTED BOARD WHERE VOLTAGES IN EXCESS OF 2000V ARE PRESENT. THESE VOLTAGES MAY BE RETAINED AS STORED CHARGE FOR UP TO ONE MINUTE AFTER THE SUPPLY IS DISCONNECTED.

- (a) To remove the Cast (Top section) DISCONNECT FROM THE SUPPLY. Remove the two fixing screws at the top front sides and lift the top cover up and forward to clear the front moulded frame and the rear plastic moulded cover.
- (b) To remove the Cast (Lower section) and Handle assembly. DISCONNECT FROM THE SUPPLY. Remove the two fixing screws at the top front sides and proceed to remove the top cover as detailed in (a) above. Rest the instrument upside down and remove the screw from the centre of the front frame, securing the cover. Lift the lower cover up and forward to clear the front moulded frame and the rear plastic cover. It may assist this operation if the screws holding the rear moulding are slackened but not removed.
- (c) Removal of the C.R.T. Remove the case as described in (a) and (b) above. Disconnect the trace rotation coil leads from pins 734 and 735 on the main printed circuit board. Unplug the tube base assembly. The base itself is carried on a small printed board which has been designed to allow access to facilitate withdrawal

from the c.r.t. pins. Remove the single clamp fixing screw (see Fig. 2) and rotate the two clamp sections approx 30° to free the clip from the centre panel. Once the tube and clamp assembly are free the clamp itself can be slackened on the tube. Slide the tube backward through the centre panel until the c.r.t. face plate is clear of the front mounting clip. The tube can then be lifted up and drawn forward, to clear the top edge of the front panel and frame moulding of the instrument. Withdraw the tube from the shield and the two part clamp.

When fitting a new tube, operate in the reverse order to the above instructions, with the exception of the tube clamp and centre panel fixing screw. On re-assembly the fixed part (rear) of the c.r.t. clamp is located in the slotted locating holes in the bulkhead and the retaining screw is fitted. The tube is then held forward against the graticule in the front moulding whilst the clamping ring is rotated to hole and lock the tube in place. Do not over tighten this ring.

Check the polarity of re-connection of trace rotation coil leads. Clockwise rotation of the front panel preset control should cause a corresponding movement of the trace.

(d) Removal of the Attenuator assembly.

Should it be necessary during repair to remove the attenuator and screens around the pre-amplifier for access to components on that board or on the front of the main board, proceed as follows.

Remove the collet fitted knob on the timebase switch. Access to the collet securing screw or nut is by prising off the clip in the centre cap on the knob. Remove the small push on knobs on the two Variable Sensitivity controls, the Mode switch, the Trigger Level, the Variable Sweep and X Shift controls. Unsolder and, using a desoldering tool clear the solder from the three screens where they are earthed onto the pre-amplifier board.

Unsolder and remove the wires from the CAL 1V pin and the EXT trigger connection on the input printed circuit board. Unsolder also the two signal connections to pins 201 and 231 on the pre-amplifier board.

The sub section front panel, carrying with it the two attenuator volts/cm switches, the two AC/GND/DC switches and the input coupling printed board can now be un-latched by springing the four latch fingers away from the moulded frame and withdrawing the complete unit.

Re-assembly is the reverse of the aforementioned. Since the two attenuator switch wafers are symmetrical the shaft can be inserted in either of the two possible alignment positions.

(e) Removal of the Input Coupling Switch printed circuit assembly.

If it is necessary to gain access to the small printed board which carried the input selection switches and the A.C. coupling capacitors for each Y channel, together with the input network for the External trigger signal proceed as follows. Using a desoldering tool, unsolder the tags of the input screen, clear the holes of solder and remove the screen Unsolder and remove the two wires connecting the input printed board with the two attenuator wafer sections of each volts/cm switch. Desolder the three input B.N.C. sockets from this board and the three screen earthing points. The board should then be free for removal by easing upward, off the screen tags, then rotated to enable the switch sliders to clear the front moulding, and so withdrawn.

Re-assembly is the reverse of this sequence.

(f) Removal of the C.R.T. Control Potentiometer board.

If it is necessary to gain access to the control pots proceed as follows. Remove the push on knobs on the Focus and the Intensity controls. Ease the spacer retaining ears out of the printed board, so freeing the board from its retaining plastic spacer. Separate the two control pot shafts from the moulded shaft couplers. Full access to both the component side and the track side of the board is now facilitated and the faulty component can be readily accessed.

(g) Removal of the Pick-off Board

If access to the pick-off board for repair or maintenance is required, the D.S.O. p.c.b. can be easily removed. First remove all plugs and sockets from the D.S.O. board and then lift the board clear of the 3 supporting hinges taking care not to catch the trailing cable assemblies. This clears the area around the Pick-off Board, which is supported by two pillars on the edge near the c.r.t. and the switch wafer on the opposite side. Unscrew the nuts securing the wafer onto the switch shaft and slide the board off the two pillars and this shaft, taking care not to damage the wiring under this board. Remove the socket from the lower edge of the board and from the 16 pin DIL SKT next to the switch wafer on the reverse of this board. The board may now be lifted clear.

### 5.3 FAULT FINDING

Before any fault location is attempted, it is suggested that all supply voltages are checked. Subsequent signal voltages and waveforms should then be checked according to the following list, which may be used as a general guide and aid to servicing. Note that the typical voltages for unstabilised supplies are quoted for nominal mid-range supply voltages.

If a fault cannot be cleared it is recommended that the instrument is returned to the manufacturer for repair (see section 7).

When faults have been cleared it is recommended that the setting-up procedure of section 5.4 is followed.

For checking the supply lines there is a double row of test pins, separated by bridged split pads. These pins will give outputs of +11V, -11V, +210V, +7V and -5V and if required the currents drawn by each line can quickly be measured simply by breaking the solder shorting the split pad for normal working operation, and inserting a current measuring meter between the two pins. In all five cases the line feed is nearer to the rear of the instrument, whilst the line load is connected to the forward pin.

The +12V +5V, -5V supplies for the DSQ board may be monitored on the D.S.O. board at PLPP pins 1 to 6.

### Normal Operating Conditions

Unless otherwise specified the controls are set for single channel operation with the trace centred and timebase running. Potentials are specified with respect to ground and should be measured with a high impedance voltmeter, digital voltmeter or oscilloscope as appropriate. The NORMal switch should be set to NORMal unless otherwise specified.

### (a) Supplies Unregulated

30V DC across C704 from 25 r.m.s. secondary voltage 268V DC across C705 from 210 r.m.s. secondary voltage 2.5kV DC across C711 + C712 from 950V r.m.s. secondary voltage

12V DC across C1201 from 8.5V r.m.s. secondary voltage 20V DC across C1204 from 14V r.m.s. secondary voltage 12V DC across C1207 from 8.5V r.m.s. secondary voltage

### Stabilised

```
+210V
           ± 21V
+11V
           \pm 0.5V
+7V
           \pm 0.4V - 0.6V
~5V
           -10.4V, - 0.6V
~11V
           ± 0.5V
+12V
           ± 0.6V
+5V
           ± 0.25V
                       From auxiliary supply board
-5V
```

### (b) Y-amplifier

Test Point	D.C. Level Sensitivity
TR203/204 Collector	+7V -
IC301, pin 1	+1V ±0.8V -
IC301, pin 14	+1V ±0.8V 2mV/cm
IC301, pins 7, 8	+3.5V 65mV/cm each sid



### HANDBOOK AMENDMENT, OS300, OS1400, OS1420 SERIES

### Note to Section 5.4

The unstabilised EHT voltage is a function of the peak-to-peak supply voltage and is thus waveform dependent. Operation of the set via a variable or other transformer may introduce peak clipping of the supply to the set and cause subsequent errors in checking or re-setting the EHT stabiliser range. (R725 according to section 5.4b above).

To check the effect of introducing a variable transformer to drive the set, first operate the set directly from the supply and note the supply voltage and the collector voltage of TR707.

Then operate the set via the variable transformer and adjust the supply voltage to the set to give the same voltage on TR707. Any difference in the supply voltage as measured represents a limitation of the variable transformer.

### For example: -

Assume that when operating directly from the supply, the supply is measured as 250V and the voltage on TR707 as 430V.

Then on operation of the set through a variable transformer, the output of that transformer into the set is measured as 265V when adjusted to give the same 430V on TR707. The difference of 15V is a result of the impedance of the variable transformer. The input to the set should be adjusted to 240V + 15V, (i.e. 255V) to check or set the voltage on TR707 to 405V.

The voltage on TR707 can have an error of  $\pm$  20V before any stabilisation problem occurs. Note that adjustment of R725 changes the stabilised EHT voltage and subsequent full recalibration of the set is required. The stabilised EHT voltage should be -1850V + 5%

E.JG. SALMON

10.8.83

(Attachment to Memo)

110.27	12.01/	20V/ =	With MODM	10501 2	(4)// (0-1	1460	
U827a	+3.9V 7	Umv/cm	With NORM /STORE	IC501, pin 2	+4V (Ov during ho	•	
U827d	+3.9V 70	70mV/cm switch in		IC501, pin 3	Trigger pulses betv +2.8V levels	veen -0.5V and	
T D	<b>DOT</b> 10		STORE	IC501, pin 4	+5V (0V during re	set by bright-	
Test Point	D.C. Level S			m . b	line)		
TR401/402 Collector		0mV/cm		Test Point	Signal +0.2V between sweeps		
TR403/404 Collector		40mV/cn	n each side	IC501, pin 5	+0.2V between sw +4.5V during swee		
TR405/406 Collector	+12.6V	-		IC501, pin 6	+4.5V between sw	-	
TR4057/408 Base	+15.6V	-		10501, pm 0	+0.2V during sweeps		
TR407/408 Collector		.8V/cm e	ach side	IC501, pins 8, 9	Beam switched bet and +4.3V levels	tween +0.2V	
(c) Analogue Ramp				IC501, pins 10, 13	-0.6V or 4.5V dep	ending on	
Test Point	Signal			,	mode switch settin	_	
Across R265 or R266	0.3V d.c. at n	nin.		IC501, pin 11	Chop/alt. pulses be and +4.7V levels	etween +0.2V	
IC261 pin 3 and pin 6	+3.7V ramp f	from 0.1V	' level	IC601, pin 8	+0.5V triggered or	bright-line	
TR264 Collector	+3.7V ramp f			, (	off +0V bright line		
	between 0 and +4V dependent on sweep rate selected.			IC601, pin 9	OV triggered or bright-line off +9.5V bright line operating		
(d) X-amplifier				(a) Pright IIs Ameli	ifian		
Test Point	D.C. Level	Signa	ıl	(g) Bright-Up Ampli Test Point			
TR512 Collector	+0.65V		nV/cm		Signal Continue signal 14	I OV (Dlank)	
	•	Centre Screen) 6.0V ramp		TR507 Collector	Swtiching signal +4 to 0V (Bright up)	F.8V (Blank)	
TR511 Emitter +3.7V 500mV/ (Centre Screen) 6.0V rar			V/CIII	Switching signal +5.0V to 0V (STORE selected on NORM/STORE			
TR514 Base -3.0V -		-	<b>F</b>				
TR513/513	+118V	12V/	cm each side		switch)		
1 13 13   3 13	1110 4		140V ramp each	TR702 Base Collector	+2V Between +6V and +48V dependent on intensity		
		side		Collector			
(e) Trigger Amplifier	r			RN720, pin 4	-2kV		
Test Point	D.C. Level	Si	gnal	RN720, pin 5	+50V with respect to pin 4		
TR601/602 Base	OV on Ext.			RN720, pin 6	+340V with respec	t to -1850V	
	OV on Int A.C	J. 65 sid	mV/cm each				
	+3.5V on Int	•	imV/cm each	(h) Analogue to Digi			
TD (01/(00 G U		sic	ie	For following measure mode at 0.5ms/cm.	ments set instrumen	t into STORE	
TR601/602 Collector	-4.8V	25 sic	mV/cm each	Test Point	D.C. Level	Sensitivity	
On TV mode:- TR601	and TR602 col			Q1302 Collector		65mV/cm	
tween -8.5V and -10.5				Q1304 Emitter	0V	65mV/cm	
Trig. Level Control.			U1301a pin 1		65mV/cm		
IC602, pin 9. Trigger o	utput switches	between	-2V and	D804, D803 Junction	0V	65mV/cm	
-5.6V levels.				Q802 Emitter	-0.25V	65mV/cm	
(f) Timebase Contro	l			Q805, Q905 Base			
Test Point	Signal			U815 Pin 16	-0.25V	65mV/cm	
IC501, pin 14 +5V, ±0.25V		Pin 2	50ns pulse 0	4V signal			
IC501, pin 1 +5V (+1V at end of ramp)			Pin 18	20MHz Clk.Switchi	ing 0 4V		
-	•						

Section 5 Maintenance

(i) Control and Tim	ing Logic	Test Point	Signal	
Instrument in STORE	mode at 0.5 ms/cm	U825a pin 1	200Hz ramp from 0V to 3.5V	
Test Point	Signal (TTL Levels	U830a pin 8	200kHz clock with even mark/space	
1 = TTL high level) 0 = TTL low level)		U830a pin 5	200Hz ramp from 0V to 3.5V	
U807 pin 9	1	(m) Sampling Circuit	гу	
U804a pin 3	50ns Negative-going pulse	Instrument in STORE	mode at 20µs/cm	
U805c pin 8	50ns Negative-going pulse	Test Point	Signal	
U806a pin 6 50ns Positive-going pulse		U903 pin 1	2.5V analogue ramp at sweep rate	
U801e pin 10	20MHz Clock		selected on TIME/CM switch	
U802a pin 3	20MHz Clock	U903 pin 2	2.5 digital ramp at 200Hz rate	
U8066 pin 8	2MHz Clock with even mark/space	U903 pin 4	0 to 4V when slow ramp crosses	
U803c pin 8	50ns Positive-going pulse		fast ramp	
U807 pin 11 100ns Positive-going pulse U807 pin 7 1		U804d pin 11	50ns pulses at Trigger rate, when updating the Store, after ARM,	
			before STORED indication	
			lights.	
(j) Store Control				
Instrument in STORE	mode at 0.5ms/cm			
Test Point	Signal (TTL logic levels	5.4 SETTING UP PE	ROCEDURE	

The following procedure details the adjustments necessary to recalibrate the OS1420 and set all the preset controls to achieve the specified performance. Inability to make these adjustments or failure to meet the specification after those adjustments have been made should be considered as a fault and the operating conditions should be checked according to section 5.3.

Set instrument initially in NORMAL mode.

- Test Equipment
  - 1. Multirange Test Meter including 2.5kV capability at  $20k\Omega/V$ .
  - 2. Variable Autotransformer, output voltage 100-170V at 5A.
  - 3. Sine/square wave signal generator, 10Hz to 100kHz, 20mV -5V.
  - 4. Source of voltage and time calibration signals, such as Bradley Oscilloscope Calibrator type
  - 5. Square wave generator, 500kHz, 100mV into  $50\Omega$ , rise time less than 50ns with square corner and flat top.
  - 6. RF Sinewave, Constant Amptitude Signal Generator. 25mV to 5V pk/pk 50kHz to 15MHz.
  - 7. 10:1 passive probe (PB12 or PB13).

### Set E.H.T.

Set the incoming a.c. supply via the auto-transformer to the nominal centre voltage of the selected range. Set to mid brilliance on the c.r.t. Monitor the collector voltage of TR707. Adjust R725 for this voltage to be +405V +5V. Remove the voltmeter. The instrument may now be operated directly from the uncontrolled supply.

Test Point	Signal (TTL logic levels  1 = TTL high level  0 = TTL low level)
U831 pin 46	1
U831 pin 48	200kHz clock even mark/space
U831 pin 27	Two 250ns Negative-going pulses every 5µs
U831 pin 47	1 during ramp 0 during hold-off
U831 pin 52	20µs positive-going pulse every 5ms
U831 pin 18	$5\mu$ s negative-going pulse every $5$ ms
U817 pin 21 U816 pin 1	Same as U831 pin 27
U816 pin 11	2 250ns positive-going pulse every 5µs

### (k) Digital to Analogue Converter

Instrument in STORE mode at 0.5 ms/cm

Test Point	Signal (TTL logic levels unless otherwise specified)
U834 pin 11	200kHz clock
U819 pin 11	200kHz clock
U820 pin 13	+6.2V
U827a pin 1	3.9V D.C. level Sensitivity 70mV/cm
U827d pin 14	3.9V D.C. level Sensitivity 70mV/cm

### (l) Digital Ramp Generator

Instrument in STORE mode at 0.5 ms/cm

Test Point Signal

U831 pin 23 200Hz clock with even mark/space

### Set Intensity Range

Set to X-Y mode with inputs grounded and centre the spot on the screen. Monitor the collector voltage of TR702. Adjust the intensity control for this voltage to be +15V and then adjust R713 for the intensity of the spot to be near cut off. Remove the voltmeter.

#### d. Astigmatism

Display a mid-frequency sinusoidal signal in the normal sweep mode on one channel, approx 2cm pk. to pk and 4cm period. Set the Variable sensitivity control fully anticlockwise. Set to a fairly low brilliance and adjust both the Focus control and R708 (Astig.) for the sharpest trace over the whole of its length. Reset the Variable sensitivity to Cal.

#### e. Trace Rotation

Ground the input and set the horizontal trace to the centre line. Adjust the Trace Rotation preset control to align the trace with the centre graticule line.

### f. Input Balance

Select CH1 and with the input grounded, adjust the preset Bal. control for no vertical movement of the trace between the 0.1V/cm and the 0.2V/cm ranges. Repeat for CH2.

### g. Trigger Balance

Set R357 for no vertical movement of the channel 2 trace when Invert is selected. Connect a sinusoidal input, AC coupled, to CH1 and set the trace for about 5cm pk. to pk. signal and one cycle displayed Adjust R307 such that there is no change of trigger point as the Trigger Coupling is switched between AC and DC. Note that the relevant shift control may have to be operated to return the trace to the centre of the screen when R357 or R307 are adjusted;

### h. Timebase Calibration

Ensure that the Variable Sweep is set fully clockwise to Cal. Apply 0.1ms calibrated time markers to either channel input. Set the timebase to 0.1ms/cm and obtain a centred triggered trace. Apply X10 Magnification and set R553 for 10cm spacing between the time markers.

Return to X1 Magnification and set R551 for 1cm spacing between markers.

Apply 1 ms/cm time markers and set the timebase to 1 ms/cm. Set R506 for 1 cm spacing between the time markers

All other timebase ranges can be checked for accuracy.

### i. X-Y Calibration

Ensure that the CH1 Variable Sensitivity control is set fully clockwise to Cal. Select X-Y and apply a calibrated 100mV square wave to Channel 1 input. Select 20mV/cm Ground Channel 2. Set R302 for 5cm horizontal trace length.

### Channel 1 Calibration

Select CH1. With 100mV input at 20mV/cm as i. above, set R415 for a 5cm vertical amplitude signal.

All other sensitivity ranges can be checked for accuracy.

k. Ensure that the CH2 Variable Sensitivity control is set fully clockwise to Cal. Transfer the 100mV calibration signal to channel 2 and set to display that channel at 20mV/cm. Set R352 for a 5cm vertical amplitude signal.

All other sensitivity ranges can be checked for accuracy.

### Attenuator Compensation

Apply a square wave input to CH1 at approx. 1V pk. to pk. and 1kHz. Select 0.2V/cm and adjust C101 on the CH1 attenuator assembly to obtain a square-topped displayed pulse. Access is through the screw driver/trim tool hole in the pre-amplifier board.

Repeat for CH2.

### m. Input Capacitance Equalisation

Select 100mV/cm on CHI with the Variable Sensitivity control set fully anticlockwise and monitor a 10V 1kHz square wave via a 10:1 probe. Adjust the capacitive compensation of the probe for a flat-topped displayed pulse. Sclect 200mV/cm, reset the Variable Sensitivity to Cal and adjust C102 for a similar flat top to the pulse. Access is through the screw driver/trim Tool Hole in the pre-amplifier board.

Repeat for Channel 2.

### n. Pulse Response and Bandwidth

Monitor a fast rise square wave input signal to examine the edge in detail on the 20mV/cm and  $0.5\mu\text{s/cm}$  ranges.

Adjust C405 for a flat top following the transition and C402 for the optimum corner to the pulse.

Connect a constant amplitude sinusoidal generator and set the input for 5cm pk. to pk. at 50kHz. Increase the frequency and check that the loss of amplitude is less than 3dB at 20MHz (3.5cm pk. to pk.).

### o Calibrator

Monitor a calibrated 1V pk. to pk. square wave input and set the sensitivity and variable sensitivity controls for a full 8cm pk. to pk. display. Disconnect the external input and connect the Y input to the OS1420 Calibrator output. Adjust R641 for a similar 8cm signal amplitude.

### p. Adjustment of the Y D.A.C. output.

Apply a 100mV square wave input to CH1 and set the CH1 attenuator to 10mV/cm. Set STORE mode, and operate the RELEASE control with the TIME/CM switch set to 0.5ms/cm. Adjust R829 to centre the display on the screen. Adjust R821 so that the upper and lower levels of the display are just on screen at both the upper and lower edge of the screen.

### Adjustment of the A.D.C.

Select STORE mode, CH1 input coupling to DC, TIME/CM switch to 0.5 ms/cm, and set DISPLAY MODE switch to CH1. Apply a 100 mV/cm signal to CH1 and select 20 mV/cm on the attenuators. Adjust R842

so that the display waveform is 5cm in amplitude.

### Adjustment of pickoff board

Set CH1 input coupling switch to GND. Ensure CH1 trigger is selected and BRIGHT LINE is On. Set NORMAL mode, and 0.5ms/cm on the TIME/CM switch. Adjust the CH1 Y shift control to centre the trace on the display. Switch to STORE mode. If a trace displacement occurs, adjust R1325 to bring the trace back to the centre of the screen. Switch back to NORMAL mode and display TRACE to the upper edge of the screen. Return back to STORE mode and adjust R1323 set the trace at the upper edge of the screen, if necessary.

Select DUAL mode on the DISPLAY MODE switch.

Set CH1 and CH2 input coupling to DC. Select a 100mV square wave input for both CH1 and CH2.

Set the attenuator to 20mV/cm. Observe the levels of the two displayed waveforms and adjust R1377 so that the amplitudes of both CH1 and CH2 are identical.

Select CH2 on the DISPLAY MODE switch and set the CH2 input coupling to GND. Set BRIGHT LINE ONE, CH2 TRIGGER and NORMAL mode. Adjust the CH2 Y shift control to centre the trace on the screen. Switch

to STORE mode and adjust R1374 to centre the trace again. Return to NORMAL mode, and shift the trace up to the upper edge of the display. Switch back to STORE mode and adjust R1373 so that the trace is at the upper edge of the screen.

### s. Adjustment of Sampling Circuitry

Select 20µs/cm on the TIME/CM switch. Set the NORM NORMAL/STORE button to STORE, select CH1 on the DISPLAY MODE switch, and CH1 TRIGGER. Set BRIGHT LINE ON and CH1 input coupling to GND.

Set R838 fully anticlockwise. Remove U902 and connect pin 12 of the socket to +5V and Pins 11, 7, 6, 5, 4, 3 to ground. Operate the ARM control. The display will now go blank. Adjust R838 until a trace appears. R838 should be set as near the point which initiates a trace as possible.

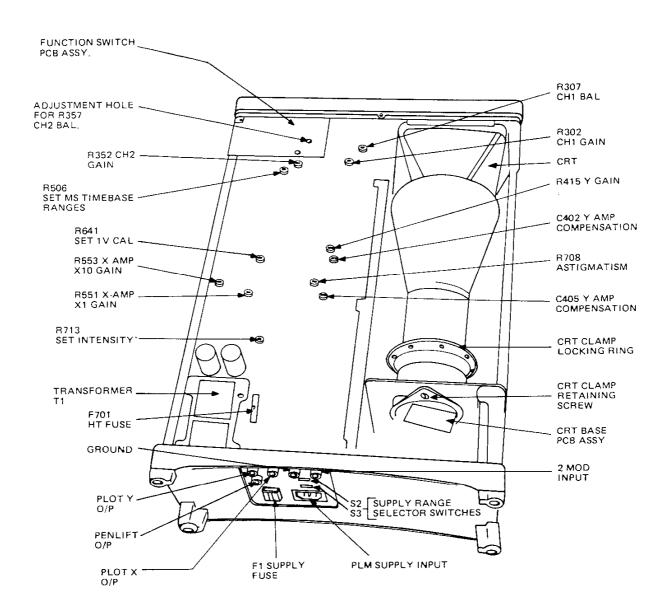
Replace U902.

### t. Digital Timebase adjustment

Apply 1ms markers to CH1 input. Set the TIME/CM switch to 0.1ms. Select STORE mode and operate the RELEASE button. Obtain a centred triggered trace and adjust R834 to obtain 1cm spacing between the markers.

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Fig. 2 Internal Assembly - Top View

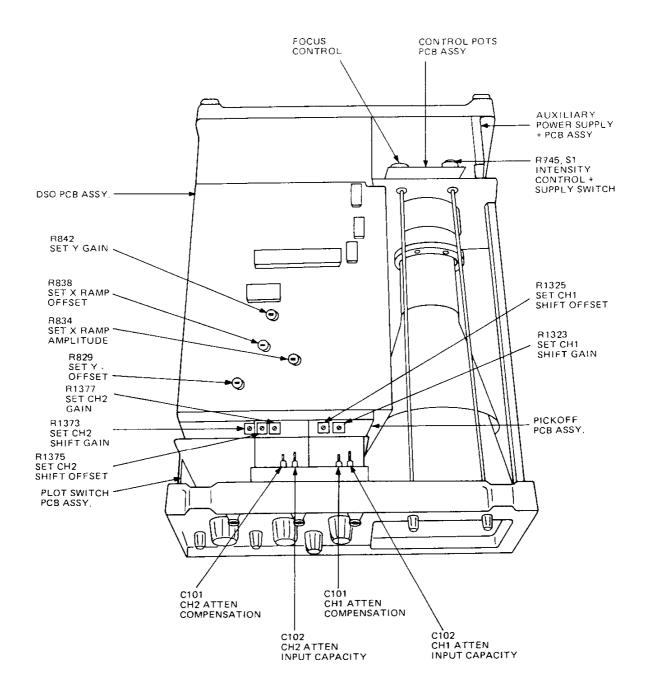


Fig. 3 Internal Assembly - Bottom View

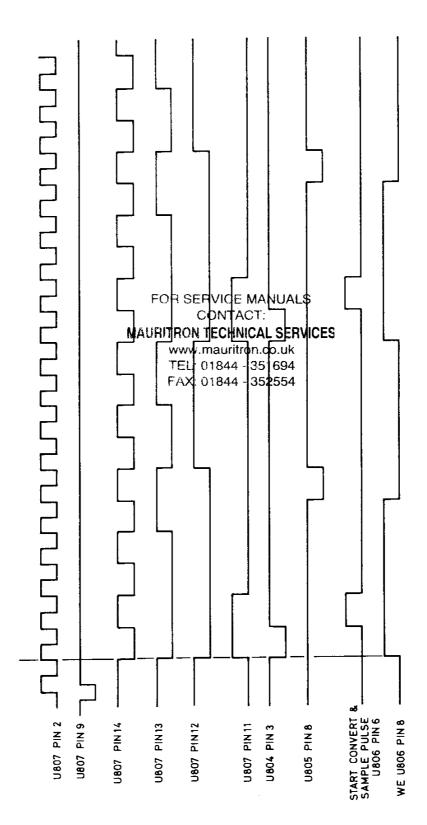


Fig. 4 Control & Timing Logic Waveforms

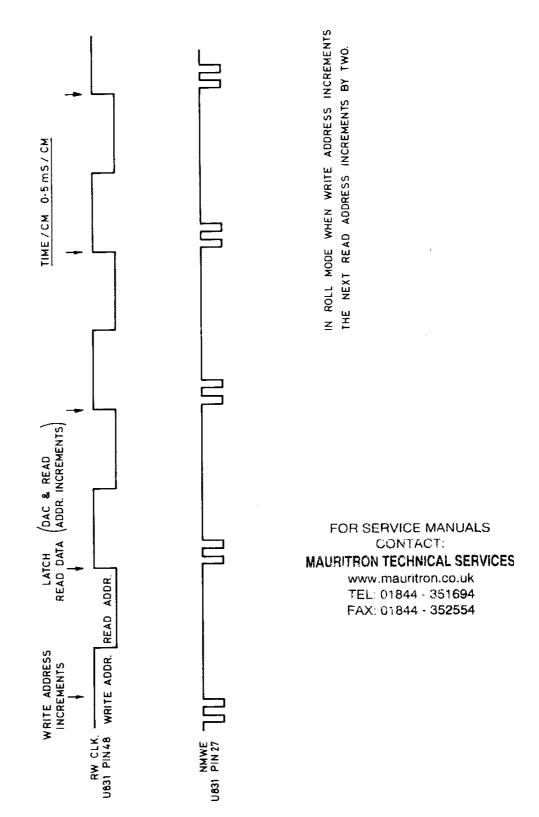


Fig. 5 Store Control Waveforms

### Section 6

#### ABBREVIATIONS USED FOR COMPONENT DESCRIPTIONS

RESISTORS				
CC	Carbon Composition	1/2W	10%	unless otherwise stated
CF	Carbon Film	1/4W	5%	unless otherwise stated
MO	Metal Oxide	1/2W	2%	unless otherwise stated
MF	Metal Film	1/4W	1%	unless otherwise stated
ww	Wire Wound	6W	5%	unless otherwise stated
CP	Control Potentiometer		20%	unless otherwise stated
PCP	Preset Potenitometer Type	MPD, PC	20%	unless otherwise stated
CAPACITORS			+80%	
CE(1)	Ceramic		- 25%	
CE(2)	Ceramic	500V		unless otherwise stated
CE(2)		50V	-1070	unless otherwise stated
CE(3)	Ceramic	30 V		diffess officiwise stated
SM	Silver Mica			1 41
PF	Plastic Film		±10%	unless otherwise stated
PS	Polystyrene			
PE	Polyester		±10%	unless otherwise stated
PC	Polycarbonate			
	The state of the state of the section of the sectio		+50%	
E	Electrolytic (Aluminium)		- 10%	
T	Tantalum		+50%	
_			- 10%	

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### Section 6

IN	TFR	CONNE	CTION	DIAGRAM

Ref	Value	Description	Tol %±	Rating	Part No	Ref	Value	Description	Tol %±	Rating	Part No
RESIST	ORS										
R1101	lk	CF			21799	C1106	10nF	CE(3)			450548
R1102	390	CF			28722						
R1103	4k7	CF			21805	DIODES	3				
R1104	10k	CF			21809	D1101					43847
R1105	10k	CF			21809						
R1106	270k	CF			21256	D1401					43847
R1107	330k	CF			32357						
R1108	470k	CF			32330	Q1101		MPS2369	)		36625
R1109	4k7	CF			21805						
						U1101		74C221			451267
R111	10k	CF			21809	U1102		ICM7555	IPA		451317
CAPACI							LANEOU	S		•	
C1101	10nF	CE(3)		25V	450548	S1101					
C1102	10nF	CE(3)		25V	450548	—11 <b>0</b> 6					450750
C1103	10nF	CE(3)		25V	450548						
C1104	470nF	CE(3)			43500	S1401					
C1105	100nF	CE(3)			43498	-1404					450764

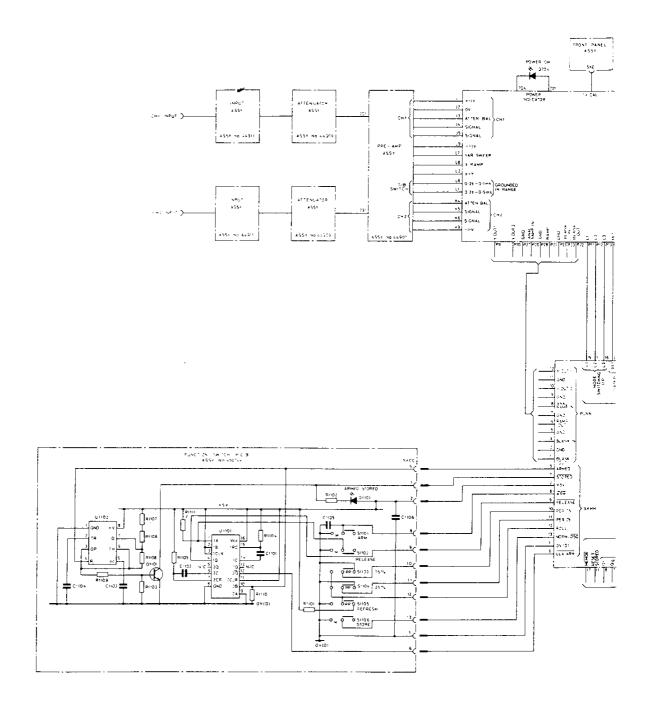
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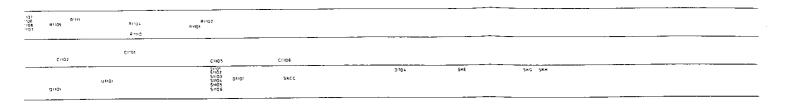
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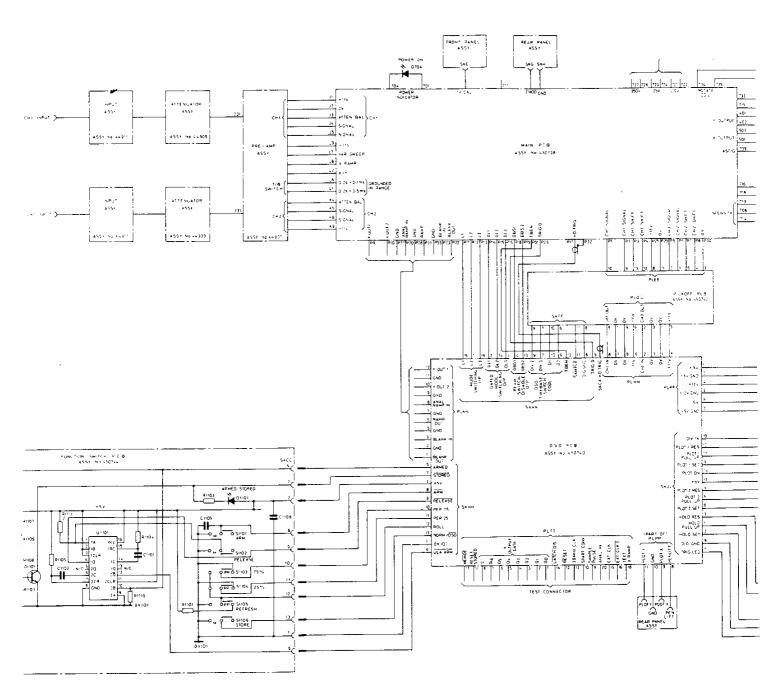
RESIS		B1109	R1107 R1106 R1108 R1101	Ang. Ang	P115 2 Philos		
CAPS	CITE	CNSI	6.103	CTOL	\$1105	C1106	
HISC		Ç.4 <b>0</b> ₹	<b>0</b> 41C1	ענונט	\$1101 \$1102 \$1102 \$1105 \$1105 \$1105 \$1106	SKCC	0104 S4E

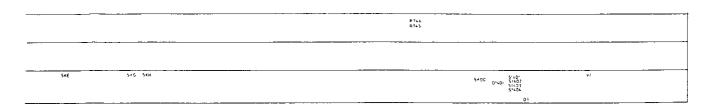


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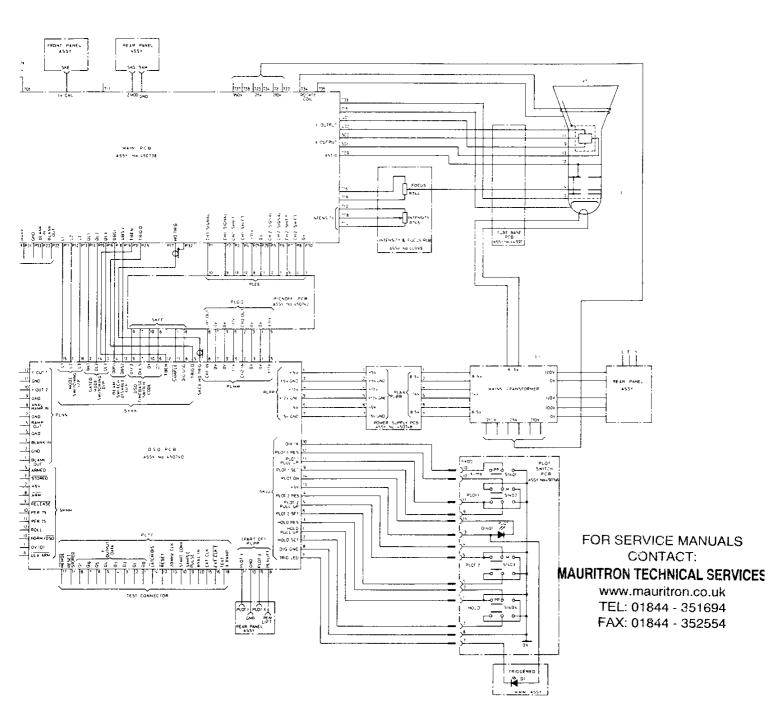


Fig. 6 Interconnection Diagrams

## Section 6

## **Component List and Illustrations**

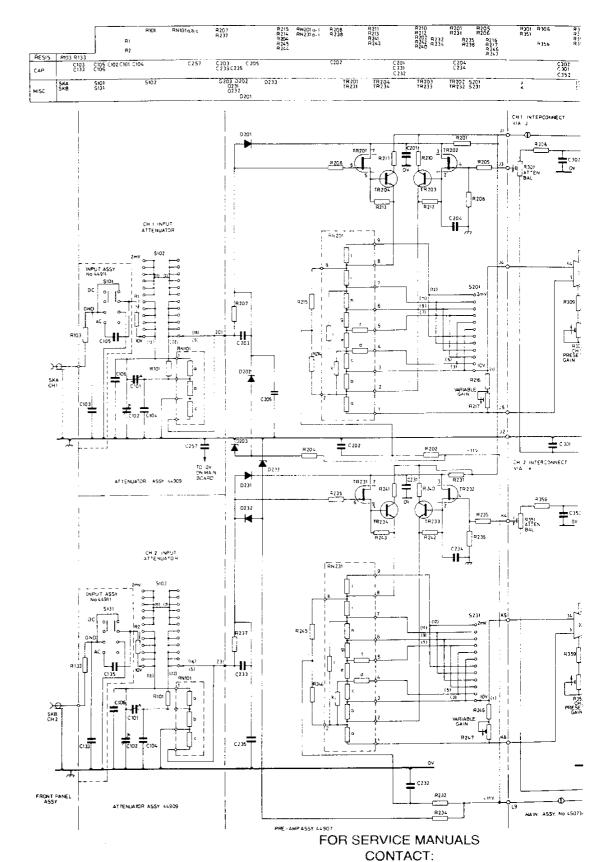
Y AMP	, TIME	ASE & TRIGO	GER								
Ref	Value	Description	Tol %±	Rating	Part No	Ref	Value	Description	To1 %±	Rating	Part No
RESIST		CE			28714	R270	4k7	СР		Δ?	3/451369
R1	47	CF				R271		CP		AJ	451370
R2	47	CF			28714	R271	2k2 47k	CF		1/8W	44242
D 101	27	CE			20211	R272 R273	8k2	CF		1/8W	44234
R101	27	CF			28711		2k2	CP		1/011	451370
	22	0.5			20710	R274	ZKZ	CP			431370
R103	22	CF			28710	D 20.1	101-	PCP			44959
					20710	R301	10k 220	PCP			36262
R133	22	CF			28710	R302	220	rcr			30202
D151	0.01	O.E.		1337	10060	R306	1k	CF			21799
R151	82k	CF		1W	19060	R307	10k	PCP			36267
D001	11.0	OF.			20725	R308	22k	CF			21812
R201	1k8	CF			28725		120	CF	2		38572
R202	10	CF			21793	R309	10	CF	2	;	21793
D204		95			21901	R311	10	CF			21793
R204	1k5	CF			21801	R312					21794
R205	3k3	CF			21803	R313	100	CF			21794
R206	47	CF			28714	R314	100	CF		4.2	3/451371
R207	470k	CC			4906	R315	4k7	CP	2	AS	38606
R208	150	CF			28719	R316	3k3	MF	2 2		38606
					20524	R317	3k3	MF	2		40297
R210	820	CF			28724	R318	7k5	CF			40297
R211	510	CF	_		29434	R319	7k5	CF			40297
R212	820	MF	2		38592	Dags	101	non			44959
R213	820	MF	2		38592	R351	10k	PCP			36262
R214	1k5	MF	2		38598	R352	220	PCP			30202
R215	1k5	MF	2		38598	D256	11.	CE			21799
R216	180	CF			21795	R356	1k	CF			36267
R217	4k7	CP			451368	R357	10k	PCP			21812
		0.5			20725	R358	22k	CF	2		38572
R231	1 k8	CF			28725	R359	120	MF	2		21793
R232	10	CF			21793	R361	10	CF CF			21793
B004	,, ,,	65			21801	R362 R363	10 100	CF			21794
R234	1k5	CF			21801	R364	100	CF			21794
R235	3k3	CF			28714	R365	4k7	CP		Δ3	/451371
R236	47	CF			4906	R366	3k3	MF	2	11.0	38606
R237	470k	CC			28719	R367	3k3	MF	2		38606
R238	150	CF			20/19	R368	7k5	CF	-		40297
D2.40	020	CE			28724	R369	7k5	CF			40297
R240	820	CF CF			29434	R401	2k2	MF	2		38602
R241 R242	510		2		38592	R401	2k2 2k2	MF	2		38602
	820	MF MF	2 2		38592	R402	2k2 2k2	CF	_		21802
R243	820		2		38598	R403	2k2	CF			21802
R244	1k5 1k5	MF MF	2		38598	R404	2k7	MF			38604
R245 R246	180	CF	2		21795	R406	47	CF			28714
	4k7	CP			451368	R407	2k7	MF	2		38604
R247	4K /	Cr			431300	R407	1k5	CF	-		21801
R261	10	CF			21793	R409	1k5	CF			21801
	470	CF			21797	R410	1k8	CF			28725
R262 R263	470 4k7	CF CF			21797	R411	1 k8	CF			18553
K203	4K /	CI.			21005	R411	390	MF	2		38584
R265	1k	CF			21799	R413	1k8	CF	_	1/2W	18553
	1k	CF			21799	R413	390	MF	2	,	38584
R266 R267	1 K 10	CF CF			21793	R414	100	PCP	2		36261
R268	100	CF CF			21793	R415	47	CF			28714
R269	47k	CP CP		Δ?	3/451367	R410 R417	150	MF	2		38574
11207	T / IL	Ç.		110	,	Y 1 (	100	4144			'

Y AMP	, TIMEBASI	E & TRI	GGER (Cont	:.)							
Ref		escription		Rating	Part No	Ref	Value	Description	Tol %±	Rating	Part No
RESIST	ORS (Cont.)										
R418	270	MO			26742	R532	180	CF			21795
R419	10	CF			21793	R533	1k2	CF			21800
						R534	6k8	CF			21807
R421	10	CF			21793	R535	680	CF			28723
R422	270	MO			26742	R536	10	CF			21793
R423	100	CF			21794	R537	10	CF			21793
R424			A.O.T.			R538	10	CF			21793
R425	100	MF	2		38570	R539	470	CF			21797
R426	120	CF			28718						
R427	120	CF			28718	R541	1k8	CF			28725
R428	22	CF			28710	R542	47	CF			28714
R429	39k	CF		1 W	19056	5.5		0.5			21707
D 422	22	or.			20710	R544	470	CF	4 O T	•	21797
R432	22	CF			28710	R545	2k7	CF	A.O.T.		28726 21807
R433	47	CF	-		28714	R546	6k8	CF			21807
R434	47	CF	5		28714	R547	2k2	CF			21802
D 427	100	CE			21794	R548	8k2	CF CF			21807
R437	100 100	CF CF			21794	R549	6k8	Cr			21007
R438 R439	270	CF		1 W	19036	R551	1 k	PCP			36264
R440	270	CF		1 W	19036	R552	5k6	CF			21806
R441	270	CF		1 W	19036	R553	4k7	PCP			36266
R442	2k2	MO	5	1 ***	44986	R554	680	CF			28723
R443	2k2	MO	5		44986	R555	47	CF			28714
R444	47	CF	-		28714	R556	2k7	CF			28726
R445	47	CF			28714	R557	1k8	CF			28725
		-				R558	10	CF			21793
R503	470	CF			21797	R559	100	CF			21794
R504	56k	CF			28729	R560	68k	CF			21816
R505	27k	CF			21813	R561	100	CF			21794
R506	10k	PCP			36267	R562	10k	CF			21809
R507	4k7	CF			21805	R563	390	CF		14W	18545
R508	4k7	CF			21805	R564	33k	CF			21814
R509	33k	CF			21814	R565	2k2	CF			21802
R510	10	CF			21793	R566	100k	MO		1/337	28822
R511	10k	CF			21809	R567	390	CF		1/2W	18545
R512	33k	CF			21814	R568	22k	CF	2		21812 38587
R515	5k6	CF			21806	R569	510	MF	2 A O T		28727
R514	1k5	CF			21801	R570 R571	15k	CF CF	A.O.T.		28724
R515	1k5	CF			21801 21799	R571	820	CF CF			21812
R516	1k	CF CF			21799	R572	22k 4k7	CF			21805
R517 R518	22k 22k	CF			21812	R574	12k	CF		1W	19051
R519	3k9	CF			21804	R575	12k	CF		1W	19051
R520	10k	CF			21809	R576	10k	MO	5	2.11	44987
R521	lk	CF			21799	R577	10k	MO	5		44987
R522	2k2	CF			21802	11377	101		Ţ.		
R523	4k7	CF			21805	R600	22k	CF			21812
R524	3k9	CF			21804	R601	27k	CF			21813
R525	2k2	CF			21804						
R526	3k9	CF			21802	R603	3k3	CF			21803
R527	680	CF			28723	R604	4k7	CF			21805
R528	680	CF			28723	R605	2k2	CF			21802
R529	1k	CF			21799	R606	27k	CF			21813
R530	56	CF			28715	R607	2k2	CF EOD or	RVICE M	ASHIAL	21802
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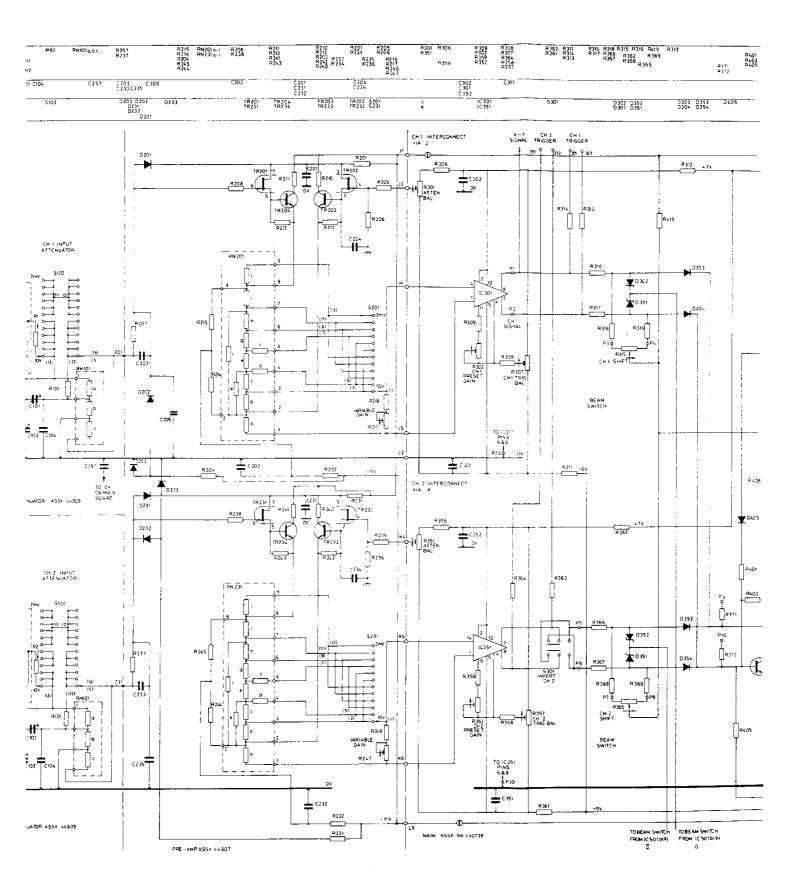
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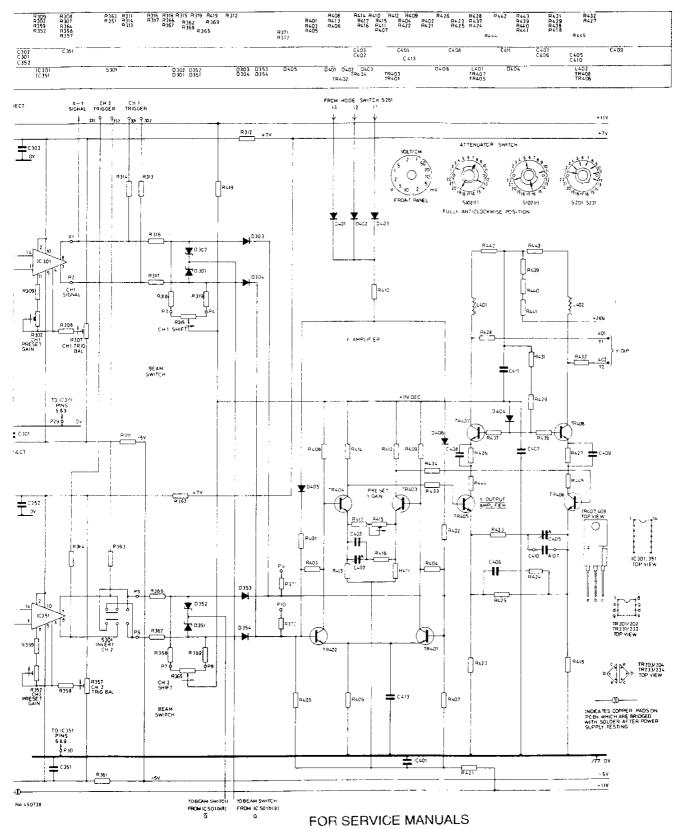
YAMP	. TIMEBASE	& TRIGGER	(Cont.)
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YAIVIP	, I HALER	ASE & IRIGG	EK (CON	c. <i>)</i>							
Ref	Value	Description	To1 %±	Rating	Part No	Ref	Value	Description	Tol %±	Rating	Part No
RESIST	ORS (Con	t.)									
R608	4k7	CF			21805	C133			A.O.T.		
R609	470	CF			21797						
R610	10	CF			21793	C135	100nF	PE		400V	44966
R611	680	CF			28723						
R612	680	CF			28723	C151	6.8p <b>F</b>	SM		500V	22362
R613	68k	CF			21816		•	-			
R614	10	CF			21793	C201	10μF	Е		25V	32180
R615	12k	CF			21810	C202	2.2nF	CE(2)			22389
R616	470	CF			21797	C204	1 n <b>F</b>	CE(3)			42432
R617	2k7	CF			28726			1-(1)			
R618	47k	CF			21815	C231	10μF	E		25V	32180
R619	3k3	CF			21803	C232	10nF	CE(3)		25V	450548
R620	1 M	CF			31840	C233	2.2nF	CE(2)			22389
R621	3k3	MF			21803	C234	1nF	CE(3)			42432
R622	1k8	CF			28725			. ,			
R623	220k	CF			21823	C237	10nF	CE(3)		25V	450548
R624	10	CF			21793			, ,			
R625	1 M	CF			31840	C263	12nF	PS		63V	450536
R626	1 M	CF			31840	C264	$1\mu$ F	PΕ		100V	41743
R627	680k	CF			31839	C265	10nF	CE(3)		25V	450548
R628	1 M	CF			31840	C266	10nF	CE(2)		100V	37018
R629	1 M	CF			31840	C267	10nF	CE(3)		25 <b>V</b>	450548
R630	100k	CF			21819	C268	10nF	CE(3)		25V	450548
R631	33k	CF			21814			•			
R632	300k	MF	2		38653	C301	10nF	CE(3)		25 <b>V</b>	450548
R633	18k	CF			21811	C302	10nF	CE(3)		25V	450548
R634	6k8	CF			21807						
R635	10	CF			21793	C351	10nF	CE(3)		25V	450548
R636	68k	CF			21816	C352	10nF	CE(3)		25 <b>V</b>	450548
R637	2k2	CF			21802						
R638	3k9	CF			21804	C401	10nF	CE(3)		25 <b>V</b>	450548
R639	10k	CF			21809	C402	10/65pH	F TRIMM	ER		30286
R640	39k	CF			28728	C403	15pF	CE(3)			42410
R641	2k2	PCP			36265	C404	120pF	CE(3)			42421
R642	56k	CF		1/2W	19058	C405	1065/pI	F TRIMM	ER.		30286
R643	470	CF			21797	C406			A.O.T.		
R644	3k3	CF			21803	C407	100nF	CE(2)		100V	37018
R645	10k	CF			21809	C408	3.3nF	CE(3)			42438
						C409	3.3nF	CE(3)			42438
RN101		RESISTO	R NETWO	ORK A	3/43194						
						C411	5.6nF	CE(2)		500V	22394
RN201		RESISTO	R NETWO	ORK A	3/44651	C412	15pF	CE(3)	A.O.T.		42410
						C413	InF	CE(3)		50V	42432
RN231		RESISTO	R NETWO	ORK A	13/44651						
						C501	220nF	PE		100V	44370
RN261		RESISTO	R NETWO	JRK A	3/38692	C502	lnF_				42432
						C503	10nF	CE(3)		25V	
						C504	10nF	CE(3)		25 <b>V</b>	450548
CAPACI		20201145	•		450510	0501	10.5	CD(a)			40.400
C101	1/6pF	TRIMMER			450510	C506	10pF	CE(3)		261/	42408
C102	1/6pF	TRIMMER	.O.T.		450510	C507	10nF	CE(3)		25V	450548
C103	490-E	PC A	.U.I.		40631	C508 C509	10nF	CE(3)		25V 16V	450548 450582
C104	680pF			400V			100μF	E CE(2)		101	
C105	100nF	CE(2)		4007	22362	C510 C511	560pF	CE(3)			42429 42438
C106	6.8pF	CE(2)			22302	C311	3.3nF	CE(3)			42430



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Fig. 7 Y Amplifier Circuit Diagram

## Section 6

## **Component List and Illustrations**

Y AMP	Y AMP, TIMEBASE & TRIGGER (Cont.)										
Ref	Value	Description	Tol %±	Rating	Part No	Ref	Value	Description	Tol %±	Rating	Part No
CAPAC	ITORS (Co	nt,)									
C512	6.5nF	CE(2)			22394	TR231	)	DUAL F.I	2 T		44704
C513	$100\mu F$	E		16V	450582	TR232	}	DOAL F.I	2.1.		44704
C514	120pF	CE(3)			42421	TR233	l	A E 20			44627
C515	150pF	CE(3)			42422	TR234	ſ	AE38			44027
C516	150pF	CE(3)			42422						
						TR261		ZTX313			40788
C520	$10\mu$ F	Е		25V	32180	TR262		BC547B			44951
0701	220 E	DE		2501/	20201	TR263		BC558C			44952
C601	220nF	PE CE(2)		250V	39201 42420	TR264		BC558C			44952
C602	100pF	CE(3)		63V	32194						
C603	2.2μF	E		100V	450593	TR401		BF371			36275
C604	2.2μF	E (2)		1004	42412	TR402		BF371			36275
C605	22pF	CE(3)		100V	37018	TR403		BF371		1	36275
C606 C607	100nF 100nF	CE(2)		100V	37018	TR404		BF371			36275
C607		CE(2) PE		100V	44370	TR405		ZTX313			40788
C609	220nF 100nF	CE(2)		100V	37018	TR406		ZTX313			40788
C610	100nF	CE(2)		25V	450548	TR407		BF468			40056
C611	22pF	CE(3)		23 V	42412	TR408		BF468			40056
C612	100nF	CE(3)		100V	37018						
C612	100m	CE(2)		25V		TR501		BC547B			44951
C614	47pF	CE(3)		23.	42416	TR502		MPS2369			36625
C615	100nF	CE(2)		100V	37018	TR503		MPS2369			36625
C616	100m	CE(2)		25V	450548	TR504		BC547B			44951
C617	47nF	CE(2)		100V	39192	TR505		2N3904			24146
C618	47nF	CE(2)		100V	39192	TR506		BC558C			44592
C619	100pF	CE(2)		1001	42420	TR507		BC557B			44590
C620	100Ft	CE(3)		25V	450548	TR508		BC557B			44950
C621	10nF	CE(3)		25V	450548	TR509		BC547B			44951
C622	2.2μF	E E		20,	32194	TPD 611		0210004			24146
C623	3.3pF	CE(3)			36600	TR511		2N3904			24146
0020	J.5p1	CE(3)				TR512		2N3906			21533
C701	10nF	CE(3)		25V	450548	TR513		NSD459			40054 40054
C702	2.2nF	PE PE			44/44990	TR514		NSD459			450226
C703	2.2nF	PΕ			44/44990	TR515		BF393			430220
C704	1000μF			40V	44992	TR601		BC558C			44952
C705	33μF	Ē		350V	44991	TR602		BC558C			44952
0,00	00,41	_				TR603		BC547B			44951
C708	10μF	E		25V	32180	TR605		BC557B			44950
C709	2.2nF	PE		4kV A	4/44990	TR605		2N3904			24146
C710	10μF	É		25V	32180	TR606		2N3904			14146
C711	100nF	PE		1.5kV	40075	TR607		2N3906			21533
C712	100nF	PE		1.5kV	40075						
C713	220nF	PE		100V	44370	TR701		TJ630			44953
C714	10nF	CE(3)		25 <b>V</b>	450548	TR702		BFR86B			44954
C715	220nF	PE		100V	44370	TR703		BFR86B			44954
C716	10nF	CE(3)		25V	450548	TR704		BC558C			44952
C717	56pF	CE(3)			42417						
C718	22pF		A.O.T.		42412	TR706		BC547B			44951
C719	5.6nF	CE(2)			22394	TR707		BUX87			44955
TRANSI	STORS					TR709		BC328			38414
TR201	Ì	DUALE	e m		44704						
TR202	j	DUALF	.E.I.		<del>17</del> /07	TR711		BC558C			44952
TR203		A E 29			44627	TR712		TIP29A			38419
TR204	J	AE38			77041	TR713		TIP112			40591

## Section 6

OS1400/1420 Y AMP, TIMEBASE & TRI	GGER (Cont.)
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	US1400/1420 F AMIF, TIMEBASE & TAIGGET (COIIC)										
Ref	Value	Description	To! %±	Rating	Part No	Ref	Value	Description	To! %±	Rating	Part No
TRANSI	STORS (Co	nt.)									
TR714		BC547B			44951	D601		IN4148			23802
TR715		BC557B			44950	D602		IN4148			23802
TR716		2N6518			36472	D603		IN4148			23802
11/10		4110310			30472	D604		IN4148			23802
						D605	5 <b>V</b> 6	ZENER			33929
DIODES	<b>i</b>	13.125.05			20220		3 4 0				
D201		IN3595			29330	D606		IN4148			23802
D202		IN3593			29330	D607		IN4148			23802
D203	6V8	ZENER			33931	D608		IN4148			23802
						D609	47V	ZENER			40049
D231		IN3595			29330	D610		IN4148			23802
D232		IN3595			29330	D611		IN4148			23802
D233	6V8	ZENER			33931						
D301		ZC2811H			40352		RATED CI				
D302		ZC2811H			40352	IC261		LF351			40130
D303		IN4148			34701						
D304		IN4148			34701	IC301		LM733CN			40084
D304		1114140			34701						
D251		7.0001111			10252	IC351		LM733CN			40084
D351		ZC2811H			40352						
D352		ZC2811H			40352	IC501		74LS74N			36732
D353		IN4148			34701			, , , , , , , , , , , , , , , , , , , ,			
D354		IN4148			34701	IC552		LM78L05	A C 7.		40406
						10332		EM70E05	102		10100
D401		IN4148			23802	IC601		MC3401P			40061
D402		IN4148			23802	IC601		LM710CN			40083
D403		IN4148			23802	10002		LM/TOCK			40003
D404	5V I	ZENER			33928	10201		140501.10	. OD		10070
D405		IN4148			34701	IC701		MC78L12			40060
D406		IN4148			34701	IC702		LM341P15	5		40059
D 100		11111110			3.701						
D501		IN4148			23802		LANEOUS	\$			
D502		OA47			4468	L401	$15\mu H$				44993
D502		IN4148			23802	L402	15μΗ				44993
D503					23802						
		IN4148			23802			****			
D505		IN4148				S1		WIT	H R745		4/44461
D506		IN4148			23802	<b>S</b> 2					<b>\</b> 4/4069
D507		IN4148			23802	S3				A	44/4069
D508		IN4148			23802						
D509		IN4148			23802	S101				A	1/44965
D510		IN4148			23802	S102					44978
D511		IN4148			23802						
D512		IN4148			23802	S131				A4	1/44965
D513		IN4148			23802						
D514		IN4148			23802	S201					450294
D515		IN4148			23802	5201					
D516		IN4148			23802	S231					450294
D517		IN4148			23802	0251	FOF	R SERVICE N	AANRTAI		1502)
D518		IN4148			23802	S261	, 0,				1/44476
D516 D519		IN4148			23802			CONTAC	<i>i</i> 11:		
						S262	MAURITI	RON TECHNIC	CAL SER	VICES <sup>4/</sup>	430700
D520	CVIO	IN4148			23802		14	/ww.mauritro	n co ub		
D521	6V2	ZENER			33930	S301				A4	1/38729
D522		IN4148			23802			EL: 01844 - :			
D523		IN4148			23802	S501	F	AX: 01844 - :	352554		
D524		ZC2811H			40352	-506					1/38728
D525		ZC2811H			40352	S507				<b>A</b> 4	1/38729

### Section 6

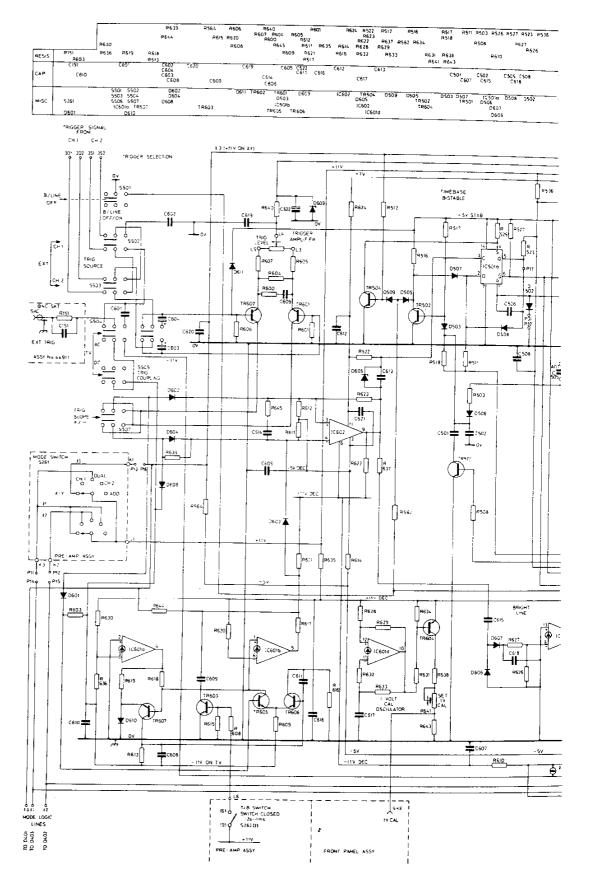
Y AMP	Y AMP, TIMEBASE & TRIGGER (Cont.)											
Ref	Value	Description	Tol %±	Rating	Part No	Ref	Value	Description	To/ %±	Rating	Part No	
SKA	LANEOL	JS (Cont.)			1222 1222	SKE					31229	
SKB SKC SKD					1222 1222 37293	F1	250mA 500mA		V SUPPLY V SUPPLY		33684 33685	

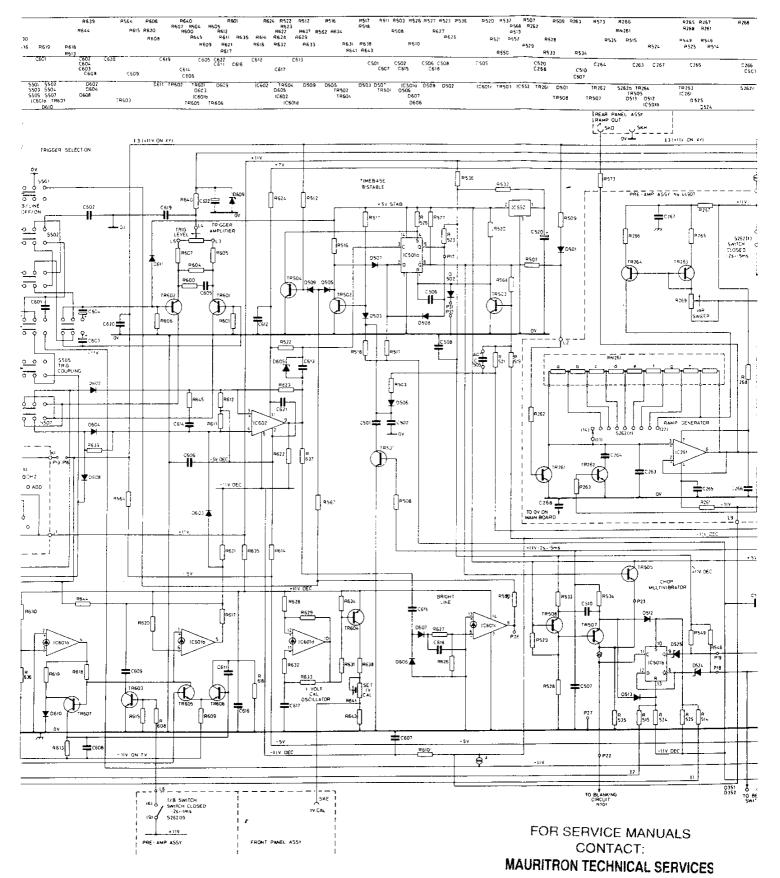
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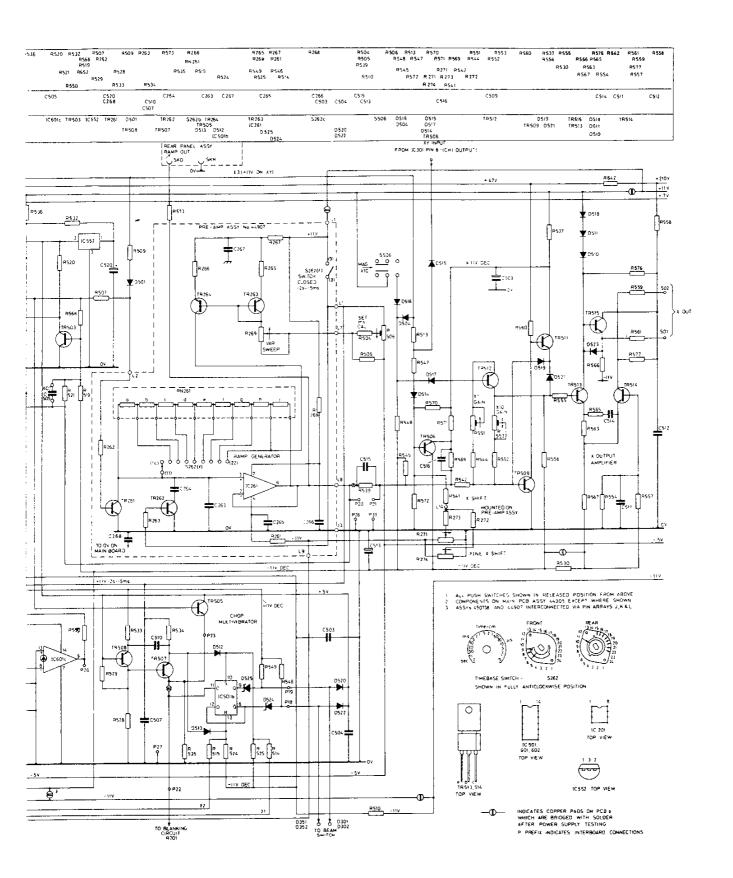


Fig. 8 Timebase and Trigger Circuit Diagram

### Section 6

## **Component List and Illustrations**

PICK-O	FF CIR	CUIT									
Ref	Value -	Description	Tol %±	Rating	Part No	Ref	Value	Description	Tol %±	Rating	Part No
RESISTO	ORS										
R1301	47	CF			28714	R1374	220k	CF			21823
R1302	47	CF			28714	R1375	100k	CP			42167
R1302	1k	ČF			21799	*****		•-			
R1303	150	CF			28719	R1376	470	CF			21797
R1305	150	CF			28719	R1377	1k	CP			35898
					28720	1(15//	110	0.			
R1306	270	CF				D 1 200	41-7	CF			21811
R1307	270	CF			28720	R1380	4k7	Cr			21011
R1309	15k	CF			28727	CAPACI				0.517	450540
R1310	15 k	CF			28727	C1301	10n <b>F</b>	CE(3)		25V	450548
R1311	100k	CF			21819	C1302					
R1312	100k	CF			21819						
						C1304	10nF	CE(3)			450548
R1314	1k5	CF			21801	C1305	100nF	CE(3)		:	43498
1(1517	110	C1			21001	C1206	10nF	CE(3)		25V	450548
21216	21-2	CE			21803	C1307	10μF	E		25V	32180
R1316	3k3	CF			28714	C1308	10μF	Ē		25V	32180
R1317	47	CF				C1308	100nF	CE(3)		201	43498
R1318	220	CF			21796					25V	450548
R1319						C1310	10nF	CE(3)		23 V	430340
R1320	18k	CF			21811	91951	250 5	an(a)			12.425
R1321	18k	CF			21811	C1351	270pF	CE(3)			42425
R1322	22k	CF			21812	C1352					
R1323	47k	CP			42166	C1353	270pF	CE(3)			42425
R1324	220k	CF			21823						
R1325	100k	CP			42167	C1355	100nF	CE(3)			43498
R1326	100k	ČF			21819	C1356	10nF	CE(3)		25V	450548
R1327	100k	CF			21819			• •			
K1527	TOOK	CI			21017	Q1301		2N5771			38089
D 1 2 6 1	17	CE			28714	Q1302		2N5771			38089
R1351	47	CF			28714	21002					
R1352	47	CF				Q1304		MPS2369			36625
R1353	1k	CF			21799	Q130 <del>4</del>		WII 32307			30023
R1354	220	CF			21796	01251		2N5771			38089
R1355	220	CF			21796	Q1351					38089
R1356	270	CF			28720	Q1352		2N5771			
R1357	270	CF			28720	Q1353		MPS2369			36625
R1358	4k7	CF			21811	Q1354		MPS2369			36625
R1359	15k	CF			28727	Q1355		MPS2369			36625
R1360	15k	CF			28727						
R1364	1k5	CF			21801	DIODES		IN14140			23802
1(1504	IKJ	C.			•1001	D1301		IN4148			
D1266	21. 2	CF			21803	D1351		IN4148			23802
R1366	3k3 47	CF			28714				_		40.000
R1367						U1301		I.C. TL082	2		451262
R1368 R1369	220	CF			21796						
R1370	18k	CF			21811	MISCELL	ANEOUS	}			
R1370	22k	ČF			21812	S1301				<b>A</b> 4	/450761
R1372	22k	CF			21812						
R1372 R1373	22k 47k	CP			42166	SKFF					38001
N13/3	→ / K	CI			,2100						

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RESIS		R1301 R1302 R1370 R1371 R1351 R1370 R1370 R1371	R1323 R1322 R1373 R1372	R1309 R1324 R1310 R1359 R1374 R1360	R1306 R1325 R1356 R1375	R1304 R1328 R1380 R1328 R13154 R1376 R1358 R1358	R1303 R1329 R1311 R1329 R1353 R1327	R1305 R1355 R1377	
CAPS				C1306 C1307	C1301 C1304	C1309 C1357	C1305 C1355	C135	
MISC					Q1301 Q1351		U1301a U1301b	Q1355 Q1353	0
	SIGNAL PLEETO	R1301		<del></del>	<del></del> .	·	·		
	+ STV PLEE7			•	<del></del>				
	CHI PLEES	R1302		(	Q1301 R1306	R1328		01305 C135	
	SHIFT PLEELS	R1320	CHI SHIFT A1323	R1309 R1324	<b>∤</b> R1325	U1301a	R1311 C1305 +11V	01355	, R
	SHIFT PLEETS	R1321	R1322	QV OFFSET	↓ [	Ι, Τ	21309 -11V		

OV PLEET

SIGNAL PLEE2

CH2 PLEE1

SHIFT PLEES

SHIFT PLEE4

PLEE3

ال م



R1356

## MAURITRON TECHNICAL SERVICES

U 13016

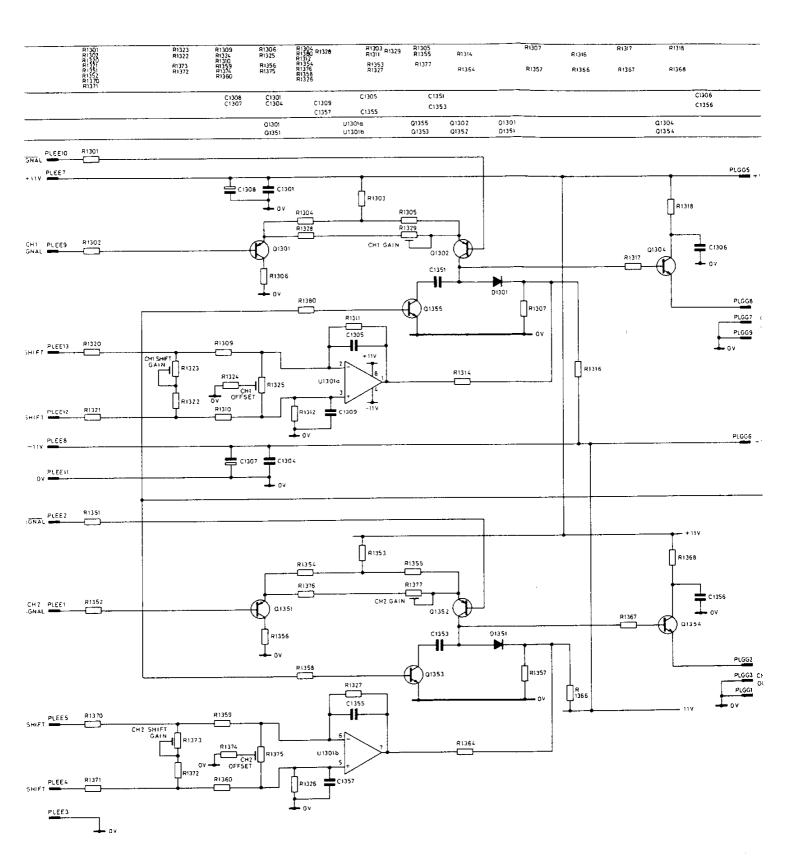
R1326 C1357

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R1353

R1327 C1355 R1355

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C 1310
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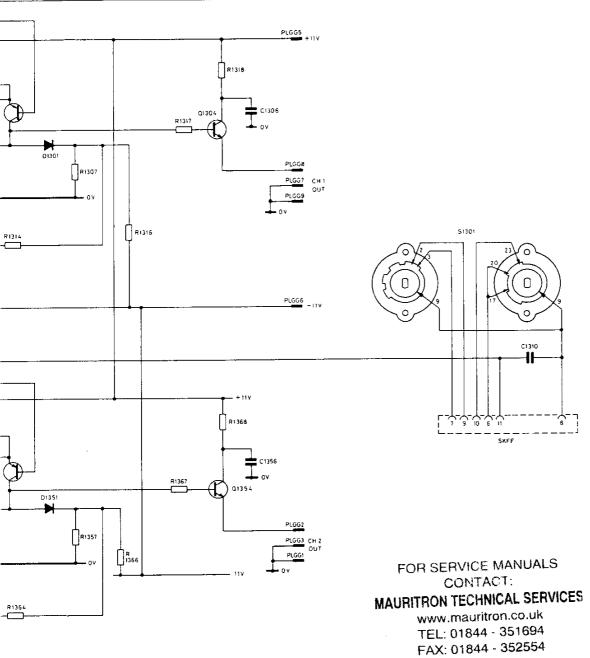


Fig. 9 Pickoff Circuit Diagram

## Section 6

## **Component List and Illustrations**

OS1420	D.S.O.	CIRCUIT									
Ref	Value	Description	Tol %±	Rating	Part No	Ref	Value	Description	Tol %±	Rating	Part No
RESIST	ORS										01010
R801	100	CF			21794	R857	22k	CF			21812
R802	10k	CF			21809	R858	22k	CF			21812
R803	2k2	CF			21802	R859	22k	CF			21812
R804	47	CF			28714	R860	5k6	CF			21806
R805	5k6	CF			21806	R861	22k	CF			21812
R807	1k8	CF			28725	R863	15k	CF			28727
R808	100	CF			21794	R864	15k	CF			28727
R809	1k	CF			21799	R865	4k7	CF			21805
R810	1 k	CF			21799	R866	4k7	CF			21805
R811	390	CF			28722	R867	680	CF			28723
R812	10	CF			21793	R868	680	CF			28723
R813	10	CF			21793	R869	18k	CF		1	21811
R814	100	CF			21794						
R815	47	CF			28714	R871	220	CF			21796
R816	820	CF			28724	R872	47k	CF			21815
R817	5k6	CF			21806	R873	1 k	CF			21799
R818	1k5	CF			21801	R874	47k	CF			21815
R819	3k9	CF			21804						
R820	6k8	ČF			21807	R880	100	CF			21794
R821	10k	CP			36267	R881	15k	CF			28727
R822	180	ČF			21795	R882	15k	CF			28727
R823	3k	MF	5		38605	R883	7k5	MF	2		38615
R824	3k	MF	5 5		38605	R884	7k5	MF	2		38615
R825	3k9	CF	,		21804	R885	560	CF			21798
R826	3k9	CF			21804	R886	6k2	MF	2		38613
R827	5k6	CF			21806	R887	6k2	MF	2 2		38613
R828	5k6	CF			21806						
R829	470	CP			36263	R891	10k	CF			21809
R830	220	CF			21796						
R831	220	CF			21796	R901	100	CF			21794
R832	100	CF			21794	R902	10k	CF			21809
R833	820	CF			28724	R903	2k2	CF			21802
R834	470	CP			36263	R904	47	$\mathbf{CF}$			28714
R835	1k5	CF			21801	R905	5k6	CF			21806
R836	1k5	CF			21801						
R837	18k	CF			21811	R907	1k8	CF			28725
R838	10k	CP			36267	R908	100	CF			21794
R839	18k	CF			21811	R909	1k	CF			21799
R840	560	CF			21798	R910	1 k	CF			21799
R841	5k6	CF			21806	R911	390	CF			28722
R842	220	CP			36262	R912	470	CF			21797
R843	390	CF			28722	R913	120	MF	2		38572
R844	6k2	MF	2		38613						
R845	6k2	MF	2		38613	R915	120	MF	2		38572
R846	6k2	MF	2		38613	R916	1k2	MF	2		38596
R847	620	MF	2		38589	R917	120	MF	2		38572
R848	18k	CF	2		21811	R918	1k2	MF	2		38596
R849	22k	CF			21812	R919	10k	CF			21809
R850	22k 100k	CF CF			21819	R920	4k7	CF			21805
R851	330	CF			28721	R921	330k	CF			32357
R851	100k	CF			21819	R922	5M6	CF			33260
R852 R853		CF			21811	R923	2M7	CF			30758
R854	18k 330	CF CF			28721	R924	1M5	CF	10		40729
K034	220	Ct.			20,21	R925	680k	CF			31839
R856	22k	CF			21812	R926	150k	CF			21821
KOOO	ZZK	CI.			21012	, 20					

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## Component List and Illustrations CONTACT: Section 6

OS1420 D.S.O. CIRCUIT (Cont.)

1

4468

4468

23802

0A47

0A47

IN4148

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Ref	Value	Description	Tol %±	Rating	Part No	Ref	Value	Description	Tol %±	Rating	Part No
RESIST	TORS (Con	t.)									
N801	10k	Resistor	Network		450452	C853					
N802	10k	Resistor	Network		450452	C854	47nF	CE(3)			43497
N803	4k7		Network		39225	C855	100nF	CE(3)			43498
N804	10k		Network		450452	C856	$2.2\mu F$	E		63V	32194
						C857	10μF	Ε		25V	32180
CAPAC	CITORS					C858	100nF	CE(3)			43498
C801						C859	10nF	CE(3)		25 <b>V</b>	450548
C802						C860	100nF	CE(3)			43498
C803	220pF	CE(2)			35914	C861	10nF	CE(3)		25V	450548
C804	10nF	CE(3)		25 <b>V</b>	450548	C862	100nF	CE(3)			43498
C805	10nF	CE(3)		25V	450548	C863	10nF	CE(3)		25V	450548
C806	10μF	E		25V	32180	C864	1nF	CE(3)			42432
C807	10μF	Ē		25V	32180	C865	10nF	CE(3)		: 25V	450548
0007	TOM	L		20.	02.00	0000		02(0)			
C809	$10\mu F$	E		25V	32180	C901					
C810	10μF	Ē		25V	32180	C902					
C811	10nF	ČE(3)		25V	450548	C903	220pF	CE(2)			35914
C812	10μF	E E		25V	32180	C904	10nF	CE(3)		25V	450548
C813	10nF	ČE(3)		25V	450548	C905	10nF	CE(3)		25V	450548
C814	10μF	E		25V	32180			( )			
C815	10nF			25V	450548	C907					
C816	10μF	E		25V	32180	C908					
	2 - 1	<del></del>				C909	10nF	CE(3)		25 <b>V</b>	450548
C818	10nF	CE(3)		25V	450548	C910	47nF	CE(3)			43497
C819	10nF	CE(3)		25V	450548	C911	220pF	CE(3)			42424
00-7	- 4	0-(0)					,	,			
C821	1nF	CE(3)			42432						
C822	2.2nF	CE(3)			42436	DIODES					
C823	100nF	CE(3)			43498	D801	2V7	ZENER			33921
C824	10nF	CE(3)		25V	450548	D802	2V7	ZENER			33921
C825	10nF	CE(3)		25V	450548	D803		ZC2811H			40352
C826	1 nF	CE(3)		-	42432	D804		ZC2811H	1		40352
0020		(-)			-	D805		IN4148			23802
C829	100pF	CE(3)			42420	D806		IN4148			23802
C830	5.6pF	CE(3)			42405	D807		IN4148			23802
C831	100nF	CE(3)			43498	D808		IN4148			23802
C832	100nF	CE(3)			43498	D809		IN4148			23802
						D010					

D827

D828

D829

25V

450548

25V 450548

25V 450548

C850

C851

C852

10nF

10nF

10nF

CE(3)

CE(3)

CE(3)

### Section 6

D.S.O.	CIRCUI	T (Cont.)									
Ref	Value	Description	Tol %±	Rating	Part No	Ref	Value	Description	Tol %±	Rating	Part No
DIODES	S (Cont.)										
D830		IN4148			23802	U812		4011			34953
						U813		74LS51			43676
D901	2V7	ZENER			33921	U814		4044			44024
D902	2V7	ZENER			33921	U815		TCD100	1 <b>J</b>		450682
D903		ZC2811H			40352	U816		74SC374			451265
D904		ZC2811H			40352	U817		HM6116	P-3		450683
D905		IN4148			23802	U818		DAC10			451264
D906		IN4148			23802	U819		74C374			451266
						U810		DAC08			450686
D909		IN4148 :			23802	U821		4053			41891
						U822		4049			36200
Q801		DUAL FE	T		44704	U823		4011			34953
Q802		2N5771			38089	U824		74C00		:	451282
Q803		MPS2369			36625	U825		TL082			451262
Q804		MPS2369			36625	U826		4049			36200
Q805		MPS2369			36625	U827		TL084			451261
Q806		2N3906			21533	U828		74LS123	i		41084
Q807		2N3906			21533	U829		74ALS04	1		451301
Q808		2N3906			21533						
Q809		2N3906			21533	U831		MT7009-	·1		450600
Q810		2N3906			21533	U832		74LS26			44362
Q811		MPS2369			36625	U833		4011			34953
Q812		MPS2369			36625	U834		74C374			451266
Q813		MPS2369			36625	U835		74ALS74	Į.		451308
Q814		MPS2369			36625	U836		74C74			451290
Q815		2N3906			21533	U837		74C00			451282
						U838		74C74			451290
Q901		DUAL FE	T		44704	U902		4520			450914
Q902		2N5771			38089	U903		NE521			44886
Q903		MPS2369			36625	0903		140321			77000
Q904		MPS2369			36625	U904		74ALS74	1		451308
Q905		MPS2369			36625						
U801		74ALS04			451301						
U802		74ALS00			451299		LANEOUS				11150607
U803		74ALS00			451299	T801					4/450687
U804		74LS00			36730	T901					4/560687
U805		74LS10			36867	XL801		CRYSTA	L 20MHz		450688
U806		74ALS74			451308						
U807		74LS162			450681	SKHH					450771

37694

36730

SKJJ

SKKK

4081

74LS00

U808

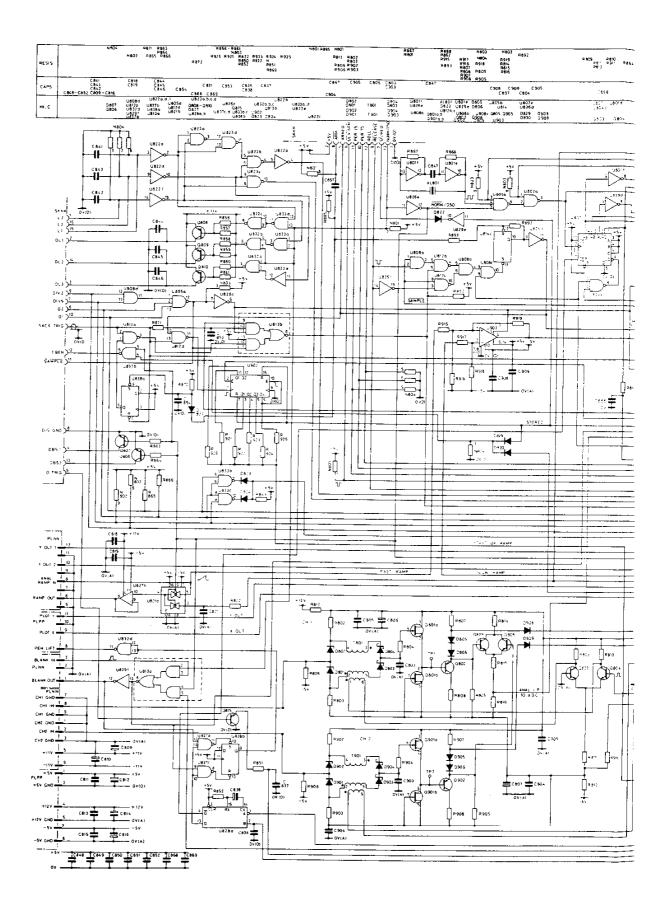
U809

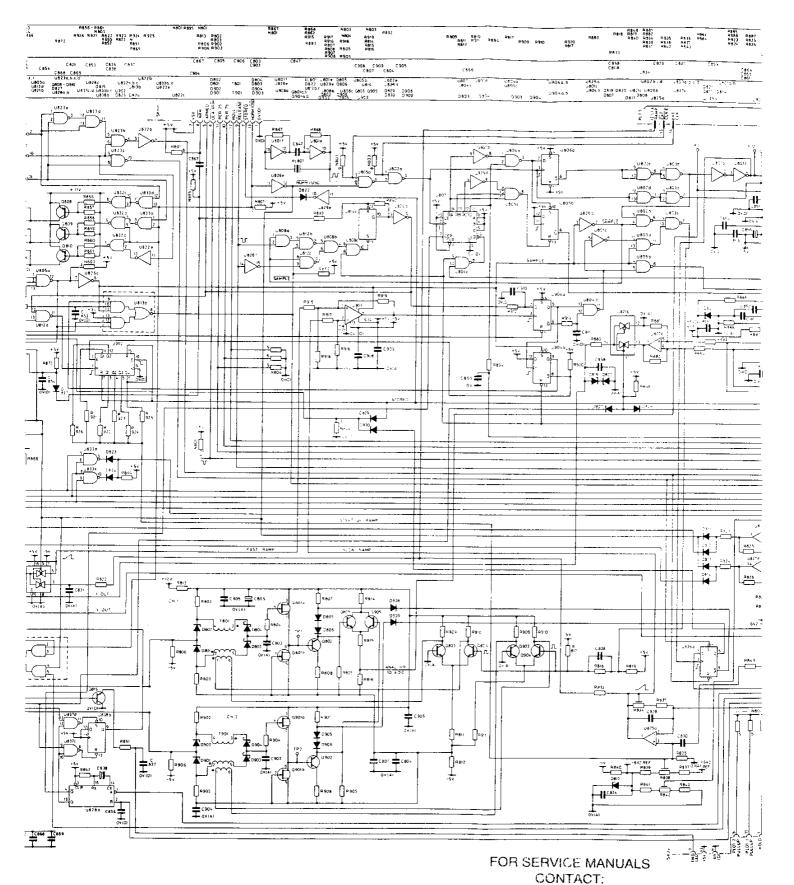
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450771

38001





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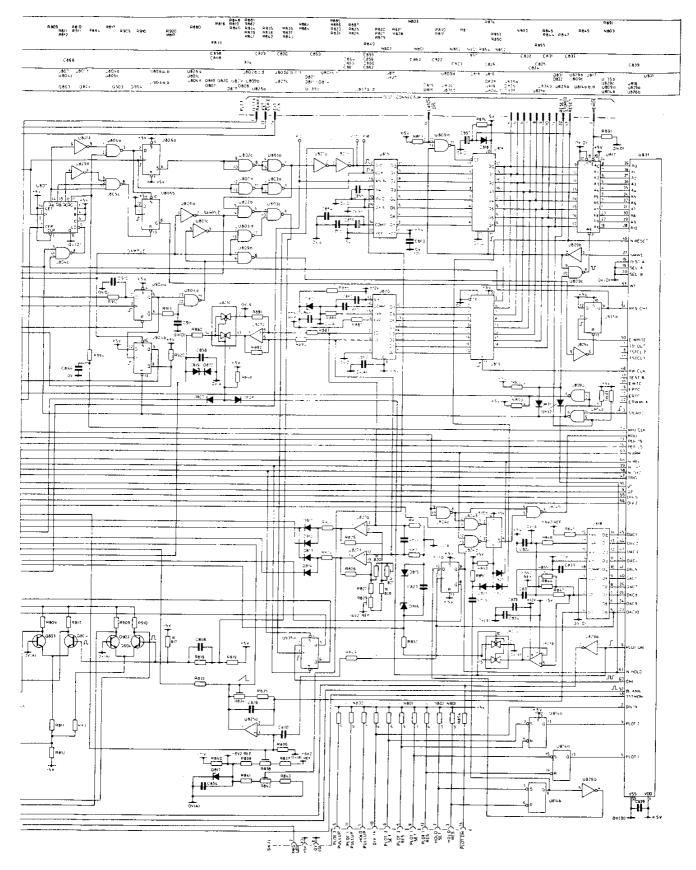


Fig. 10 Digital Storage Circuit Diagram

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TEL 01844 351694

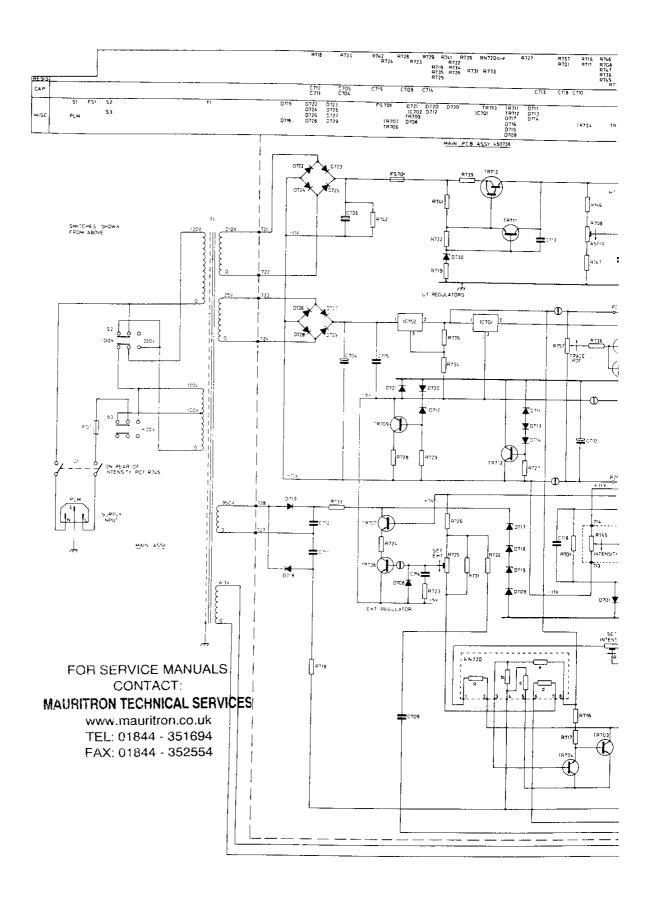
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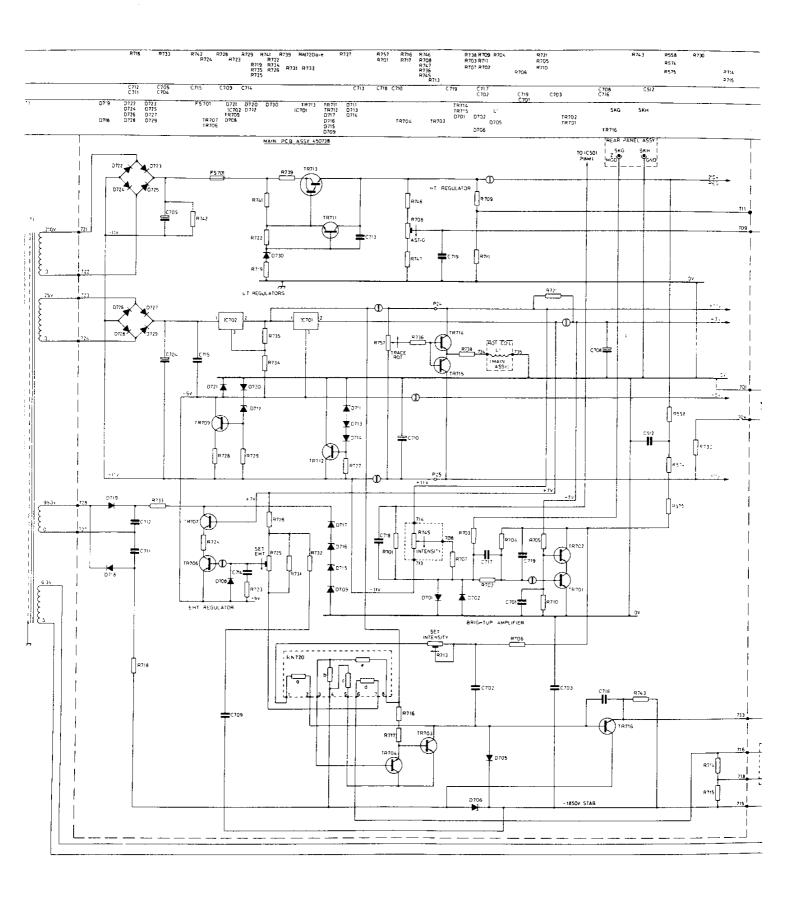
### Section 6

POWE	R SUPPL	Y AND CRT	-								
Ref	Value	Description	To/ %±	Rating	Part No	Ref	Value	Description	Toi %±	Rating	Part No
RESIST	rons										
R701	1k	CF			21799	RN720	)	RESISTOR	R NETWO	RK A	3/44608
R702	680	CF			28723						•
R703	10k	CF		1 W	2882	DIODE	s				
R704	22k	CF			21812	D701		IN4148			23802
R705	5k6	CF			21806	D702		IN4148			23802
R706	470.	CF			21797	2.02		1111110			20002
R707	8k2	CF			21808	D704		L.E.D.			43847
R708	220k	PCP			36270	D705		BAX17			402022
17.00	220K	101			30270	D703	150V				37559
D710	2k2	CF			21802		130 4	ZENER			
R710	ZKZ	Cr			21002	D708	20017	IN4148			23802
D712	4701-	DCD			26271	D709	200V	ZENER			40052
R713	470k	PCP		1/11/	36271						
R714	1M	CF		1/2W	18588	D711	9V1	ZENER	¥		33934
R715	680k	CF	-	1/11/	31839	D712	5V 1	ZENER			33928
R716	33M	MG	5	1/2W	43008	D713		IN4148			23802
R717	33M	MG	5	½W	43008	D714		IN4148			23802
R718	22k	CF	10		3433	D715	200V	ZENER			40052
R719	18k	CF		½W	18565	D716	200V	ZENER			40052
						D717	200V	ZENER			40052
R721	180	CF		1/2W	18541	D718	12kV				44550
R722	1 k	CF			21799	D719	12kV				44550
R723	2k2	CF			21802	D720		IN4148			23802
R724	5k6	CF			21806	D721		BAX17			402022
R725	47k	PCP			38261	D722		IN4004			450266
R726	33k	MF	2		38630	D723		IN4004			450266
R727	150	CF			28719	D724		IN4004			450266
R728	68	CF			28716	D725		IN4004 IN4004			450266
R729	680	CF			28723	D725					
R730	1 k	CF			21799	D723 D727		IN4004			450266
R731	10k	MF	2		38618			IN4004			450266
R732	47k	CF	2		21815	D728		IN4004			450266
R732	22k	CF	10		3433	D729	2001/	IN4004			450266
R734		CF	A.O.T.		28716	D730	200V	ZENER			40052
	68		A.O.1.								
R735	lk5	CF			21801	****					
R736	1k	CF			21799		LANEOUS				
R737	10k	PCP			44959	V1		MULLARI			
R738	180	MF	2		38576			NOR	MAL VEF	RSION	44932
R739	47	CF		1/2 <b>W</b>	18534						
						T1					<del>451429</del>
R741	5k6	CC	5		2363					į	+26050
R742	220k	MF	2		38650						Ū
R743	33M	MG	5	½W	43008	SKG					37293
R744	1 M	CP		Α	4/44460	SKH					37293
R745	10k	CP	WITH SI	A	4/44461			•			
R746	82k	CF			21818	PLM					44960
R747	120k	CF			21820						
R748	100k	CF			21819	F701	125mA				450551

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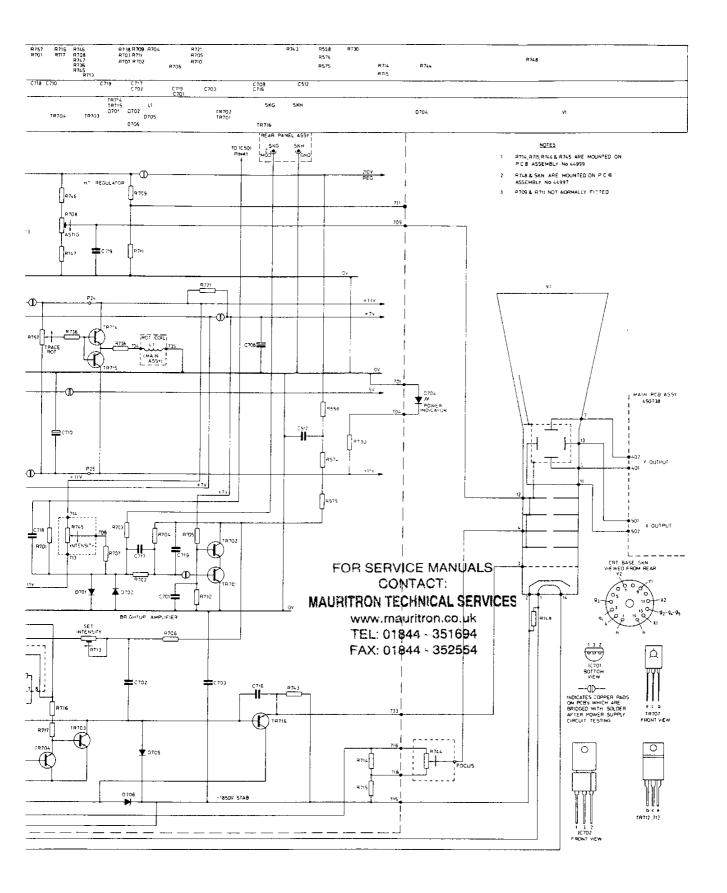


Fig. 11 Power Supply and CRT Circuit Diagram

**AUXILARY POWER SUPPLY** 

### Section 6

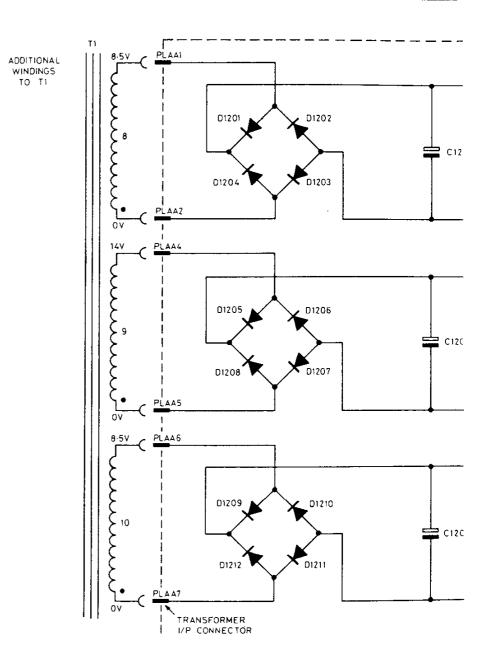
Ref	Value	Description	Tol %±	Rating	Part No	Ref	Value	Description	Tol %±	Rating	Part No
CAPACI	TORS										
C1201	6800μF	E		16V	450796	D1203		IN4003			23462
C1202	$2.2\mu F$	T		35V	35930	D1204		IN4003			23462
C1203	$2.2\mu F$	T		35V	35930	D1205		IN4003			23462
C1204	4700μF	Ε		25V	38893	D1206		IN4003			23462
01305	22 5	-			25020	51000					

52 62 62 52 C1205 2.2μF C1206 2.2μF 35V 35930 D1207 IN4003 23462 35V T 35930 D1208 IN4003 23462 C1207 4700µF 16V 450795 D1209 Ε IN4003 23463 C1208 2.2µF Τ 35V 35930 D1210 IN4003 23463 C1209 2.2µF T 35V 35930 D1211 IN4003 23463 D1212 IN4003 23463 DIODES U1201 7805 36176 D1201 IN4003 23462 U1202 7812 36178 D1202 IN4003 23462 U1203 7905 36182

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CAPS.		C1201 C1204 C1207
MISC.	T1 D1201 - D1212	



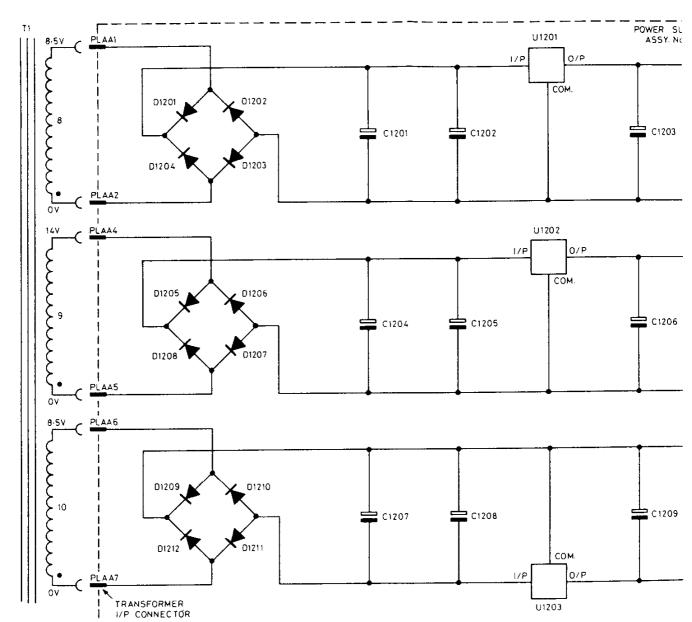
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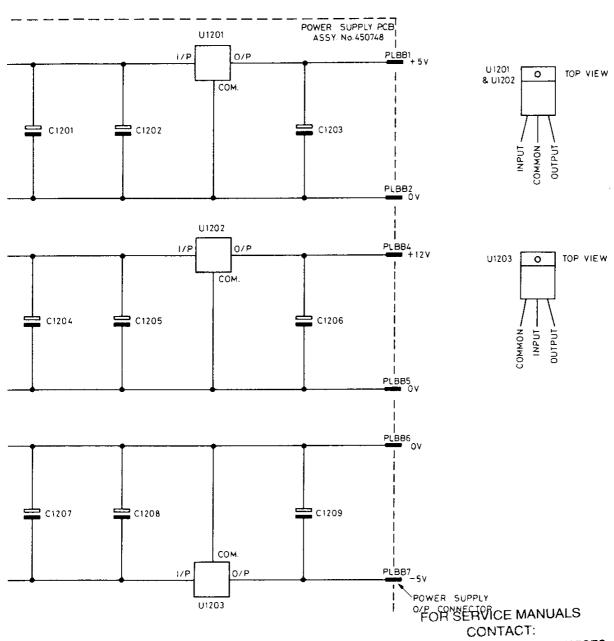
TEL: 01844 - 351694 FAX: 01844 - 352554

		C1201 C1204 C1207	C1202 C1205 C1208	C1203 C1206 C1209
т1	D1201 - D1212		U120 U120 U120	02





C1201 C1204 C1207	C1202 C1205 C1208		C1203 C1206 C1209	
		ป1201 ป1202 ป1203		



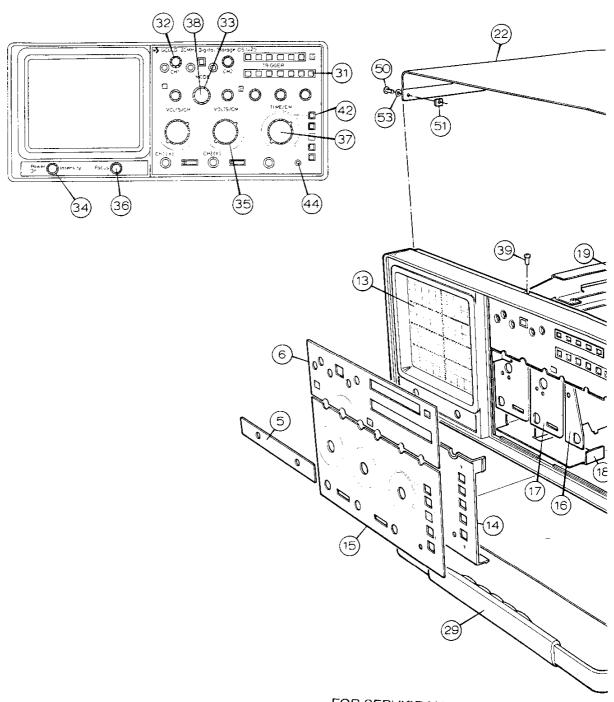
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Fig. 12 Auxiliary Power Supply

### Section 6

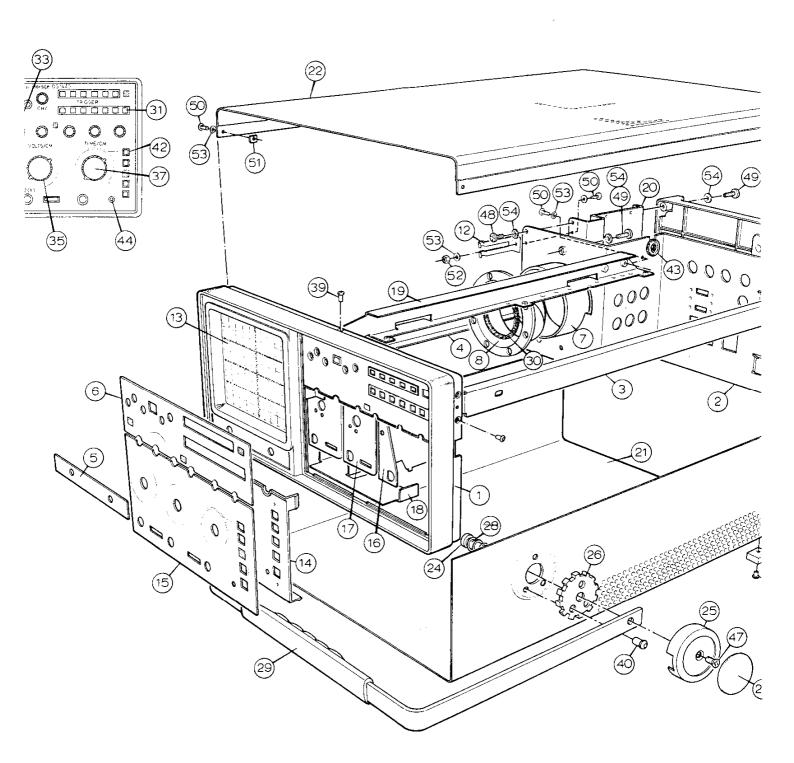
## **Component List and Illustrations**

Ref	Description	Part No	
1	Frame/Panel Moulding	451068	
2	Panel Rear	451595	
3	Support Side (Long)	450730	
4	Side Support (Short)	450043	
5	Coverlay Focus/Brill	450754	
6	Coverlay Pushbuttons	450731	
7	Clamp C.R.T. (Moulding)	450009	
8	Base C.R.T. (Moulding)	450008	
9	Cover Rear (Moulding)	44969	
10	Holder Fuse	40068	
11	Connector Supply	44960	
12	Earth Spring	44984	
13	Graticule Blue	44964	
14	Panel Front	44478	
15	Coverlay	450732	
16	Screen Timebase	44972	'
17	Screen Attenuator	44973	
18	Screen B.N.C. Sockets	450089	
19	Heatsink	450648	
20	Heatsink (Aux Power Supply)	450752	
21	Case Bottom	450768	
22	Case Top	450769	
23	Button Handle	36681	
24	Spindle Moulded	44470	
25	Cover Handle	44471	
26	Base Handle	44472	
27	Foot	36329	
28	Spring	44568	
29	Handle Assy	44469	
30	Washer C.R.T.	44963	
31	Knob — Pushbutton	38407	
32	Knob 10mm 'D' Type	402009	
33	Knob 15mm 'D' Winged	402010	
34	Knob R2-234	40408	
35	Knob R4–454 (21mm)	40410	
36	Cap W1-208	44957	
37	Cap W1 -400	44958	
38	Cap W1-300	44959 450690	
39	'POP' Rivet	12862	FOR SERVICE MANUALS
40	River .2" Long	29426	CONTACT:
41	Rivet .29" Long	43256	MAURITRON TECHNICAL SERVICES
42	Bezel	382	www.mauritron.co.uk
43 44	Grommet Terminal	24159	TEL: 01844 - 351694
44	Fuse 500mA	33685	
46	Fuse 250mA	33684	FAX: 01844 - 352554
40 47	Screw M4 x 12 C'sk Hd.	33077	
48	Screw M4 x 8 Pan Hd.	33044	
49	Screw M4 x 10 Pan Hd.	33045	
50	Screw M4 x 10 ran rid. Screw M3 x 8 Pan Hd.	33038	
51	Nut M3 Sq.	41407	
52	Nut M3 Sq.	33023	
53	Washer M3 Wavey	33016	
54	Washer M4 Wavey	33017	



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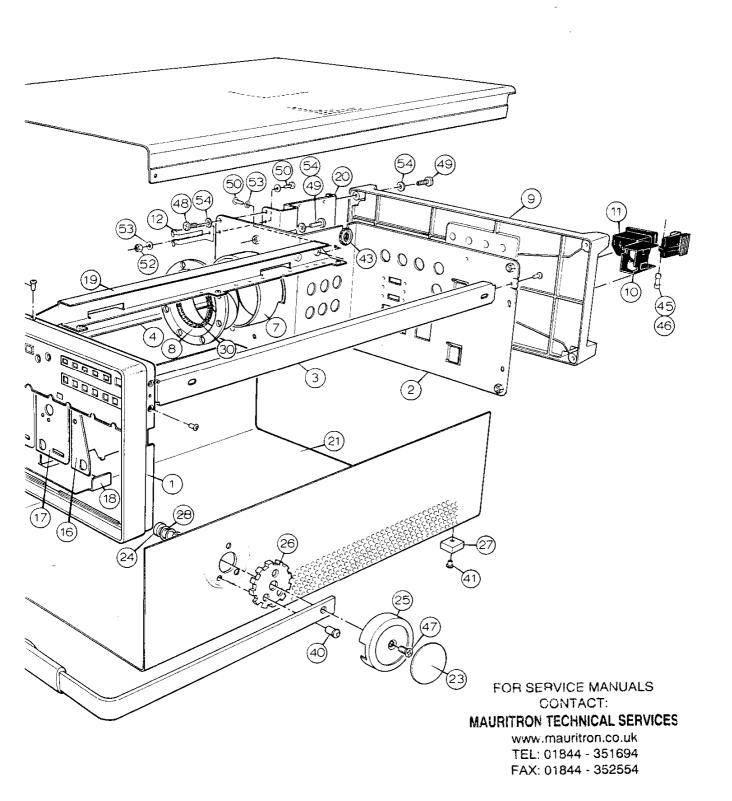


Fig. 13 Mechanical View Circuit Diagram

#### **Guarantee and Service Facilities**

#### Section 7

This instrument is guaranteed for a period of two years from its delivery to the purchaser, covering faulty workmanship and replacement of defective parts other than cathode ray tubes and batteries (where fitted). Cathode ray tubes are subject to the manufacturers guarantee. This assumes fair wear and tear and usage in the specified environment and does not cover routine recalibrations and mechanical adjustments.

We maintain comprehensive after sales facilities and the instrument should be returned to our factory for servicing if this is necessary. The type and serial number of the instrument should always be quoted, together with full details of any fault and service required.

Equipment returned for servicing must be adequately packed, preferably in the box in which the instrument was supplied and shipped with transportation charges

Service Dept., Roebuck Road, Hainault, Essex, IG6 3UE

Tel: 01-500 1000 Telex: 263785

Telegrams: Attenuate Ilford

prepaid. We accept no responsibility for instruments arriving damaged. Should the cause of failure during the guarantee period be due to misuse or abuse of the instrument, or if the guarantee has expired the repair will be put in hand without delay and charged unless other instructions are received.

Our Sales, Service and Engineering Departments are ready to assist you at all times.

The Service Department can provide maintenance and repair information by telephone or letter, if required.

Note: Please check fuses before returning instruments for service and ensure that any 13 Amp mains plugs fitted are removed. To prevent possible transit damage, we regret that mains plugs cannot be returned.

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